

BVR, POTSDAM, AND HARVARD PHOTOMETRIES

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SUMARIO

Las fotometrías visuales de Potsdam y de Harvard se han transformado al sistema foto-eléctrico BVR con ayuda del método de análisis de regresión múltiple. Los resultados indican que las transformaciones son aceptables y que dependen marcadamente del color de la estrella. La dependencia de las desviaciones de la escala de Pogson y del efecto Purkinje no es grande. La ausencia de estos factores en las fórmulas hacen que los resultados tengan una tendencia sistemática: en las estrellas brillantes hay más residuos positivos y en las estrellas débiles hay más residuos negativos. Cuando la muestra de magnitudes se divide en zonas de ascensión recta o declinación los resultados difieren un poco de aquellos en que se incluyen todas las A. R. y Dec. La fotometría de Harvard tiene su punto cero más cercano al del sistema BVR que la de Potsdam. Esta última, sin embargo, es más uniforme que la primera. Probablemente el color B-V casi siempre dé resultados ligeramente mejores que el V-R.

Las ecuaciones dadas al final del resumen en inglés ilustran las propiedades arriba mencionadas. Los símbolos que aparecen en estas ecuaciones representan la magnitud y los colores del sistema BVR, V, B-V y V-R; a las magnitudes de Potsdam y de Harvard, Gr y m44, respectivamente, al número de estrellas, n, que se metieron en la solución y el error estandar de la estimación. Otros datos estadísticos y más ecuaciones se dan también en las tablas 2-5.

ABSTRACT

Multiple Regression Analysis has been used to find equations to transform Potsdam (Müller and Kempf, 1907) and Harvard (Pickering, 1908) visual photometries into the BVR photoelectric system (Johnson and Mitchell, 1962). The results indicate that the transformations are good. They strongly depend on the colors (B-V or V-R). The dependence on Pogson scale deviation and Purkinje effect is not large. However, if these coefficients are absent in the formulae (Ideal Systems), then the residuals are not distributed at random in the (magnitude, residuals)-plane, specially at both ends. If a sample of magnitudes is divided in zones according to the stellar right ascension or declination, then the results are somewhat different than those that include all R. A. and Dec. The Harvard photometry has a zero point closer to that of the BVR-system than Potsdam's. However, the latter is more uniform than the former. In most cases probably the B-V color gives slightly better results than V-R.

The following equations are a part of the results given in Tables 2-5. They illustrate the characteristics of Harvard and Potsdam visual photometries. The symbols in these equations represent V, B-V and V-R, the visual magnitude and colors of the BVR-system; Gr and m44, the Potsdam and Harvard visual magnitudes (see Table 1) respectively; n, the number of stars entered in the solution; and ϵ , the standard error of the estimation:

$$\begin{aligned} \text{Gr-V} &= 0.253 - 0.070 (\text{B-V}) + 0.001 (\text{Gr-4.92}) - 0.014 (\text{B-V}) (\text{Gr-4.92}); \\ &\quad n = 963; \text{ all R. A.; all Dec.; } \epsilon = \pm 0.09. \\ \text{Gr-V} &= 0.258 - 0.091 (\text{V-R}) + 0.000 (\text{Gr-4.92}) - 0.012 (\text{V-R}) (\text{Gr-4.92}); \\ &\quad n = 963; \text{ all R. A.; all Dec.; } \epsilon = \pm 0.09. \\ \text{Gr-V} &= 0.227 - 0.066 (\text{B-V}) - 0.022 (\text{Gr-4.61}) + 0.009 (\text{B-V}) (\text{Gr-4.61}); \\ &\quad n = 86; \text{ all R. A.; } 90^\circ \geq \text{Dec.} > 60^\circ; \epsilon = \pm 0.07. \\ \text{Gr-V} &= 0.229 - 0.082 (\text{V-R}) - 0.024 (\text{Gr-4.61}) + 0.019 (\text{V-R}) (\text{Gr-4.61}); \\ &\quad n = 86; \text{ all R. A.; } 90^\circ \geq \text{Dec.} > 60^\circ; \epsilon = \pm 0.07. \\ \text{Gr-V} &= 0.234 - 0.059 (\text{B-V}) - 0.033 (\text{Gr-4.66}) + 0.008 (\text{B-V}) (\text{Gr-4.66}); \\ &\quad n = 293; 16 \text{ hs} \leq \text{R. A.} < 24 \text{ hs.; all Dec.; } \epsilon = \pm 0.09. \\ \text{Gr-V} &= 0.237 - 0.080 (\text{V-R}) - 0.036 (\text{Gr-4.66}) + 0.021 (\text{V-R}) (\text{Gr-4.66}); \\ &\quad n = 293; 16 \text{ hs} \leq \text{R. A.} < 24 \text{ hs.; all Dec.; } \epsilon = \pm 0.09. \\ \text{m44-V} &= 0.018 + 0.128 (\text{B-V}) - 0.039 (\text{m44-4.42}) + 0.061 (\text{B-V}) (\text{m44-4.45}); \\ &\quad n = 1421; \text{ all R. A.; all Dec.; } \epsilon = \pm 0.21. \\ \text{m44-V} &= 0.014 + 0.159 (\text{V-R}) - 0.038 (\text{m44-4.42}) + 0.067 (\text{V-R}) (\text{m44-4.45}); \\ &\quad n = 1421; \text{ all R. A.; all Dec.; } \epsilon = \pm 0.21. \\ \text{m44-V} &= 0.028 + 0.141 (\text{B-V}) - 0.029 (\text{m44-4.08}) + 0.006 (\text{B-V}) (\text{m44-4.08}); \\ &\quad n = 50; \text{ circumpolar stars; } \epsilon = \pm 0.08. \\ \text{m44-V} &= 0.027 + 0.166 (\text{V-R}) - 0.023 (\text{m44-4.08}) - 0.014 (\text{V-R}) (\text{m44-4.08}); \\ &\quad n = 50; \text{ circumpolar stars; } \epsilon = \pm 0.08. \\ \text{m44-V} &= -0.029 + 0.127 (\text{B-V}) - 0.045 (\text{m44-4.45}) + 0.051 (\text{B-V}) (\text{m44-4.45}); \\ &\quad n = 83; 8 \text{ hs.} \leq \text{R. A.} < 16 \text{ hs., } 60^\circ \geq \text{Dec.} > 30^\circ; \epsilon = \pm 0.11. \\ \text{m44-V} &= -0.029 + 0.151 (\text{V-R}) - 0.041 (\text{m44-4.45}) + 0.044 (\text{V-R}) (\text{m44-4.45}); \\ &\quad n = 83; 8 \text{ hs.} \leq \text{R. A.} < 16 \text{ hs.; } 60^\circ \geq \text{Dec.} > 30^\circ; \epsilon = \pm 0.12. \end{aligned}$$

Other statistical results are also given in Tables 2-5.

I. Introduction

Müller and Kempf (1907) determined visually magnitudes of 14199 stars brighter than 7.5 mag. at Potsdam. Bailey, Frost, Pickering, Searle, and Wendell (see H. A. 50, 1908) measured 9110 stars brighter than 6.5, distributed over the entire sky from the North to the South Pole. All these observations are very valuable for many astrophysical problems since they were performed with great care.

It is well known that the human eye is not an ideal detector for photometry. At very low levels of illumination (starlight) the eye becomes more sensitive to blue and less sensitive to red light

(Purkinje effect). When dark adapted, a different spectral curve (scotopic) is valid for the eye than under daylight conditions (photopic). These curves change from eye to eye and with age.

To make the best use of the above visual photometries, they should be transformed to an "ideal system" (see section III). In this paper we have taken the BVR photoelectric system defined by Johnson and Mitchell (1962) as the system to which Potsdam and Harvard photometries can be transformed.

II. Selection of the data

We have selected 1640 stars that are listed either in Potsdam or Harvard photometric catalogues (Müller and Kempf, 1907 and Pickering, 1908); in addition they also have been observed in the BVR system (Johnson and Mitchell, 1962). The photoelectric data have been taken from Johnson, Mitchell, Iriarte, and Wisniewski (1966) and Mendoza (1967, 1967b, and 1969a and 1969b). The selected stars are listed in Table I. The columns of Table I give:

- 1st, Bright Star (BS) Catalogue number (Hoffleit, 1964);
- 2nd, Potsdam Star (PD) Catalogue number (Müller and Kempf, 1907);
- 3rd, V magnitude;
- 4th-5th, (B-V) and (V-R) colors;
- 6th, Mean PD magnitude (Müller and Kempf, 1907; Table 1, column 9), Gr;
- 7th, PD magnitude (Müller and Kempf, 1907; Table 1, column 6, left), Gr 1;
- 8th, PD magnitude (Müller and Kempf, 1907; Table 1, column 6, right), Gr 2;
- 9th, Mean Harvard Revised Magnitude (H. A. 50, Table 1, column 9), mag;
- 10th, Magnitude in H. A. 14, Table XXVII, column 13th (m14);
- 11th, Magnitude in H. A. 23, Table VI, column 19th (m23);
- 12th, Magnitude in H. A. 24, Table I, column 5th (m24,1);
- 13th, Magnitude in H. A. 24, Table IV, column 6th (m24,4);
- 14th, Magnitude in H. A. 34, Table VII, column 6th (m34);
- 15th, Magnitude in H. A. 44, Table I, column 5th (m44);
- 16th, Magnitude in H. A. 45, Table "A Photometric Durchmusterung", column 5th (m45);
- 17th, Magnitude in H. A. 46, Table I, column 5th and Table VI, column 5th (m46);
- 18th, Remarks, C = HR standard (circumpolar star); D = double or multiple star; F = PD standard; V = variable star (only those with a small amplitude are included in Table I).

III. Transfer from one system to another

Ideal systems are linear, have the Pogson scale and are independent of intensity. They may differ only in their zero point and/or in the spectral sensitivity function of their photometric receivers. Strömgren (1937) has shown that the difference between two ideal magnitude systems is nearly linear in the reciprocal color temperature or

$$m(1) - m(2) = a + bC \quad (1)$$

where $m(1)$ and $m(2)$ are the magnitudes in the two systems; a and b are constants, and C is the color index.

Except for good photoelectric systems which because of the nature of the photocell are linear, a magnitude system will probably not be ideal. Instead of differing from another ideal system by merely a zero point correction they will also differ in scale and probably will also evidence Purkinje effect. Let us suppose that the scale of the catalogue in question is not a Pogson scale but it is characterized by the constant $2.5/(1-s)$ where $s \ll 1$, usually. If Purkinje effect is present the spectral sensitivity function will depend on the magnitude. Strömgren (1937) also has shown that the comparison of two observational systems, in the first order approximation, is given by equation (1) for any two ideal systems and by

$$m(1) - m(2) = a + bC + s(m-m_0) + p(m-m_0) C \quad (2)$$

where $m(1)$ and $m(2)$ are, again, the magnitudes in the two systems, a , b , s , p are constants, C is the color index, m is either $m(1)$ or $m(2)$, and m_0 is also a constant (a standard magnitude). In equation (2), $m(1)$, $m(2)$, $m-m_0$ and C are known. A least squares solution can give a , b , s (Pogson scale deviation) and p (Purkinje effect contribution).

T A B L E 1

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BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
					(PD magnitudes)			(H a r v a r d									
3		4.61	1.04	0.78	2.42	2.43	2.41	4.68	4.62					4.62	4.78	4.72	
15	31	2.06	-0.11	-0.03	2.56	2.58	2.55	2.15	2.08			2.16		2.09	2.28		
21	41	2.27	0.34	0.31	2.56	2.58	2.55	2.42	2.42	2.39				2.44	2.44		C
25		3.88	1.03	0.75	5.26	5.16	5.36	3.94	4.92			3.85		3.90	4.08	3.95	
27	51	5.04	0.40	0.42	5.26	5.16	5.36	5.08	4.92			5.12		5.23	5.04		
39	81	2.84	-0.23	-0.10	3.28	3.12	3.25	2.87	3.04			2.77		2.80			V
45	97	4.80	1.57	1.34	5.00	5.03	4.98	4.94	4.92	4.60		4.95		4.94			
48		4.46	1.66	1.40	4.67	4.72	4.62	4.68	4.62					4.87			
63	128	4.61	0.06	0.08	4.67	4.72	4.62	4.44	4.50					4.57			
68	147	4.52	0.05	0.08	4.70	4.81	4.59	4.51	4.65					4.45	4.44		
74		3.55	1.22	0.85	3.75	3.75	3.62	3.75	3.62	3.91				3.85	3.69	3.66	
77		4.23	0.58	0.49	4.34	4.34	4.34	4.34	4.34			4.28		4.39	4.39	4.39	
98		2.80	0.62	0.50	2.90	2.90	2.90	2.90	2.90			2.91		2.89	2.89	2.89	
99		2.40	1.09	0.81	2.44	2.44	2.44	2.44	2.44			2.45		2.40	2.42	2.48	
100		3.94	0.17	0.14	3.90	3.90	3.90	3.90	3.90			3.95		3.78	3.69	4.18	
105	271	4.81	1.64	1.59	4.93	4.92	4.94	4.96	4.78	5.13		4.81		4.99	5.10	4.93	V
123		4.73	-0.10	0.00	4.93	4.92	4.94	4.85	4.83			4.50		4.93	4.87	4.54	D
126		4.27	-0.05	0.00	4.93	4.92	4.94	4.85	4.83			4.50		4.93	4.87	4.54	
127		4.55	0.14	0.18	4.38	4.33	4.44	4.48	4.18	4.28		4.53		4.25	4.23	4.64	
130	290	4.16	0.14	0.14	4.38	4.33	4.44	4.24	4.18	4.28		4.53		4.25	4.23	4.64	C
153	331	3.66	-0.19	-0.08	4.08	4.14	4.01	3.72	3.74					3.78	3.65		
154	332	4.36	-0.16	-0.04	4.52	4.53	4.52	4.44	4.39					4.50			
163	350	4.38	0.87	0.68	4.52	4.65	4.40	4.52	4.58					4.45			
165	355	3.28	1.28	0.92	3.48	3.41	3.50	3.49	3.41			3.66		3.40	6.06		
166	357	5.86	0.85	0.65	6.08	6.05	6.12	6.08	6.08	6.15				6.04			
168		3.23	1.17	0.78	2.47	2.47	2.47	2.47	2.25					2.47	2.69		
175	368	5.23	0.89	0.71	5.60	5.71	5.48	5.42	5.57					5.27			
179	376	4.81	-0.10	-0.01	5.08	5.20	4.97	4.85	4.80			4.61		4.90	4.89	4.63	
180		4.59	0.97	0.75	4.65	4.65	4.65	4.65	4.65			2.31		4.48	4.89	2.18	
188		2.02	1.01	0.72	2.24	2.24	2.24	2.24	2.13					2.35			
191		4.36	-0.01	0.06	4.53	4.53	4.53	4.53	4.53			4.49		4.77	4.57	4.57	
193	396	4.50	-0.06	0.05	4.86	4.91	4.81	4.70	4.64					4.88			
194		4.75	1.00	0.74	4.34	4.22	4.39	4.93	4.93					4.21	4.31	4.98	V
215	419	4.06	1.12	0.85	3.72	3.74	3.75	3.64	3.64			3.64		3.62	3.65		D
219	429	3.44	0.58	0.50	3.72	3.74	3.75	3.64	3.64					3.62			
222	432	5.76	0.88	0.77	5.98	5.96	6.01	5.82	5.68			5.93		5.85			
224	435	4.44	1.51	1.17	4.65	4.67	4.64	4.55	4.58					4.52			
226	448	4.55	-0.15	-0.03	4.80	4.82	4.79	4.42	4.42					4.43			
235		5.20	0.50	0.46	5.24	5.24	5.24	5.24	5.27					5.21			
244	480	4.82	0.53	0.48	5.06	5.11	5.00	4.93	4.89			5.06		4.80	4.97		

T A B L E 1 (continued)

BS	ED	V	B-V	V-R	Gr	Gr1	Gr2	m _g	m14	m23	m24,1	m25,4	m34	m44	m45	m46	R
510	1046	4.26	0.26	0.74	4.56	4.48	4.64	4.50	4.42			4.65		4.45	4.46		R
511	1050	2.63	0.81	0.64	5.82	5.70	5.94	5.74	5.74				5.40	4.84	4.64	5.52	D
519	1078	3.49	1.29	1.49	6.07	6.09	6.05	5.89	5.98					5.74	5.96	4.92	D
530		5.86	0.74	0.68				4.77	4.77					4.74	4.74		
531		4.68	0.32	0.29													
534	1088	5.94	0.30	0.33	6.17	6.17	6.17	5.94	5.83			6.10		5.82	6.00		R
539		3.72	1.14	0.80				3.92	3.85					3.94	3.96		
542	1102	3.38	-0.15	-0.04	3.64	3.71	3.58	3.44	3.55	3.43				3.40	3.39		C
544	1105	3.42	0.48	0.42	3.64	3.69	3.58	3.58	3.58					3.58			
545	1109	3.88	-0.04	0.01	4.15	4.07	4.23	4.04	4.27			4.02		3.87	4.00		D
549	1114	4.63	0.94	0.73	4.91	4.89	4.93	4.84	4.74			4.99		4.78			
553	1127	2.65	0.13	0.14	3.02	2.96	3.07	2.72	2.79		2.45	2.87		2.79			
555		4.41	1.52	1.73				4.41					4.11	4.65	4.69	4.43	
558		3.11	-0.06	0.02				5.00					4.95	4.86	4.86	5.35	
566		3.67	0.84	0.68				3.73					3.62		3.84		
569	1158	4.79	0.28	0.28	5.02	4.94	5.10	4.83	4.89					4.74	4.85		
570		4.71	0.94	0.75				4.72						4.65		4.78	
574		4.83	0.88	0.70	4.72	4.79	4.66	4.74	4.60	4.62			4.65	4.62	4.61	4.84	C
575	1165	4.54	0.16	0.18	4.72	4.79	4.66	4.61	4.60					4.62			
580	1176	3.98	-0.01	0.06	4.12	4.18	4.05	4.06	4.06					4.05			
585		4.01	1.56	1.26				4.18	3.83			4.48		4.25	4.27	4.08	
590	1183	5.04	-0.08	0.03	5.22	5.22	5.22	4.99	4.93				2.96	5.05	5.00	3.08	
591		2.84	0.29	0.29				3.02						4.02			
595	1193	3.82	0.02	0.08	4.12	4.07	4.18	4.16	4.21			4.24		5.48			D
599	1197	3.50	0.03	0.06	5.80	5.76	5.83	5.44	5.40								
602		5.14	1.49	1.22				4.96					4.91	4.97	5.01	5.01	D
603	1204	2.10	1.21	0.94	2.35	2.37	2.33	2.20	2.14				4.79	2.36		4.92	
612		4.69	-0.17	-0.04				4.74	4.63				4.65	4.58			
617	1234	2.00	1.15	0.84	2.19	2.19	2.19	2.23	2.04					2.19			
618	1236	5.67	0.61	0.59	5.86	5.86	5.86	5.90							5.90		
620	1241	4.83	0.12	0.14	4.95	4.83	5.07	4.77	4.77					4.77			
622	1251	3.00	0.14	0.14	3.30	3.27	3.33	3.08	3.12			3.14		2.96			
627	1260	6.35	0.33	0.34	6.56	6.46	6.66	6.36				6.36		6.53	6.46		
641	1276	6.43	0.60	0.55	6.58	6.58	6.59	6.50						6.53	6.03		
647	1291	6.06	0.40	0.38	6.12	6.12	6.13	6.03									
648	1290	5.70	1.55	1.24	5.76	5.76	5.76	5.99	6.17					5.81			
649	1292	4.37	0.88	0.67	4.70	4.69	4.70	4.54	4.45			4.54		4.63			
654	1313	7.38	0.25	0.26	7.50	7.40	7.59								6.42		
654	1315	6.48	0.28	0.34	6.78	6.68	6.89	6.42	5.79		5.91			5.83			
656	1319	5.79	0.44	0.40	5.96	6.00	5.92	5.84						4.10			
664		4.01	0.02	0.03	4.28	4.28	4.29	4.07	4.15			3.95		4.10			
664	1331	6.52	0.45	0.52	6.80	6.73	6.88										
664	1340	6.63	0.50	0.55	6.90	6.85	6.94										
695		5.20	0.60	0.54				5.37	5.36			5.57		5.21		5.34	
695	1364	6.83	0.31	0.41	7.02	7.05	7.00										
696	1377	6.37	0.56	0.60	6.62	6.56	6.69										
696	1386	7.44	0.70	0.73	7.56	7.55	7.58										
696	1387	6.98	0.62	0.58	7.06	7.00	7.12				6.26						
696	1409	6.25	0.39	0.33	6.48	6.49	6.47	6.24	6.23					6.27	6.21		
699	1413	4.70	1.33	1.18	4.83	4.93	4.73	4.86	4.87					4.80	4.91		

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	G _r	G _r 1	G _r 2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
707	1430	4.53	0.13	0.16	4.78	4.81	4.75	4.59	4.61	4.56				4.60	4.58		D
708		4.89	-0.02	-0.02				4.90	4.88					4.90	4.87	4.96	
710	1417	5.83	0.14	0.12	7.66	7.82	7.42	5.84	5.48	6.02	5.84			5.84	5.84	6.03	
	1422	7.38	0.44	0.44	7.28	7.34	7.22										
	1446	7.22	0.77	0.71	7.26	7.26	7.27	4.34	4.41		4.29	4.28		4.31			
718	1448	4.29	-0.06	0.02	4.48	4.47	4.50	4.44	4.70							4.55	
721		4.25	-0.14	-0.03				4.82									
740		4.55	0.45	0.41				4.95						4.78	4.80	4.84	D
749		4.89	-0.06	0.02													
	1471	7.01	0.78	0.71	7.10	7.09	7.11	5.92	5.89					5.96			
753	1545	5.82	0.97	0.83	6.16	6.12	6.20	5.02	4.90	5.11	5.14			5.96			
754	1547	4.86	0.86	0.65	5.06	5.05	5.08	4.04	4.13		3.88			4.10	3.90	4.21	
779		4.06	-0.21	-0.07				4.99	4.90					5.06	5.00		
788	1598	4.92	0.59	0.50	5.24	5.26	5.21	4.53	4.67					4.28	4.17	4.95	
								4.06						3.92	4.00	4.20	
789		4.75	0.06	0.10				6.27	6.26					6.24			
794	1607	4.11	1.02	0.79	7.98	8.09	7.88	4.22	4.24					4.30	4.13		
	1611	6.30	0.06	0.05	6.62	6.57	6.66										
797	1614	4.13	0.49	0.46	4.33	4.33	4.34										
799		4.75	0.13	0.02													
801	1616	4.67	-0.13	-0.02	4.92	5.01	4.83	4.58	4.68					4.47	3.64	4.45	D
804	1623	3.47	0.09	0.11	3.80	3.80	3.83	3.58	3.59		3.67			4.47			
811		4.25	-0.14	-0.02				4.39	4.28					4.37			
813	1635	4.27	0.31	0.30	4.41	4.54	4.28	4.36	4.38		4.46			4.33			
818		4.46	0.48	0.43				4.61	4.67					4.65	4.48	4.56	
824	1661	4.52	1.11	0.80	4.79	4.84	4.74	4.62	4.64					4.63	4.60		
825	1664	6.26	0.88	0.82	6.37	6.41	6.33	6.53						4.63	6.53		
834	1677	3.79	1.69	1.23	3.91	3.88	3.94	3.93						3.93			
838	1684	3.63	-0.10	-0.02	3.67	3.71	3.62	3.68	3.78					3.93			
840	1687	4.23	0.34	0.30	4.51	4.61	4.41	4.27	4.44					4.15	4.24		
841	1698	4.46	0.99	0.76	4.66	4.72	4.61	4.50	4.71					4.60	4.54	4.42	
843		4.53	1.56	1.21				4.67	4.80					4.47	4.75		
850	1708	4.77	0.90	0.70	4.10	4.10	4.11	4.81	4.83		4.88			4.90	4.75	4.62	
854		3.95	0.75	0.62				4.06	3.97					4.07	4.14		
857		6.05	0.87	0.71				6.14			6.11			6.12	6.18		
874		3.87	1.12	0.79				4.05	3.95					4.00		4.02	
875		5.17	0.08	0.11				5.27	5.21		4.24			4.00			
878	1756	5.80	0.41	0.38	6.06	6.04	6.07	5.85	5.88		5.38			5.13		5.37	
879	1757	4.70	0.05	0.10	4.88	4.77	4.98	4.62	4.74		5.90			5.78			
882	1760	4.94	1.25	0.89	5.10	5.03	5.17	4.62	4.74					4.50			
								4.97	5.04					4.90			
887	1768	4.63	0.04	0.05	4.74	4.70	4.78	5.55	5.49					5.62	5.56		D
896	1776	4.70	-0.12	-0.03	4.96	4.96	4.96	3.69	4.60					4.71			
897		3.51	0.12	0.14				3.06						4.71	2.79	3.28	D
906	1793	5.95	0.15	0.13	5.98	6.01	5.95	5.95	5.97					5.98			
911	1797	2.53	1.64	1.35	2.89	2.83	2.96	2.82	2.68		5.90			2.96			
														2.84			
915	1805	2.93	0.70	0.59	3.17	3.17	3.16	3.08	3.11					3.03	3.10		
919		4.09	0.16	0.13				4.16	4.10					4.12		4.32	
932	1837	4.88	0.02	0.08	5.12	5.20	5.04	4.89	4.73					4.98	4.96		
937	1844	4.05	0.60	0.53	4.22	4.21	4.22	4.17	4.14					4.20			
941	1852	3.81	0.98	0.74	3.98	3.94	4.01	4.00	3.95					4.07	3.98		

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
947	1873	4.64	1.11	0.83	4.70	4.67	4.74	4.82	4.74					4.90			
951	1885	4.37	1.03	0.77	4.68	4.69	4.67	4.53	4.48			4.05		4.64	4.46	4.03	D
963		3.85	0.51	0.46				3.95	3.77			4.88		3.95			
972	1914	4.89	-0.02	0.06	5.09	5.06	5.12	4.95	4.93				5.71	5.16	4.83	5.74	V
977		5.74	2.27	1.89				5.72									
984		4.80	0.23	0.22				4.90	4.80		5.02			4.83	4.85	5.00	C
985	1931	4.85	-0.15	-0.03	5.02	5.18	5.03	4.76	4.78	4.72	4.76			4.75	4.81		
1942		7.40	0.57	0.49	7.80	7.90	7.70	4.80	4.80					4.93	5.04		
991	1948	4.82	1.49	1.07	4.96	4.90	5.03	4.92	4.97					5.01	4.90		
996	1964	4.84	0.68	0.57	5.23	5.27	5.19	4.96	4.97					4.90	4.90		
999	1965	4.47	1.54	1.20	4.54	4.54	4.54	4.72	4.73					4.70			F
1002		4.95	0.04	0.08	5.18	5.10	5.27	4.98	4.84					5.03			
1003	1973	3.70	1.62	1.58				3.95	3.79			4.11		3.95			
1006		5.54	0.64	0.54				5.48					5.47	4.26	4.21	5.49	
1008		4.27	0.71	0.62				4.30					4.27	4.26	4.21	4.47	
1010		5.24	0.60	0.49				5.16					5.13	5.55	5.68	5.20	
1016		5.52	0.88	0.66				5.67	5.76					1.85			
1017	1993	1.79	0.48	0.45	2.16	2.16	2.15	1.90	1.94			5.69		3.78	3.85		
1030	2023	3.60	0.89	0.68	3.86	3.79	3.92	3.80	3.77			3.82		4.90			
1034	2037	4.98	-0.10	0.01	5.23	5.18	5.29	4.94	4.95			4.97		4.90			
1035	2038	4.21	0.41	0.37	4.43	4.42	4.44	4.42	4.16					4.48	4.63		D
1038		3.75	-0.09	-0.01	3.94	3.80	4.07	3.75	3.77			3.70		4.73			
1040	2050	4.54	0.56	0.51	4.75	4.73	4.77	4.76	4.79					4.73			
1044	2055	4.67	-0.09	0.02	4.92	4.87	4.96	4.67	4.77					4.53	4.71		
1046	2061	5.10	0.04	0.09	5.26	5.23	5.28	4.98	4.96		4.91			5.07			D
1052	2074	4.38	1.34	1.09	4.52	4.54	4.49	4.55	4.39					4.50	4.76		
1066	2104	4.10	1.15	0.77	4.44	4.57	4.50	4.28	4.26			4.30		4.28			
1069		5.32	0.41	0.41	5.51	5.52	5.50	5.35	5.40					5.27	5.39	4.94	
1070		4.73	-0.09	-0.01				4.80	4.75			4.82		4.67			
1084		3.73	0.88	0.72				3.81	3.66			3.88		3.80		3.80	
1087	2148	4.23	-0.06	0.10	4.63	4.63	4.63	4.26	4.24					4.22	4.31		
1088		4.28	-0.12	0.00				4.32	4.21			4.31		4.29		4.47	
1101		4.28	0.57	0.49				4.40	4.35					4.44	4.45		
1103	2182	6.50	0.15	0.17	6.74	6.71	6.76	6.42	6.15			6.52		6.52	6.47		
1106		4.58	1.04	0.84				4.58					4.48	4.55	4.66	4.62	
2180		6.77	0.00	0.05	6.94	6.89	6.99										
2184		7.28	0.08	0.10	7.48	7.49	7.46										
2212		5.01	-0.12	0.02	5.51	5.51	5.50	3.10	3.18					3.11	3.00		F
2226		4.79	0.81	0.74	4.92	4.92	4.92	4.96	4.98					4.94	4.96		
2230		7.52	0.15	0.15	7.82	7.75	7.88										
2233		3.83	0.05	0.12	3.84	3.92	3.75	3.94	4.01					3.88			
1134	2233	5.00	-0.16	-0.05				4.93	4.77	4.94			4.92	4.94	4.89	5.11	
1135	2237	3.77	0.42	0.41	4.00	4.03	3.96	3.93	4.00					3.90	3.90		
1136		3.54	0.92	0.72				3.72	3.68			3.66		3.84			
1138	2243	5.44	0.09	0.11	5.56	5.48	5.64	5.40	5.31					5.50			
1140	2244	5.46	-0.04	0.06	5.90	5.88	5.92	5.43						5.40	5.42		
1142	2245	3.70	-0.12	-0.01	4.01	3.85	4.17	3.81						3.80			
1144	2248	5.65	-0.07	0.03	6.06	5.97	6.16	6.65						5.62			
1145	2249	4.30	-0.11	-0.01	4.61	4.47	4.57	4.44			5.81			4.50			
1148	2252	4.66	0.03	0.13	4.84	4.81	4.88	4.67	4.65	4.61				4.71	4.70		C

T A B L E 1 (continued)

ES	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
1149	2254	3.87	-0.07	0.04	4.11	4.02	4.20	4.02	3.98					4.07			
1151	2255	5.76	-0.04	0.06	6.14	6.10	6.19	5.85			5.95			5.84	5.77		
1152	2256	6.43	-0.02	0.04	6.71	6.76	6.66	6.46			6.46			4.76	4.68		VC
1155	2260	4.48	1.88	1.71	4.48	4.46	4.50	4.71	4.61	4.78	4.71			4.28	4.30		
1156	2262	4.18	-0.06	0.07	4.34	4.29	4.38	4.25	4.22		4.20						
2269	2269	6.83	0.02	0.07	7.18	7.13	7.24										
2272	2272	7.04	0.03	0.04	7.35	7.21	7.49										
2276	2276	7.24	0.07	0.12	7.55	7.57	7.53										
1162	2280	4.42	1.62	1.54	3.09	3.07	3.11	4.64	4.39		2.88			4.83	4.70		
1165	2280	2.87	-0.09	0.03	3.09	3.07	3.11	2.96	3.00					3.00			
1172	2281	6.83	0.07	0.09	7.14	7.12	7.15	5.51							5.55		
1173	2293	5.45	-0.07	0.05	5.83	5.82	5.84	4.33	4.30		4.36			4.33			
1178	2300	3.62	0.42	0.39	3.92	3.78	4.07	3.80	3.77					3.90	3.73		
1180	2302	5.09	-0.08	0.07	5.36	5.22	5.50	5.18						5.19	5.16		V
2303	2303	6.57	-0.02	0.03	7.04	7.09	7.00										
2308	2308	7.03	0.03	0.05	7.30	7.28	7.32										
2309	2309	6.17	-0.03	0.03	6.36	6.30	6.43	6.11						6.02	6.11		
1183	2311	6.07	-0.01	0.07	6.30	6.19	6.40	5.92	5.83								
1185	2312	6.72	0.06	0.10	7.04	6.98	7.10										
2318	2318	6.93	0.09	0.10	7.20	7.17	7.23			4.20			4.52	4.18	4.29	4.54	D
1189	2318	4.27	-0.01	0.02	4.24	4.24	4.24	4.24	4.24	4.37			4.12	4.38	4.20	4.15	
1195	2338	5.97	0.34	0.33	6.34	6.21	6.47	5.96	6.04					5.87			
1201	2339	6.36	0.12	0.10	6.57	6.57	6.57										
1203	2343	2.85	0.12	0.14	3.05	3.13	3.16	2.91	3.10					2.87	2.76		
1204	2351	5.04	-0.10	0.07	5.20	5.23	5.17	4.87	4.75					4.97	4.89		
1211	2351	4.45	0.68	0.59	4.20	4.10	4.31	4.28	4.79					4.58			
1213	2351	4.85	-0.13	-0.03	5.80	5.88	5.73	4.68	4.70		4.77		4.75	4.74			D
1220	2369	2.89	-0.18	-0.07	3.14	3.06	3.23	2.96	3.04					2.88			
1228	2369	4.04	0.02	0.16	4.05	4.06	4.05	4.05	4.06					4.08	4.01		
1231	2394	1.60	1.26	1.26	3.19	3.19	3.05				3.34			3.41	2.95		
1233	2378	7.20	0.04	0.05	7.42	7.43	7.41	6.42	6.42								
1238	2391	6.37	0.42	0.38	6.78	6.76	6.81	6.42	5.68		6.37			5.84	6.56		
1240	2403	5.89	0.32	0.32	6.20	6.16	6.25	5.76									
1242	2414	4.66	-0.14	0.02	4.51	4.51	4.51	4.69	4.62		4.71			4.62		4.80	
1244	2432	3.91	0.03	0.08	5.27	5.27	5.27	5.07	4.94					5.13	5.13		
1254	2436	5.46	0.36	0.37	4.20	4.10	4.31	3.94	3.99		4.02			3.90	3.85		
1256	2440	4.37	1.07	0.79	5.80	5.88	5.73	5.48	5.55		5.49			5.41			
1261	2448	4.29	0.02	0.08	4.48	4.55	4.40	4.30	4.45					4.54			
1264	2448	4.29	0.02	0.08	4.51	4.51	4.51	4.33	4.54		4.27		4.41	4.20	4.30	4.51	D
1273	2472	4.49	1.62	1.65	4.33	4.36	4.30	4.46	4.32					3.88			
1279	2481	6.01	-0.03	0.12	6.30	6.30	6.47	5.94			6.04			5.91	5.87		
1292	2511	6.62	0.42	0.39	6.98	6.96	7.00										
1298	2520	5.73	0.36	0.35	6.10	5.96	6.24	5.71	5.68		5.71			5.75	4.52	4.16	
1302	2520	4.05	0.33	0.31	4.14	4.14	4.14	4.10	4.10				4.78	4.17	4.82	4.92	
1303	2535	4.93	0.33	0.35	4.26	4.31	4.21	4.85	4.85					4.88			
1305	2535	4.15	0.95	0.70	4.26	4.31	4.21	4.23	4.23		4.30			4.30	4.82	4.92	
1306	2538	4.71	1.01	0.80	4.77	4.82	4.72	4.89	4.94		4.92			4.80			

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
1570	2991	4.67	0.08	0.11	4.94	4.94	4.94	4.74	4.82		4.72			4.69	2.99		F
1577	3004	2.69	1.55	1.06	2.84	2.84	2.84	2.50	2.72					2.99			
1580	3007	4.06	1.15	0.88	4.22	4.35	4.09	4.28	4.33					4.24	4.98		D
1592	3021	4.95	0.05	0.05	5.10	5.05	5.14	4.99	5.07					4.93	4.66		
1601	3027	4.49	1.40	1.05	4.60	4.66	4.55	4.73	4.72					4.82			
3035		6.76	0.45	0.38	6.98	6.92	7.04										
3040		4.03	0.93	0.70	4.14	4.11	4.17	4.22	4.21	4.22				4.24	4.19		V
1611	3048	4.78	0.26	0.28	3.85	3.84	3.86	3.94	3.96		6.64			4.80	4.02		
1612		3.75	1.22	1.13				3.94						3.80	6.36		
1614		6.21	1.06	0.85				6.50									
1617		4.81	-0.19	-0.08	4.90	4.79	5.01	4.81	4.66					4.82	4.72	5.05	
1620	3060	4.64	0.16	0.16	4.90	4.79	5.01	4.70	4.75					4.67	4.67	5.11	
1621		4.92	-0.05	0.02	5.16	5.17	5.14	4.99	5.05		5.01	5.07		4.90	4.87		
1637	3078	5.00	0.34	0.31	5.08	5.09	5.07	4.99	4.89					5.13	4.87		
1658	3077	4.68	-0.05	0.04	5.08	5.09	5.07	4.65	4.71					4.67	4.57		
1641	3085	3.18	-0.18	-0.05	3.46	3.44	3.48	3.28	3.33					3.26	3.25		V
1648	3096	6.17	3.44	2.32	6.02	5.97	6.07			4.67			4.59	4.69	4.66	4.48	D
1652		4.55	1.20	0.91				4.62						3.36	3.10		
1654		3.19	1.46	1.10				5.19	5.18					5.23	5.08		
1657		5.14	-0.06	0.01													
1663		5.01	1.45	1.20				4.92					4.91	2.87	5.98		
1666		2.79	0.13	0.14				2.92						5.97		3.06	
1670	3121	6.01	0.27	0.25	6.22	6.11	6.32	5.97	5.96					5.34			
1672	3126	5.43	0.24	0.20	5.69	5.66	5.72	5.42	5.32								
1674		4.72	0.52	0.48				4.76					4.70			4.83	
1676	3129	4.82	0.32	0.32	5.20	5.25	5.16	4.86	4.81					4.91			
1679		4.27	-0.20	-0.08				4.34	4.39					4.30			
1689	3151	4.88	0.18	0.19	5.00	4.93	5.08	4.78	4.92					4.67	4.74		
1690		6.67	-0.07	0.02				6.58							6.60		
1696		4.44	-0.09	-0.02				4.54	4.66					4.49		4.46	D
1698	3159	4.45	1.19	0.85	4.70	4.68	4.72	4.64	4.47					4.55			D
1702		3.29	-0.11	-0.01				3.30	3.29					4.55			
1705		4.36	-0.10	-0.01				4.46	4.55					4.21		3.32	D
1708	3171	0.08	0.80	0.60	0.43	0.43	0.43	0.21	0.18					0.24		4.51	D
1715		0.13	-0.03	0.01				0.34	0.32					0.28	0.40	0.36	V
1724	3193	6.42	-0.02	0.05	6.78	6.87	6.68	6.37						6.37			
1726	3195	4.54	1.27	0.98	4.55	4.57	4.53	4.81	4.97					4.68	4.79		
1729	3202	4.71	0.62	0.53	4.83	4.82	4.84	4.85	4.95					4.83	4.85		
1735		3.59	-0.12	-0.02				3.68	3.65					3.62		3.77	
1743		4.83	1.00	0.74				4.91		4.84			4.96	5.02	4.96	4.76	
1748		6.35	-0.11	0.01				6.42	6.40					6.43			
1756		4.29	-0.25	-0.12				4.29	4.28					4.17		4.41	
1761	3250	6.65	-0.08	0.04	6.92	6.95	6.90	6.71	6.71					6.41			
1762		4.71	-0.05	0.05				4.73	4.63					4.71		4.83	D
1763	3251	5.80	-0.13	0.01	6.26	6.18	6.33	5.71	5.75					5.72			
1764		5.69	-0.11	-0.02				5.65						5.51	5.77	4.76	
1765		4.74	-0.16	-0.05				4.65	4.65					4.55			
1770	3259	5.00	-0.15	-0.09	5.21	5.29	5.13	4.99	5.00					4.97	4.93		D
1781		5.70	-0.21	-0.08				5.64	5.64					5.51		5.82	
1784		4.12	0.96	0.72				4.21	4.30					4.26		4.18	

T A B L E 1 (continued)

ES	ED	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
1786	3273	6.32	-0.15	-0.05	6.64	6.57	6.70	6.32	3.49					5.33	6.32	5.39	DV
1788	3275	3.35	-0.17	-0.09				3.44	4.73			4.76		4.78			
1789	3276	4.96	-0.20	-0.08	5.20	5.19	5.21	4.73	4.64					4.78			
1790	3275	1.64	-0.22	-0.09	2.06	2.01	2.05	1.70	1.86			1.64		1.59			
1791	3277	1.65	-0.13	-0.01	2.01	2.01	2.00	1.78	1.90					1.66			
1803	3287	6.15	-0.18	-0.06	6.56	6.51	6.61	6.02		5.98				6.08	5.99		
1806	3300	6.23	-0.05	0.01				6.13		6.12				6.08	6.19		
1810	3300	4.89	-0.14	-0.05	5.05	4.84	5.16	4.83	4.82		4.77			4.84			D
1811	3299	4.59	-0.20	-0.10	4.89	4.79	4.79	4.66	4.73					4.48			
1833	3303	6.75	-0.16	-0.06	7.16	7.19	7.14							4.48			
1820	3313	6.44	-0.17	-0.07	6.80	6.77	6.84	5.37	6.39	2.83				6.35	6.36	2.90	D
1829		2.84	0.82	0.65				2.96	3.03					3.07			
1830		5.78	1.15	0.83	6.12	6.01	6.22	6.06	5.96					6.17	5.69		D
1833	3342	5.78	-0.20	-0.06	6.12	6.01	6.22	5.67	5.55			4.18		5.78			
1839	3351	4.20	-0.13	-0.06	4.48	4.47	4.48	4.32	4.34					4.45			
1840		6.32	-0.19	-0.08				6.24			6.20			6.28			
1842	3355	5.46	-0.17	-0.04	5.75	5.15	5.76	5.52	5.50					5.55			D
1843	3361	4.77	0.35	0.37	4.02	4.92	4.92	4.88	5.00					4.91	4.72		D
1845	3362	4.55	2.06	1.76	4.54	4.42	4.65	4.73	4.57					4.70	4.91		V
1848		6.21	-0.18	-0.06				6.03						6.03	6.03		
1852		2.24	-0.22	-0.08				2.48	2.38					2.51		2.46	V
1855		4.62	-0.26	-0.12	4.64	4.64	4.64	4.64	4.66		4.83			4.51	4.48	4.74	V
1861		5.35	-0.19	-0.05	5.30	5.20	5.33	5.33	5.20					5.38	5.38		D
1862		3.87	1.14	0.82	3.92	3.78	3.92	3.92	3.78	3.99			3.86	3.95	4.05	3.86	D
1863		6.53	-0.10	0.00	6.46			6.46						6.46			
1865		2.57	0.20	0.22				2.69	2.67					2.73	2.64	2.66	V
1868		5.34	-0.18	-0.05	5.37	5.37	5.37	5.37	5.37					5.33	5.22	5.56	V
1871	3388	6.58	-0.16	-0.07	6.80	6.84	6.76	6.42	6.42					6.42	6.42		
1872	3391	5.36	0.05	0.08	5.62	5.54	5.69	5.32	5.33			5.32		5.31	6.18		
1873		6.20	-0.16	-0.05				6.18						6.18			
1876	3393	4.41	-0.15	-0.01	4.68	4.79	4.58	4.53	4.40			4.54		4.65			D
1879	3395	6.71	-0.14	-0.02	7.02	7.06	6.99	2.57	2.57			2.57		2.56			
1886		5.67	-0.24	-0.07	5.70	3.70	3.71	5.58	5.58					5.58			
1887		4.79	-0.25	-0.11				4.67	4.47			4.87		4.67			
1890		6.57	-0.13	-0.06				6.54			6.44			4.68	4.68		D
1891		6.25	-0.15	-0.01				6.28			6.35			6.20	6.20		
1892		4.59	-0.19	-0.08				4.65	4.60					4.68	4.55	4.75	D
1893		6.72	0.00	0.31				6.84	6.58			7.16		6.69			
1895		5.13	0.00	0.22				5.36	5.01			5.68		5.21			
1896		6.70	0.08	0.29				6.85	6.50		7.01	7.01		6.70			D
1897		5.08	-0.11	0.11				5.17	4.90		5.28			5.34			
1898		6.31	-0.13	-0.02				6.29						2.77	6.29	3.08	D
1899		2.77	-0.24	-0.07				2.87	2.97					2.77			
1900		6.40	-0.12	-0.01				6.33			6.33						
1901		5.27	0.23	0.29				5.28	4.95		5.43			5.32	5.33	5.38	V
1903		1.69	-0.18	-0.07				1.75	1.76		1.54			1.74	1.74	1.96	
1905	3414	5.54	0.22	0.21	5.84	5.76	5.92	4.39	5.37					5.34	5.46		
1907	3416	4.09	0.95	0.76	4.20	4.24	4.15	4.39	4.42			4.44		4.32			
1908	3417	5.90	1.60	1.19	6.16	6.11	6.20	6.10			5.99	6.21		6.11			

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gz	Gz1	Gz2	m _{8g}	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
1910	3420	3.03	-0.19	-0.03	3.29	3.29	3.30	3.00	2.92					3.02	5.62		
1911		2.74	-0.22	-0.06				5.62							2.75		
1918		6.06	-0.21	-0.07				2.75							6.41		
1925	3439	6.25	0.84	0.69	6.42	6.45	6.39	6.41						3.84	3.69	3.86	D
1931		3.80	-0.24	-0.08				3.78	3.74								
1934	3445	4.59	-0.11	0.02	4.77	4.75	4.79	4.54	4.50		4.57			4.51	4.57	4.91	D
1937		4.81	0.13	0.15				4.88	4.96					4.77	5.96		
1938	3447	6.04	0.05	0.11	6.30	6.28	6.33	5.96			4.91			4.77			D
1946	3463	4.86	-0.12	-0.01	5.12	5.26	4.97	4.93	4.93					1.89			D
1948		1.77	-0.21	-0.08				1.91	1.89								D
1956		2.64	-0.12	-0.02				2.75	2.72	2.99			2.74	2.55	2.69	2.82	
1963	3486	4.90	1.17	0.88	5.12	5.22	5.01	5.24	5.26					5.22			
1971	3493	5.77	0.03	0.08	5.78	5.82	5.75	5.52	5.42					5.60			
1982		3.60	0.47	0.45	4.70	4.65	4.74	3.80	3.76		3.81			3.86	3.92	3.66	
1995	3543	4.53	0.94	0.73	4.70	4.65	4.74	4.64	4.60					4.80	4.53		
1998		3.55	0.10	0.12				3.67	3.74		3.68			3.50	3.70	3.72	
2004		2.05	-0.18	-0.02				2.20	2.22		2.23			2.20	2.05	2.30	
2010	3560	4.91	-0.07	0.02	5.10	5.14	5.05	4.92	4.83		4.98			4.94	4.91		
2011	3561	4.74	1.62	1.36	4.83	4.95	4.71	4.99	5.20					4.17	4.94		
2012	3564	3.97	1.14	0.82	4.18	4.19	4.16	4.18	4.19					4.18			
2018	3570	6.25	1.75	1.55	6.50	6.45	6.56	6.41						6.41			
2029	3584	5.00	0.05	0.09	5.15	5.17	5.13	4.92	5.03					4.80			
2034	3590	4.59	-0.02	0.04	4.84	4.78	4.90	4.54	4.46		4.46			4.37	4.65		
2035		3.85	0.98	0.86				3.50	3.98		3.90			3.94	3.76		
2040		3.12	1.16	0.85				3.22	2.95	3.54			3.06	3.34	3.10		
2047	3600	4.41	0.59	0.51	4.65	4.71	4.59	4.62	4.65		4.70			4.58	4.55	5.05	V
2056		4.87	-0.15	-0.07				4.89	4.84					4.82	4.72		
2061		0.42	1.84	1.64				0.92	0.91					0.94			
2077	3634	3.72	0.99	0.77	3.92	3.89	3.95	3.88	3.79					3.98	4.67		
2084	3641	4.82	-0.06	0.06	5.02	5.02	5.01	4.90	5.06					4.96			
2085		3.72	0.33	0.33				3.77	3.74		3.67			3.75		3.93	V
2088	3646	1.90	0.03	0.08	2.21	2.23	2.20	2.07	2.07		2.17			1.98			V
2091	3654	4.25	1.72	1.69	4.34	4.37	4.31	4.59	4.47					4.57	4.72		V
2095	3658	2.62	-0.08	0.00	2.87	2.82	2.93	2.71	2.67					2.70	2.77		D
2106		4.36	-0.18	-0.07				4.36	4.08	4.40			4.49	4.34	4.38	4.45	
2113		4.52	1.22	0.93				4.68	4.73					4.77	4.76	4.45	
2120		3.96	1.14	0.82				4.03	4.73					4.14	4.00	3.98	DF
2124	3695	4.13	0.16	0.19	4.36	4.36	4.36	4.19	4.29			4.00		4.14			
2128		4.94	-0.12	-0.03				4.97	4.77					4.78			
2134	3712	4.15	0.87	0.68	4.37	4.40	4.34	4.30	4.33		5.06			4.44	4.14	5.09	
2135	3709	4.63	0.28	0.31	4.80	4.87	4.73	4.71	4.78					4.81	4.60	4.91	
2155		4.67	0.05	0.09				4.67	4.63		4.55			4.81	4.56		
2159	3745	4.42	-0.15	-0.06	4.62	4.63	4.61	4.40	4.37		4.66			4.74	4.20		
2198	3793	4.92	-0.12	-0.02	5.19	5.27	5.11	4.92	5.01		4.94			4.81			
2199	3791	4.48	-0.17	-0.05	4.60	4.62	4.57	4.35	4.21		4.47			4.37			
2209	3811	4.80	0.03	0.07	4.96	4.97	4.96	4.73	4.66					4.77	4.78		C
2219	3824	4.35	1.01	0.80	4.56	4.59	4.52	4.45	4.46					4.47	4.42		
2227		3.06	1.31	0.97				4.03	4.04					4.26	6.50	3.98	
2228	3838	6.52	0.27	0.27	6.94	6.93	6.94	6.46	6.40					6.48	6.50		
2250	3839	6.09	0.90	0.69	6.30	6.31	6.28	6.11	6.40		6.09			6.10	6.13		

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m25	m24,1	m24,4	m34	m44	m45	m46	R	
2238	3850	4.48	0.01	0.06	4.65	4.70	4.61	4.42	4.33			6.33		4.50	6.18			
2240	3854	6.25	0.45	0.47	6.52	6.56	6.49	6.26	4.84	4.47			4.50	5.01	4.66	5.11		
2244		5.01	-0.03	0.02				4.99					4.50	4.56	4.66	4.37		
2256		4.57	1.00	0.73				4.51				5.20		5.01	4.66	5.07		
2261		5.09	0.72	0.61				5.14						4.56	4.66	5.07		
2282		3.02	-0.18	-0.05				3.10	3.09	3.07			3.25	3.03	3.02	3.22		
2286	3918	2.87	1.64	1.57	3.06	3.02	3.11	3.19	3.22					3.16				
2291	3930	5.64	0.24	0.22	5.84	5.74	5.94	5.50	5.36					5.63				
2294		1.97	-0.24	-0.14				1.99	2.01					1.97				
2296		3.85	0.88	0.67				3.98	4.07	4.07			3.84	4.02	4.04	3.87		
2298	3933	4.31	0.20	0.19	4.60	4.58	4.62	4.33	4.40			4.38		4.21	6.43	0.96	D	
2308	3951	6.23	2.34	1.83	6.26	6.36	6.16	6.56		6.49	6.77	0.76		4.16	4.03		V	
2326		-0.75	0.15	0.24	4.42	4.51	4.34	4.06	3.98	5.05				4.88	5.03			
2343	3987	4.14	-0.14	-0.03				4.96	4.98					4.16	4.03			
2344		5.05	-0.18	-0.10				4.96	4.98					4.88	5.03			
2356		3.76	-0.15	-0.01				4.33	4.33	4.64				4.34	4.40	4.57	D	
2361		4.48	-0.17	-0.06	6.04	5.97	6.12	4.48	4.13					4.54	4.40			
2362	4035	5.83	1.00	0.72	4.73	4.62	4.84	5.98	6.27	6.01	5.98		4.60	6.03	6.20			
2385	4040	4.50	0.00	0.10				4.50	4.31		4.61			4.36	4.72			
2387		4.33	-0.24	-0.12				4.35	4.21		4.41			4.37	4.72	4.42		
2392		6.24	1.11	0.75	5.56	5.70	5.42	6.38	6.30					6.47	5.73			
2405	4068	5.29	2.60	1.97				5.87	4.54		5.84			6.04	5.73			
2414		4.54	-0.06	0.04	2.34	2.28	2.41	4.54	4.35		4.70			4.54	4.58			
2421	4089	1.82	0.00	0.06	4.88	4.93	4.83	1.33	2.00		1.91			4.54	4.58			
2427	4094	4.79	1.23	0.90				5.09	5.17					4.92	5.17			
2429		3.92	1.05	0.79				4.14	4.25	4.10	4.71			4.30	4.10	3.97	D	
2443		4.42	1.15	0.86	4.65	4.62	4.61	4.65	4.68	5.07	5.07			4.69	4.61	4.54		
2450		4.81	1.49	1.03	3.18	4.97	4.97	4.97	4.97				3.23	5.04	4.79	4.79		
2451		3.17	-0.11	0.00				3.18	3.18	4.72	4.85			3.17	3.06	3.27	D	
2456		4.66	-0.24	-0.11				4.68	4.57					4.59				
2467	4144	6.37	-0.05	0.07	6.64	6.67	6.62	6.20	6.20					6.20	6.20		D	
2470	4149	4.87	0.08	0.12	5.00	5.04	4.97	4.89	4.68					5.10	4.89			
2473	4153	2.98	1.40	0.96	3.21	3.19	3.24	3.18	3.19					3.18				
2478	4158	4.49	1.16	0.86	4.57	4.60	4.54	4.65	4.62			4.71		3.18				
2484	4172	3.36	0.43	0.39	3.63	3.66	3.60	3.40	3.36					3.45				
2491		-1.46	0.00	0.00				-1.36	1.73			1.40		1.49		1.70		
2506	4193	4.46	1.11	0.79	4.64	4.66	4.61	4.70	4.75		4.56			4.79				
2527	4219	4.55	1.36	1.02	4.72	4.82	4.62	4.75	4.62					4.88				
2538		3.95	-0.23	-0.10				3.78	3.92	3.70			3.90	3.81	3.78	3.60		
2540	4229	3.60	0.10	0.10	3.84	3.77	3.90	3.64	3.74					3.53				
2553		2.92	1.19	0.85				2.83				2.76				2.90		
2560	4252	4.35	0.85	0.65	4.53	4.53	4.53	4.54	4.52					4.55			D	
2564	4258	4.65	0.30	0.32	4.78	4.70	4.87	4.70	4.78					4.61			D	
2571		4.83	-0.21	-0.12				4.66	4.43		4.72			4.65		4.82		
2574		4.08	1.43	1.13				4.25	4.23					4.25	4.27	4.07		
2580		3.92	1.71	1.17				4.12	4.04					4.16	4.11	3.80		
2583		6.75	-0.30	0.28				6.55	6.37			4.17		4.16	4.11	3.80		
2585	4270	4.90	0.03	0.05	5.16	5.16	5.16	4.80	4.74		6.70			6.57	4.78	4.63	D	
2590		4.69	0.36	0.38				4.62	4.45	4.68				4.72	4.78	4.63		
2591		6.32	2.24	1.73				6.00						4.72	4.78	4.63		

T A B L E 1 (continued)

BS	FD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
2596		4.37	-0.06	0.05				4.39	4.46				4.91	4.32		4.86	
2608		4.95	1.69	1.48				4.88				1.72		1.65		1.67	
2618		1.50	-0.21	-0.09				1.63	1.49			3.82		3.92	3.90	3.26	
2646		3.43	1.72	1.32				3.68	3.49		4.96			4.91		4.88	
2648		5.00	-0.20	-0.06				4.89	4.82								
2653		3.01	-0.08	0.01				3.12	3.05		3.98	3.07		3.22		3.12	
2657		4.12	-0.11	-0.01				4.07	4.10				5.48	4.52		4.06	D
2667		5.28	0.66	0.23				5.47				2.14		4.16		4.51	
2693		1.84	0.67	0.51				1.98	1.85					2.17		1.76	
2697	4401	4.42	1.26	0.96		4.59	4.69	4.48	4.63				4.47	4.35			
2701		4.92	1.03	0.79				5.02	5.09	5.00	5.03			5.08		5.07	
2702		4.83	-0.18	-0.07				4.85					4.87	4.94		4.80	
2714		4.15	0.00	0.06				4.09	4.01				4.17	4.10		4.10	
2740		4.49	0.32	0.32				4.47				4.54	4.61	4.47		4.54	
2745		4.65	-0.20	0.01				4.66	4.54			4.90	4.61	4.61		4.74	V
2749		3.82	-0.18	0.02				3.83	3.69			3.99	3.82	3.82		3.82	
2751	4458	5.05	0.08	0.15		5.16	5.19	4.80	4.77				4.88	4.84		4.89	
2762		4.76	-0.10	-0.01				4.88				4.79		3.70	3.66		
2763	4470	3.58	0.12	0.12		3.75	3.63	3.87	3.58				4.85	4.98			
2764		4.78	1.70	1.32				4.82	4.67								
2766		4.60	1.60	1.48				4.77	4.92	2.80		4.86	4.68	4.68		4.63	
2773		2.70	1.62	1.24				2.74	3.65				2.92	2.96		2.53	
2777	4482	3.53	0.34	0.35		3.69	3.66	3.71	3.51			4.92	3.54	3.34		5.09	D
2781		4.95	-0.15	0.00				4.90	4.77			4.45	4.79	4.94		5.09	V
2782		4.40	-0.15	-0.04				4.40	4.31				4.52	4.26		4.68	
2787		4.67	-0.10	0.10				4.68		4.50			4.80	4.60		4.88	
2790		5.11	-0.16	-0.06				5.11		4.77			5.33	5.17		5.23	
2812		4.96	-0.05	0.06				4.87	4.90				4.84	4.84			
2818	4521	4.64	-0.02	-0.01		4.80	4.79	4.81	4.45				4.32	4.44			
2821	4524	3.79	1.04	0.77		3.96	3.96	3.89	4.03				3.86	3.78			
2827		2.44	-0.09	0.07				2.43	2.41		2.30		2.50	2.50		2.52	
2828	4531	4.99	1.01	0.73		5.02	4.90	5.15	5.07				5.12	5.09			
2845	4552	2.89	-0.09	-0.01		3.20	3.12	3.28	3.09				3.11				
2852	4563	4.18	0.32	0.32		4.40	4.43	4.39	4.18				4.21				
2854	4564	4.30	1.43	1.11		4.30	4.24	4.36	4.60				4.58				
2864	4582	4.55	1.29	0.90		4.76	4.72	4.79	4.85			4.76	4.84				
2874		4.34	0.24	0.27				4.80	4.83			4.73	4.93	4.75		4.75	
2878		3.25	1.52	1.21				3.27				2.89	3.60	3.31		3.18	
2881		4.63	0.33	0.67				4.77	4.79	4.70			4.72	4.92		4.64	
2890	4614	1.58	0.04	0.06		1.94	1.94	1.94	1.50				1.53				D
2902		4.99	1.46	1.62				5.06	5.00	5.07			5.02	5.17			
2905	4635	4.06	1.54	1.24		4.18	4.21	4.16	4.22				4.26				
2906		4.45	0.51	0.51				4.52	4.51			4.51	4.54				
2922		4.61	-0.12	-0.03				4.55	4.40			4.47	4.57			4.76	
2930	4665	4.91	0.40	0.39		5.08	5.10	5.05	4.92		5.07		5.03				
2937		4.53	-0.09	-0.02				4.62		4.44			4.67	4.76		4.70	
2943	4678	0.37	0.42	0.42		0.72	0.72	0.72	0.46			0.54	0.47	0.45		4.62	D
2944		4.70	-0.11	0.01				4.64	4.34			4.77	4.67	4.76		4.62	
2946	4679	4.39	0.08	0.18		5.18	5.18	5.18	4.96			4.77	4.67	5.07		4.92	F
2948		3.60	-0.19	-0.04				3.81	3.86			3.76	3.82				D

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
2961	4692	4.85	-0.19	-0.08	5.68	5.66	5.69	4.91	5.87	4.60	5.74	5.13	5.16	4.89	4.77		
2967		5.56	1.64	1.60	5.66	5.66	5.69	5.81	5.87		4.10		5.84	5.79	3.88		
2970	4698	3.93	1.02	0.77	4.38	4.34	4.39	4.07	4.20				4.10	4.10	6.77	6.50	
2973		4.29	1.12	0.92	4.38	4.34	4.39	4.26	4.13				4.40	4.40			
2974		6.56	1.18	0.87				6.64									
2985	4711	3.57	0.92	0.71	3.75	3.80	3.67	3.68	3.61				3.82	3.62			D
2990	4719	1.14	1.00	0.75	1.51	1.51	1.51	1.21	1.12		1.26		1.25	1.25			
2993		4.59	1.65	1.51	5.02	5.01	5.02	4.82	5.04		4.15		4.70	4.70	4.64		
2996		3.95	0.18	0.26	5.02	5.01	5.02	4.10	4.15				3.96	3.96	4.12		
3003	4726	4.87	1.46	1.15	5.02	5.01	5.02	4.10	4.15				5.01	4.98			
3017		3.61	1.73	1.35	3.72	3.72	3.72	3.72	3.72	3.90			3.40	3.95	4.00	3.33	
3034		4.52	-0.05	0.15	4.55	4.55	4.55	4.59	4.68		4.55		4.55	4.55	4.51	4.70	
3045		3.55	1.25	0.88	3.47	3.47	3.47	3.47	3.40		3.41		4.68	3.55	3.51	4.26	
3046		4.71	1.06	0.76	4.64	4.64	4.64	4.64	4.62				4.11	4.55	4.39	4.26	
3055		4.11	-0.18	-0.08	4.25	4.25	4.25	4.25	4.25				4.11	4.39	4.26	5.26	
3064		5.16	0.60	0.52	5.25	5.30	5.20	5.34	5.49		5.34		5.27	4.90	4.90	3.68	
3067	4791	4.98	0.09	0.13	4.92	4.92	4.92	4.92	4.89				5.17	3.87	3.87	4.85	
3080		3.75	1.05	0.81	5.25	5.30	5.20	3.76	4.27				3.72	4.55	4.55	4.85	
3084		4.49	-0.19	-0.08	4.53	4.53	4.53	4.53	4.53				4.67	4.63	4.63	4.85	
3089		4.65	-0.23	-0.13	4.83	4.83	4.83	4.83	4.83				4.81	4.83	4.83	4.85	
3090		4.24	-0.14	-0.02	4.32	4.32	4.32	4.32	4.32				4.28	4.60	4.60	4.36	
3102		4.20	0.72	0.59	4.35	4.35	4.35	4.35	4.26		4.30		4.60	4.60	4.60	4.28	
3113		4.79	0.15	0.20	4.81	4.81	4.81	4.85	4.81	4.97			4.91	4.79	4.84	4.79	
3131		4.61	0.08	0.15	4.64	4.64	4.64	4.64	4.62		4.74		4.56	4.56	4.56	4.79	
3141		4.67	1.49	1.17	4.88	4.88	4.88	4.88	4.88		5.05		4.77	4.77	4.83	4.83	
3145		7.00	0.71	0.60	7.32	7.28	7.35	7.34	7.35				4.88	4.88	4.88	4.83	
3152	4882	4.38	1.25	0.99	4.60	4.61	4.59	4.52	4.56		2.83		2.53	4.48	2.34	2.30	
3173	4912	2.25	-0.27	-0.12	2.27	2.27	2.27	2.27	2.27	2.04			2.53	4.35	4.37	2.84	
3185		2.81	0.45	0.35	2.88	2.88	2.88	2.88	2.88				2.95	2.95	2.95	2.84	
3188		4.32	0.97	0.73	4.41	4.41	4.41	4.41	4.47				4.38	4.38	4.38	4.38	
3192		4.40	-0.15	-0.03	4.34	4.34	4.34	4.34	4.23				4.32	4.32	4.32	4.48	
3206		4.27	-0.24	-0.11	4.79	4.79	4.79	4.79	4.79				4.91	4.79	4.79	4.67	
3207		1.83	-0.25	-0.02	2.22	2.22	2.22	2.22	2.22				2.21	2.22	2.22	2.22	
3211		4.72	0.96	0.73	4.68	4.68	4.68	4.68	4.61				4.74	4.74	4.74	4.82	
3225		4.45	1.62	1.20	4.43	4.43	4.43	4.43	4.43	4.44			4.27	4.52	4.66	4.26	
3226		4.75	0.18	0.24	4.87	4.87	4.87	4.87	4.87				4.85	4.82	4.82	4.20	
3237		4.77	-0.17	0.09	4.77	4.77	4.77	4.77	4.77	4.82			5.00	4.71	4.65	4.71	
3243		4.44	1.17	0.84	4.43	4.43	4.43	4.43	4.43	4.44			4.50	4.44	4.59	4.59	
3249	4988	3.53	1.48	1.12	3.74	3.78	3.70	3.76	3.82		3.65		4.53	3.70	3.85	4.74	
3270		4.45	0.22	0.21	4.21	4.34	4.08	4.43	4.42	4.27			4.53	4.34	4.53	4.47	
3275		4.25	1.55	1.20	4.43	4.43	4.43	4.43	4.42		5.69		4.45	4.45	4.42	5.50	
3279		5.58	0.77	0.64	5.56	5.56	5.56	5.56	5.42	5.14			5.63	5.63	5.01	4.82	
3282		4.83	1.45	1.00	4.94	4.94	4.94	4.94	4.94				4.77	4.96	4.82	4.82	
3294		4.82	-0.15	-0.04	4.90	4.90	4.90	4.90	4.90				4.83	4.83	4.82	4.98	
3306	5062	5.13	0.94	1.25	5.34	5.38	5.29	5.23	5.09				5.36	5.23	5.23	1.74	
3307		1.85	1.27	1.15	1.74	1.74	1.74	1.74	1.74			1.74	1.74	1.74	1.74	4.02	
3314		3.90	-0.02	0.03	3.95	3.95	3.95	3.95	3.85				3.98	3.98	3.98	4.02	
3319	5073	5.50	1.60	1.62	5.78	5.73	5.83	5.75	5.63		5.73		5.86	5.86	5.86	5.86	
3323	5081	0.85	0.85	0.69	3.43	3.45	3.40	3.47	3.45	3.47		3.47	3.47	3.47	3.47	3.50	

T A B L E 1 (continued)

BS	FD	V	B-V	V-R	Gr	Gr1	Gr2	maE	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
3387		6.59	0.68	0.54				6.55									
3391	5151	5.64	0.62	0.52	5.82	5.89	5.75	5.65			6.60	6.45		5.73	6.60		
3403	5159	4.61	1.17	0.89	4.75	4.80	4.70	4.79	4.77				4.91	4.73	4.75	4.83	C
3407	5166	5.01	1.33	0.97				4.87									
	5166	6.75	0.13	0.20	6.94	6.94	6.93										
3410	5170	4.17	0.00	0.04	4.38	4.29	4.46	4.18	4.13		4.14			4.28			
3418	5183	4.43	1.20	0.89	4.58	4.58	4.59	4.54	4.40					4.69			
5185	5185	6.67	0.24	0.25	6.79	6.78	6.80										
5187	5187	6.59	0.95	0.72	6.68	6.68	6.69						4.08	4.07	4.17	4.21	
3426		4.14	0.10	0.15				4.13									
5193	5193	6.39	0.98	0.72	6.54	6.50	6.59	6.48			6.48						
5194	5194	6.61	0.01	0.05	6.78	6.72	6.85										
5195	5195	6.77	0.27	0.26	7.04	7.14	6.93								6.49		
3428	5196	6.44	1.02	0.74	6.70	6.67	6.74	6.40	6.32		6.42			6.32	6.28		
3429	5197	6.30	0.17	0.17	6.56	6.57	6.55			4.14			3.92	4.04	4.10	4.01	
3438		3.98	0.93	0.66				4.04	5.02		4.97		3.71	5.01	5.01	4.91	
3441	5207	4.88	1.07	0.82	4.90	4.97	4.83	4.73	4.75				4.81	4.76	4.67	4.89	
3445	5216	3.83	0.70	0.63	4.57	4.41	4.73	4.32	4.17		4.43			4.77	4.53	4.86	
3447	5199	3.60	-0.18	-0.06	7.07	7.15	6.99	4.70	4.77					4.57	4.59		
	5199	6.85	0.20	0.20													
3449	5207	6.91	0.96	0.71	7.18	7.20	7.17										
3452	5216	4.66	0.02	0.06	4.90	4.97	4.83	4.73	4.75					4.76	4.67		
3454	5222	4.77	0.12	0.21	4.57	4.41	4.73	4.85	4.81					4.77	4.53	4.86	
3459	5222	4.30	-0.20	-0.07	4.57	4.41	4.73	4.32	4.17					4.57	4.59		
3459	5222	4.61	0.84	0.65				4.70	4.77								
3461	5227	3.94	1.08	0.78	4.04	3.97	4.12	4.17	4.27		4.15			4.10	6.21		
3464	5229	6.15	0.94	0.70	6.30	6.33	6.28	6.14	3.69		6.07			6.13	6.21		
3468	5243	3.69	-0.18	-0.08	4.11	4.06	4.16	3.70	3.55				3.72	3.70	3.68	3.85	D
3474	5243	4.02	1.03	0.75	4.11	4.06	4.16	3.70	3.55				3.98	4.05	4.05	4.07	
3477	5243	4.07	0.87	0.63				4.12	4.16					4.26	4.18		
3482	5252	3.38	0.68	0.60	3.57	3.53	3.61	3.48	3.58		3.45			3.43	3.48		D
3484	5252	4.32	0.90	0.68				4.44	4.38					4.44			
3485	5252	1.96	0.04	0.05				2.01					2.00				
3487	5259	3.91	0.00	0.05	4.66	4.61	4.71	4.09	4.31		4.68			4.15	4.15	4.05	D
3492	5259	4.37	-0.05	0.05				4.42	4.31					4.27			
3518		4.01	1.26	0.95				4.19	4.33		4.17			4.15			
3527		2.10	-0.21	-0.08				4.89					5.23	4.28			
3541	5315	6.64	3.56	2.28	6.39	6.46	6.31	3.30	3.33		4.90			3.28	3.30		
3547	5322	3.10	1.00	0.71	3.34	3.36	3.32	4.87	4.80					4.68	4.85	5.11	
3556		4.89	0.10	0.13													
3569	5345	3.14	0.19	0.22	3.40	3.37	3.42	3.12	3.17		4.41			3.07			
3572	5351	4.26	0.13	0.14	4.56	4.66	4.46	4.27	4.26					4.13			
3576	5355	4.76	1.53	1.47	4.96	4.99	4.93	4.99	5.04		5.02			4.94	4.96		
3579	5361	3.97	0.43	0.40	4.12	4.12	4.13	4.09	4.19		4.10			4.02	4.04		
3591		4.45	0.65	0.55				4.42						4.47	4.48	4.37	
3594	5376	3.60	0.00	0.07	3.86	3.85	3.87	3.68	3.70					3.67			
3595	5378	5.46	-0.03	0.02	5.63	5.64	5.62	5.45	5.56		5.41			5.50	5.33		
3612	5403	4.56	1.04	0.75	4.79	4.80	4.78	4.71	4.69					4.67	4.78	3.60	
3614		3.75	1.20	0.82				3.69					3.74				
3616	5411	4.81	0.49	0.45	5.06	5.06	5.05	4.87	4.79		4.87			4.87	4.94		D

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
3619	5415	4.48	0.27	0.27	4.67	4.70	4.64	4.54	4.44					4.60	4.57		
3624	5425	4.67	0.35	0.32	4.80	4.77	4.84	4.74	4.76	4.72	4.76			4.73	4.75		
3628		4.56	1.61	1.34				4.82	4.79					5.00	4.94	4.61	
3634		2.21	1.65	1.54				2.62					2.10	2.37	2.37	2.04	
3654		5.00	0.22	0.20				4.96					5.04	4.97	4.88	4.95	
3662	5462	4.84	0.18	0.25	4.99	4.98	5.00	4.89	4.92		4.76			5.00			
3665	5464	3.88	-0.07	-0.01	4.26	4.19	4.33	3.84	3.93					3.75	3.86	5.04	
3682		4.94	1.11	0.79				4.98		4.94			4.80	4.99	5.11	4.85	
3684		4.62	0.45	0.38				4.70		4.64			4.70	4.68	4.62	4.85	
3685		1.68	0.00	0.07				1.80					1.73			1.87	
3690	5491	3.82	0.06	0.12	3.98	3.98	4.04	3.82	3.82					3.82			D
3705	5508	3.13	1.55	1.23	3.58	3.39	3.56	3.30	3.44	3.17				3.29			
3706		4.81	0.93	0.72				4.94	4.90					4.99		4.92	
3709		4.79	0.94	0.70				4.87	4.89					4.98	4.98	5.04	
3718		4.72	1.61	1.40				4.93	4.93	5.09				4.88	5.06	4.69	
3721	5541	4.46	1.23	0.91	4.66	4.61	4.72	4.61	4.63					4.60	4.60	4.96	
3733		4.68	0.91	0.71				4.90	4.93	4.89			2.59	4.90	4.88	4.96	
3734		2.50	-0.18	-0.04				2.63						2.67		2.67	
3748		1.97	1.45	1.04				2.16	2.02	4.95				2.29		2.33	
3749		4.68	1.13	0.88				4.94	5.02					4.89	4.88		
3751	5563	4.30	1.48	1.13	4.42	4.50	4.34	4.58	4.58	4.73				4.42			C
3757	5571	3.87	0.33	0.34	3.86	3.85	3.87	3.75	3.71					3.80	3.72		
3759		4.51	0.45	0.43				4.78	4.94					4.63			
3765		4.51	1.44	1.01				4.64	4.94	4.70			4.40	4.74	4.78	4.56	
3771	5587	4.57	0.77	0.66	4.80	4.79	4.81	4.57	4.59					4.61	4.51		
3773	5593	4.31	1.54	1.23	4.50	4.54	4.46	4.48	4.39					4.57			
3775	5599	3.18	0.46	0.44	3.49	3.53	3.45	3.26	3.22					3.30	3.25	3.82	D
3786		3.60	0.36	0.36				3.64		3.67			3.53	3.62	3.57		
3787		4.57	0.10	0.16				4.50	4.60					4.40			
3799	5619	4.51	0.00	0.09	4.78	4.71	4.85	4.65	4.57					4.80	4.57		
3800	5620	4.55	0.92	0.71	4.80	4.91	4.69	4.62	4.67					4.53	4.67		
3809	5627	4.81	0.99	0.76	4.98	5.03	4.93	4.99	5.04					5.03	4.89		
3815	5636	5.41	0.77	0.62	5.66	5.66	5.65	5.48	5.47					5.50			
3834	5662	4.68	1.32	1.06	4.90	4.90	4.90	4.78	4.78	4.71				4.86			
3836		4.35	0.17	0.15				4.49			4.25					4.57	
3845		3.91	1.32	0.99				4.10	4.15					4.04			
3849		3.05	-0.15	-0.07				4.96	4.94					5.02	4.91	3.87	
3852	5685	3.52	0.49	0.41	3.88	3.88	3.89	3.76	3.80			3.80		3.69		3.57	
3858		4.78	-0.12	0.02				4.74	4.62			4.87		4.81	4.68	5.05	
3871		4.79	0.50	0.47				4.98	4.93			5.00		5.00			
3873	5720	2.98	0.81	0.65	3.22	3.19	3.24	3.12	3.14					3.11			
3881	5734	3.10	0.62	0.53	5.36	5.29	5.43	5.20	5.34					5.13	5.12		
3888	5744	3.81	0.29	0.34	4.01	3.97	4.05	3.89	3.98	3.85				3.88	3.84		C
3894	5754	4.60	0.03	0.10	4.74	4.76	4.71	4.54	4.43					4.68	4.50		D
3903		4.11	0.92	0.69				4.29	4.30					4.37	4.23	4.08	
3905	5773	3.88	1.22	0.91	4.08	4.16	4.04	4.10	4.14					4.05		4.70	
3912		4.98	1.20	0.93				4.56				4.69	4.45	4.55	4.50	4.70	
3950	5820	4.70	1.60	1.43	4.76	4.74	4.77	4.89	4.97					4.89	5.02	4.78	
3970		4.59	-0.10	-0.01				4.72	4.69					4.79	4.62		
3974	5868	4.49	0.18	0.18	4.71	4.74	4.70	4.47	4.50			4.37		4.50	4.45		

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	G _r	G _r 1	Cr2	m ₀ G	m14	m23	m24,1	m24,4	m34	m44	m45	m46	F
3975	5873	3.53	-0.04	0.09	3.82	3.84	3.81	3.58	3.59		3.54			3.62			F
3980	5877	4.37	1.45	1.13	4.52	4.52	4.52	4.58	4.60		4.60			4.55			F
3981	5881	4.50	-0.04	0.06	4.68	4.67	4.67	4.50	4.51					4.40	4.59		
3982	5885	1.25	-0.31	-0.02	1.73	1.73	1.73	1.34	1.42		1.23			1.34	1.36		
3986	5896	6.59	1.25	1.23	6.60	6.64	6.56										
3994	5904	3.61	1.00	0.77	6.58	6.59	6.57	3.83	3.92		6.41			3.81	3.84	3.76	
3998	5904	6.44	0.46	0.41	6.41	6.41	6.41	6.41						4.29	3.96	4.15	
4023	5934	3.85	0.05	0.02	3.73	3.69	3.78	3.65	3.78				3.96	3.77	3.96		
4031	5934	3.44	0.31	0.31	3.68	3.70	3.65	3.52	3.57					3.57	3.42		
4033	5932	3.45	0.03	0.08													
4039	5941	5.82	0.50	0.48	6.02	6.07	5.96	5.85							5.85		
4054	5956	1.98	0.45	0.45	5.09	5.16	5.02	4.97	4.95					4.86	5.10		
4057	5957	1.98	1.15	0.85	2.43	2.49	2.37	2.30	2.24					2.35			D
4069	5970	3.05	1.59	1.28	3.29	3.29	3.29	3.21	3.12		3.24			3.18	3.30		
4072	5972	4.99	-0.07	0.04	5.20	5.15	5.24	4.92	5.00	4.87	4.92			4.92	4.91		C
4080	6001	4.83	1.12	0.80	4.96	5.01	4.92	4.99					4.88	5.18	4.97	4.93	
4090	6001	4.74	0.25	0.26	4.74	4.74	4.74	4.83	5.07					4.70	4.72		
4092	6001	5.56	1.52	1.25	5.56	5.56	5.56	5.85	6.04					5.86	5.92	5.64	
4094	6018	3.79	1.48	1.11	3.79	3.79	3.79	4.06	4.14					4.03	4.07		D
4100	6018	4.21	0.90	0.69	4.33	4.42	4.29	4.41	4.42					4.40	4.07	3.98	
4104	6038	4.25	1.45	1.10	4.25	4.25	4.25	4.42	4.50	4.44			4.23	4.43	4.49	4.44	
4112	6044	4.84	0.52	0.48	5.12	5.18	5.07	4.84	4.89					4.80	4.82		
4119	6044	5.10	-0.14	-0.03	5.36	5.34	5.39	4.95	4.94		4.96	-5.05		4.86	4.82		
4132	6060	4.75	0.23	0.20	5.02	5.05	4.98	4.84	5.10					4.73	4.69		
4133	6082	3.85	-0.14	-0.05	3.98	3.90	4.05	3.85	3.99		3.57	3.92		3.92			
4141	6069	5.16	0.34	0.33	5.36	5.36	5.36	5.16	5.16	5.90				5.22	5.10		F
4153	6087	5.28	2.88	2.11	4.90	4.97	4.82	4.77	4.76				5.41	5.90	6.01	5.55	
4166	6087	4.72	0.81	0.68	4.90	4.97	4.82	4.77	4.76					4.80			
4167	6118	3.84	0.30	0.25	6.07	6.01	6.12	6.06					3.99	6.28		4.14	V
4195	6118	6.00	2.41	1.74							6.37						
4199	6194	2.76	-0.22	-0.11	2.76	2.76	2.76	3.03					3.01				
4216	6216	2.69	0.90	0.68	2.69	2.69	2.69	2.84					2.81				
4232	6180	3.11	1.24	0.93	3.11	3.11	3.11	3.32	3.26		3.30			3.30			D
4247	6183	3.83	1.04	0.83	3.93	3.96	3.92	3.92	3.92		3.87			3.97			
4248	6183	4.71	-0.05	0.05	4.98	4.98	4.98	4.84	4.90					4.77			
4259	6194	4.32	0.02	0.10	4.47	4.49	4.46	4.32	4.33	4.67				4.30	4.75	4.76	D
4273	6223	4.60	1.05	0.75	6.16	6.22	6.10	6.22	6.34				4.61	4.71	4.75		
4278	6223	6.00	1.99	1.49										6.10			
4287	6249	4.07	1.09	0.80	4.07	4.07	4.07	4.20	4.09					4.26	4.26		
4293	6293	4.39	0.11	0.13	4.39	4.39	4.39	4.56					4.58	4.48	4.56	4.64	
4295	6239	2.37	-0.02	0.06	2.63	2.60	2.66	2.44	2.60					2.57			
4299	6299	4.75	1.62	1.33	4.75	4.75	4.75	4.97	5.00		2.16			5.03			
4300	6245	4.42	0.05	0.06	4.62	4.61	4.62	4.42	4.48		5.00			5.03	4.86		
4301	6249	1.79	1.07	0.81	2.04	2.04	2.04	1.95	1.96	1.95				1.93	1.95		C
4310	6264	4.63	0.33	0.33	4.88	4.88	4.88	4.66	4.74		4.52			4.78	4.62		F
4335	6301	3.01	1.14	0.84	3.26	3.25	3.26	3.15	3.12					3.18	3.15	4.68	
4343	6337	4.48	0.03	0.07	2.92	2.92	2.91	4.52	4.42		4.37			4.63			
4357	6341	3.56	0.12	0.13	3.56	3.56	3.56	3.41	3.47		2.55			2.68	2.53		
4359	6341	3.35	-0.02	0.05	3.58	3.54	3.65	3.41	3.47		3.51			3.44			
4362	6347	4.63	1.66	1.56	4.67	4.65	4.69	4.87	4.89		4.83			4.87	4.88		

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
4915		2.89	-0.12	-0.13	3.10	3.16	3.05	2.90	3.10		2.77		2.87	2.84			D
4914	7087	2.84	-0.10	-0.04	4.78	4.79	4.78	2.80	3.00		2.67		2.77	2.74			D
4920	7102	4.79	1.56	1.55	5.13	5.07	5.19	4.96	5.00				4.97	4.92			D
4931	7125	4.93	0.36	0.37	3.11	3.12	3.10	2.89	4.79		3.13		4.88	5.00			D
4932	7128	2.84	0.94	0.64				2.95	3.00				2.89	2.77			
4940		4.71	-0.14	-0.06				4.96					4.94	4.97			
4942		4.27	-0.19	-0.09				4.40					4.36	4.45			
4949		5.60	1.59	1.97	5.85	5.82	5.88	5.90	6.06				5.74				
4954	7162	4.82	1.45	1.18	4.95	4.96	4.94	4.89	4.89		5.13	5.54	4.90	5.19			
4955		5.19	1.14	0.82				5.26	5.22				5.38	5.10			
4963		4.38	-0.01	0.05				4.44	4.37		4.43		4.22	4.64			D
4979		4.85	0.70	0.57	4.45	4.48	4.42	4.89	4.89				4.82	4.98			
4983	7194	4.26	0.58	0.49	7.06	6.99	7.12	4.32	4.38				4.27	4.88			
5017	7241	4.73	0.30	0.25	4.98	4.96	4.99	4.66	4.72				4.60	4.66			
5019		4.74	0.71	0.58				4.80	4.82				4.76	4.84			
5020		3.00	0.92	0.60				3.33	3.35				3.23	4.76			
5026		5.49	-0.13	-0.08				5.70					5.72	4.84			
5028		2.73	0.03	0.05				2.91					2.98	5.68			
5054	7290	2.06	0.02	-0.04	2.38	2.37	2.39	2.17	2.38			1.96	2.95	2.89			D
5056		0.97	-0.23	-0.09				1.21	1.23		1.31	1.21	1.09	-			V
5062	7294	4.02	0.16	0.17	4.18	4.12	4.23	4.02	4.18				3.85	4.96			
5068		4.75	1.10	0.79				4.89	4.85		4.79		5.02	4.81			
5072	7301	4.98	0.71	0.61	5.25	5.35	5.15	5.21	5.21			5.27	5.01	4.08			D
5089		3.88	1.16	0.84				3.96			3.80		3.95	4.04			
5095		4.69	1.60	1.46				4.83	4.91		4.69		4.90	4.96			
5105	7346	4.94	0.02	0.08	5.15	5.08	5.22	4.93	4.87				4.96	4.96			
5107	7348	3.38	0.12	0.07	3.56	3.55	3.57	3.44	3.53		3.23	4.93	4.96	4.96			
5110	7355	4.08	0.40	0.41	5.11	5.06	5.16	4.96	4.99			3.65	3.52	4.95			
5112	7356	4.70	0.12	0.11	4.96	4.97	4.96	4.83	4.84				4.67	4.95			
5127	7374	4.83	0.23	0.27	5.02	5.01	5.02	4.92	5.00				4.83	4.83			D
5132		2.30	-0.22	-0.15				2.56					2.58	2.54			
5154	7404	4.66	1.63	1.40	4.64	4.70	4.59	4.75	4.83		5.63		4.67	5.64			
5165		5.60	0.81	0.64				5.71	5.78				4.25	4.39			
5168		4.23	0.38	0.33				4.36	4.36		4.47		4.28	4.41			
5185	7438	4.50	0.48	0.41	4.74	4.64	4.83	4.51	4.50			4.55	4.47	3.65			
5190		3.41	-0.22	-0.12				3.53					3.54	3.47			
5191	7444	1.86	-0.19	-0.12	2.26	2.26	2.26	1.91	2.02		1.82		1.88	3.65			
5192		4.19	1.50	2.13				4.40			4.69		4.28	4.47			
5193		2.94	-0.16	0.03				3.32					3.53	3.28			V
5200	7454	4.07	1.52	1.20	4.07	4.01	4.13	4.28	4.11			4.31	4.35	4.39			D
5210		4.32	-0.13	-0.05				4.47			6.77		6.05	4.26			
5214	7469	6.65	0.12	0.08	7.01	6.91	7.11	6.57	6.37				6.57	4.67			
5217		5.89	0.01	0.06				6.06					6.05	6.08			
5219	7478	4.75	1.65	1.54	4.90	4.83	4.96	4.96	4.94		4.92		5.93	4.05			
5221		4.73	-0.14	-0.04				4.76	4.66				4.88	4.70			D
5226	7487	4.66	1.57	1.61	4.78	4.80	4.76	4.77	4.71				4.83	4.76			
5231		2.55	-0.22	-0.14				3.06					2.81	4.76			
5235	7497	2.68	0.58	0.44	3.08	3.16	3.00	2.89	2.89		2.72		2.80	2.81			
5248		3.83	-0.21	-0.13				4.05					4.04	4.05			

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
5249		3.87	-0.20	-0.14				4.17					4.05	4.24	4.30	4.08	
5260		4.34	0.60	0.48				4.39					4.50	4.23	4.24	4.45	
5264	7546	4.26	0.10	0.15		4.50	4.53	4.34	4.36		4.27		4.27	4.32	4.42		
5270	7556	6.19	0.91	0.82		6.42	6.40	6.12		6.19			4.59	6.05	4.43	4.70	
5285		4.36	-0.19	-0.11				4.54						6.45			
5287		3.28	1.12	0.87				3.48	3.51		3.61			3.44	2.34	3.35	
5288		2.66	0.99	0.76				2.64	1.73	2.74			2.19	2.34	2.34	2.23	
5291	7585	3.65	-0.05	-0.03		3.84	3.84	3.64	3.63					3.79	3.62		
5299	7600	5.28	1.58	1.85		5.39	5.31	5.46	5.47		3.50			5.37	5.48		
5304	7614	4.83	0.54	0.44		5.12	5.05	4.82	4.84			4.86		4.77			
5313	7622	5.02	-0.12	-0.08		5.28	5.25	4.90	4.97					4.79	4.93	4.18	
5315		4.21	1.32	1.07				4.31	4.29		4.29			4.30			
5328	7641	4.41	0.20	0.17		4.66	4.59	4.72	4.44		4.50			4.40	4.48		D
5338		4.09	0.51	0.50				4.16	4.23		4.18			4.17		4.06	
5340	7656	-0.05	1.23	0.97		0.24	0.24	0.24	0.03		0.62			0.07			
5343	7658	5.98	0.26	0.23		6.26	6.32	5.84			5.80			5.87			
5350	7670	4.75	0.20	0.15		4.98	4.91	4.78	4.79					4.80	4.75		
5351	7669	4.18	0.08	0.02		4.40	4.26	4.26	4.29					4.23			
5354		3.55	-0.18	-0.10				4.10	4.20				3.91	4.04	4.63	3.80	
5359		4.52	0.13	0.10				4.60	4.56					4.49	4.74	4.74	
5361	7681	4.81	1.06	0.76		4.98	4.90	4.83	4.77					4.80	4.92		
5365	7690	5.41	0.38	0.34		5.59	5.62	5.31	5.23		5.40			5.29	4.17	4.26	
5367		4.05	-0.03	-0.01				4.97	4.86	4.10			4.19	4.15			
5370	7696	4.86	1.23	0.89		5.08	5.13	4.97	4.86		5.04			5.00			
5373	7701	6.33	0.05	0.06		6.47	6.47	5.98	5.94					6.03			
5378		4.42	-0.18	-0.11				4.55		4.44				4.54	4.56	4.59	
5381		4.75	1.31	0.97				4.93	4.90		4.90			4.81	5.16	4.89	
5384	7712	6.27	0.63	0.56		6.45	6.54	6.34	6.32					6.35			
5385		4.56	-0.13	-0.10				4.65						4.60		4.77	
5396		4.35	0.43	0.41				4.49						4.66		4.45	
5404	7746	4.06	0.50	0.42		4.38	4.26	4.06	4.25					4.07	3.86		
5409		4.82	0.74	0.58				4.97	4.89					5.01		5.01	
5429	7784	3.59	1.30	0.92		3.75	3.71	3.78	3.64					3.67	4.03		
5430	7786	4.25	1.44	1.05		4.37	4.46	4.37	4.29					4.54	4.29		
5435	7790	3.02	0.19	0.14		3.34	3.31	3.00	3.10		3.13			2.82	2.97		
5440		2.31	-0.19	-0.10				2.65						2.84	2.55	2.68	
5447	7804	4.47	0.37	0.34		4.70	4.67	4.48	4.49					4.55	4.43		
5453		4.05	-0.15	-0.09				4.14						4.04		4.24	
5463		3.19	0.24	0.23				3.41						3.37		3.45	
5469		2.50	-0.20	-0.09				2.89						2.46	3.13	2.63	
5471		4.00	-0.17	-0.11				4.09		3.94				4.17	4.00	4.27	
5475	7837	4.54	-0.04	0.07		4.61	4.54	4.54	4.59					4.49	4.09		D
5477	7840	3.78	0.05	0.02		4.04	4.02	3.86	3.84					3.88			D
5485		4.05	1.35	1.01				4.13		4.04				4.41	4.34	4.08	
5487		3.88	0.38	0.40				3.95	3.92		4.03			3.84		4.01	
5489		4.92	0.01	0.06				5.00		4.90				5.01	4.98	5.14	
5490	7861	4.81	1.66	1.49		4.91	4.91	4.93	4.93					4.93	4.98		PV
5492	7862	6.25	0.41	0.37		6.47	6.43	6.17	6.23					6.07	6.19		C
5502	7868	4.60	0.98	0.73		4.84	4.81	4.69	4.81	6.19				4.57			
5505	7869	2.37	0.97	0.75		2.66	2.57	2.55	2.56					2.62	2.59		D

T A B L E 1 (continued)

BS	FD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
5511	7877	3.73	-0.01	0.07	4.00	3.94	4.05	3.76	3.72					3.80			
5526		4.41	1.40	1.07				4.63	4.96		4.36			4.61	4.73	4.47	
5528		4.33	-0.14	-0.05				4.49					4.43	4.54	4.42	4.58	
5530		5.16	0.41	0.38				5.33	5.30		5.22			5.10	5.38	3.08	
5531		2.75	0.15	0.14				2.90	3.02		2.75			2.96	2.68		
5544	7921	4.54	0.77	0.63	4.81	4.78	4.84	4.64	4.60		4.65			4.67			D
5565	7954	2.08	1.47	1.11	2.26	2.24	2.27	2.24	2.13	2.24	2.24			2.31	2.29		
5568		5.71	1.11	0.99				5.76	5.89		5.74			5.64			
5570		4.49	0.32	0.32				4.59	4.55				2.74	2.68	2.77	3.04	
5571		2.68	-0.22	-0.10				2.81									
5576		3.13	-0.20	-0.08				3.35					3.36	3.36	3.22	3.46	V
5586		4.93	0.00	0.08				4.84	4.91					4.76	4.83		V
5589	7994	4.59	1.59	1.86	4.74	4.73	4.75	4.86	4.84	4.88	4.86			4.87	4.83		
5600	8009	4.82	1.50	1.19	5.04	5.04	5.04	4.93	4.86					5.00			
5601	8010	4.40	1.04	0.81	4.64	4.61	4.66	4.62	4.56					4.67			
5602	8013	3.50	0.97	0.65	3.70	3.71	3.69	3.63	3.62		3.66			3.53	3.75	3.30	D
5603		3.27	1.71	1.53				3.41	3.25				3.20	3.62		4.20	
5605	8032	3.89	-0.14	-0.10	4.64	4.58	4.70	4.02	4.46				3.84	4.70	4.84	6.11	
5616		4.55	1.25	0.93				4.67					6.01	5.89			
5625		5.85	-0.12	-0.07				6.00									
5626		4.05	-0.18	-0.08				4.39					4.34	4.41		4.42	D
5634	8055	4.93	0.43	0.40	5.24	5.17	5.30	5.03	5.03				3.98	5.05		3.95	D
5646		3.70	-0.03	-0.05				3.97					4.97	4.79	5.01	5.01	
5651		4.82	-0.17	-0.10				4.92	4.87		4.36	5.02		4.37	4.53	4.79	
5652		4.54	-0.08	-0.04				4.66						4.37			
5660		4.91	0.37	0.36				4.95		4.84			5.01	4.89	4.96	5.06	
5681	8127	3.09	0.95	0.73	3.59	3.59	3.59	3.54	3.50				4.18	3.57	4.59	4.53	D
5683		4.27	-0.09	-0.02				4.36						2.66	2.59	2.84	
5685		2.61	-0.11	-0.04				2.74	2.74		2.85		4.37	4.44		4.42	
5686		4.33	1.10	0.81				4.43	4.69		4.21						
5694	8144	5.06	0.54	0.41	5.17	5.14	5.20	5.18	5.12					5.21	5.20	3.51	
5695		3.22	-0.22	-0.11				3.43					3.37	3.40	3.50	3.61	
5705		3.56	1.54	1.19				3.59		3.54			3.28	3.81	3.72	3.68	D
5708		3.37	-0.18	-0.11				3.74		4.54			3.56	3.97	4.60	4.89	
5712		4.54	-0.15	-0.06				4.69					4.69	4.75			
5721		6.12	0.26	0.24				6.10	6.09		6.13			6.01			D
5727	8182	4.98	0.58	0.48	5.24	5.18	5.29	5.05	4.98					5.07	5.13		D
5731	8189	4.32	0.31	0.30	4.60	4.56	4.65	4.47	4.52		4.51			4.37			D
5732	8193	3.05	0.05	0.08	3.34	3.34	3.34	3.14	3.18					3.10	3.16	5.78	C
5736		5.43	-0.15	-0.09				5.52		3.11			5.60	5.32	5.46		
5744	8216	3.29	1.16	0.78	3.52	3.54	3.49	3.47	3.35					3.52	3.53		C
5747	8223	3.68	0.29	0.18	3.90	3.77	4.04	3.72	3.79					3.65			
5763	8253	5.02	1.59	1.27	5.13	5.12	5.15	5.15	5.09		5.17			5.20			
5764		5.50	-0.14	-0.09				5.59	5.41		5.67			5.57	5.70		D
5774	8260	5.02	0.07	0.15	5.21	5.21	5.21	4.98	5.04					4.98	4.93		
5776		2.78	-0.20	-0.14				2.95			4.74		2.96	2.84	2.94	3.07	D
5777		4.62	1.01	0.77	4.44	4.38	4.50	4.83	4.86					4.81	4.72	4.72	
5778	8263	4.13	-0.13	-0.05				4.17	4.27					4.07			
5780		5.18	-0.09	-0.04				5.15	4.95		5.22			5.11	5.20	5.25	D
5781		4.54	-0.18	-0.15				4.84					4.76	4.95	4.80		

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
5787		3.91	1.02	0.71				4.02	4.01		4.06	4.13		4.10		3.78	D
5788	8268	3.80	0.26	0.22	4.08	4.07	4.08	3.85	3.96					3.74			V
5793	8269	2.24	-0.02	0.03	2.58	2.55	2.61	2.31	2.37					2.25			
5794		3.57	1.39	1.00				3.78	3.93			3.55	4.04	3.85	3.93	3.64	
5797		4.53	1.43	1.05				4.27	4.00					4.29	4.04	4.37	
5812		3.65	-0.18	-0.11				3.80	3.91			3.67		3.80		3.80	
5820		4.67	1.00	0.68				4.63	4.58	4.50		4.91	4.44	4.64	4.82	4.79	
5824		4.96	1.33	0.96				5.06	5.22			4.91	4.51	5.07	5.04	5.04	
5825		4.64	0.40	0.35	6.01	6.00	6.02	4.69	5.74					4.76	4.74	4.75	
5830	8310	5.75	0.36	0.33				5.78	5.74					5.80	5.80	5.80	
5838		4.72	1.58	1.28				4.96	4.97		4.69	5.39	4.75	4.97		4.80	
5839		4.75	-0.14	-0.10				4.82	4.82	4.72				4.79	4.82	5.00	
5840		6.01	0.90	0.69	6.25	6.18	6.32	5.97	5.84		4.50	4.48	4.75	6.07	6.01		D
5842	8330	4.53	0.05	0.04	4.82	4.74	4.89	4.90	4.55					4.44			
5843	8329	5.53	0.04	0.05	5.50	5.53	5.48	5.26	5.15			5.35		5.30			
5849	8344	3.85	-0.01	-0.03	3.98	3.91	4.05	3.93	4.18			5.66		3.68			D
5854	8351	2.64	1.17	0.81	2.88	2.90	2.87	2.75	2.71					2.79			
5859	8361	5.58	0.04	0.04	5.95	5.94	5.96	5.56						5.47			
5867	8367	3.67	0.06	0.06	3.84	3.78	3.91	3.74	3.84					3.65			P
5868	8368	4.43	0.60	0.51	4.62	4.62	4.62	4.42	4.35					4.49			
5879	8394	4.09	1.62	1.25	4.10	4.16	4.03	4.28	4.25		4.32			4.27			
5881		3.53	-0.04	-0.01	3.63	3.48	3.53	3.48	3.48				4.20	4.27		3.80	
5883		3.95	-0.04	-0.02	4.11	4.01	4.01	4.11	4.01	4.04				4.03	4.06	4.32	
5885		4.68	-0.06	0.01	5.42	5.45	5.38	4.77	4.79			4.83		4.80	4.66	4.79	
5888	8403	5.23	1.02	0.77	5.42	5.45	5.38	5.33	5.19					5.35	5.46		
5889	8405	4.63	0.80	0.63	4.78	4.62	4.93	4.73	4.56		3.80			4.80	4.84		
5892	8407	3.70	0.16	0.08	3.96	3.96	3.96	3.75	3.67				3.09	3.79		2.98	
5897		2.85	0.29	0.32	3.04			3.04						4.97			
5899	8409	4.78	1.54	1.22	4.89	4.85	4.93	4.88	4.78					4.80			
5901	8414	4.82	1.00	0.76	5.03	5.02	5.04	4.77	4.74					4.80			
5902		5.03	-0.01	0.01				5.06	5.04		5.04	5.18		5.09	4.93		
5903	8417	4.32	0.04	0.06	4.52	4.57	4.48	4.34	4.49					4.16	4.36		D
5904		4.59	-0.06	-0.02				4.66	4.74			4.64	4.72	4.55			
5906		5.23	-0.02	0.01				5.44	5.58			5.38		5.35			
5907		5.43	-0.04	0.01				5.36	5.38			5.38		5.31			
5908		4.16	1.01	0.72				4.34	4.31					4.36			
5914	8427	4.62	0.57	0.48	4.78	4.75	4.81	4.61	4.47			6.02		4.70	4.70		D
5915		5.93	-0.02	0.02	5.57	5.63	5.50	5.90	6.05		5.65			5.89	5.78		
5924	8435	5.44	1.59	1.26				4.02	4.01			4.07		4.00		3.98	
5928		3.86	-0.20	-0.11													
5932	8439	5.38	1.64	1.49	5.35	5.50	5.20	5.54	5.47					5.60			
5933	8442	3.86	0.48	0.49				3.86	4.00		3.99			3.77	3.67		
5941		4.87	-0.10	-0.04				4.80	4.68					4.68	4.57		
5944		2.91	-0.20	-0.09				3.00	3.08		2.95			2.98		2.98	
5947	8450	4.15	1.23	0.89	4.30	4.25	4.34	4.22	4.13		4.26			4.28			D
5948		3.41	-0.22	-0.14				3.61		3.54			3.77	3.60	3.37	3.78	D
5953		2.32	-0.12	-0.05				2.54	2.52		2.47			2.49	2.71	2.52	
5960	8462	4.35	0.26	0.23	5.19	5.17	5.21	4.96	5.02		4.96		4.66	4.90		4.82	
5962		4.65	0.92	0.67				4.74					5.10	5.00	4.77	4.82	
5967		4.89	-0.14	-0.07				4.97		4.76						5.24	

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
5971	8479	4.98	-0.07	0.01	5.25	5.19	5.31	4.91	5.09					4.73			
5972	8481	4.85	0.07	0.10	5.06	5.09	5.02	4.82	4.99					4.66			
5977		4.17	0.47	0.37				4.16	4.10		4.17		4.78	4.20	4.72	4.27	
5980		4.72	0.23	0.20				4.84	4.70					4.57		5.01	
5982	8493	4.76	-0.11	0.02	4.98	4.95	5.02	4.64	4.70					4.70			
5984		2.59	-0.08	-0.02				2.76	2.91		2.66			2.70		2.88	D
5986	8496	4.03	0.52	0.45	4.24	4.25	4.23	4.11	4.15	4.12				4.06			C
5987		4.23	-0.18	-0.10				4.33	4.33	4.27			4.42	4.33	4.11	4.47	
5993		3.97	-0.05	0.06				4.13	4.10		4.01			4.02	4.14	4.22	
5997		4.33	0.84	0.65				4.58	4.57		4.37	4.94		4.44	4.28	4.47	
6018	8541	4.76	1.01	0.75	4.98	4.96	4.99	4.94	5.20					4.70			
6023	8543	4.27	-0.07	0.00	4.46	4.49	4.41	4.26	4.22					4.19	4.37		
6027		4.01	0.03	0.11				4.29	4.30		4.26	4.60		4.24	4.04		D
6028		4.59	-0.16	-0.05				4.70	4.69		4.66	4.66		4.62		4.81	
6031		4.93	0.09	0.12				4.91	4.81		4.84			5.08			
6056		2.75	1.59	1.29				3.03	2.77		3.13	3.13		3.16	3.07		
6070		4.77	0.02	0.08				4.87	4.96					4.84	4.76	5.08	
6072		4.02	1.08	0.78				4.14					4.19	4.76	4.09		
6074	8605	5.78	0.07	0.07	5.98	6.02	5.94	5.73	5.80					5.63			
6075		3.23	0.98	0.70				3.34	3.37		3.13			3.40		3.48	
6076		6.28	1.07	0.83				6.38			6.38			6.51	6.24		
6081		4.57	0.84	0.87				4.76	4.70					4.78		4.65	
6084		2.88	0.13	0.20				3.08	2.99				3.02	3.10	3.03	3.15	V
6092	8627	3.90	-0.15	-0.09	4.17	4.18	4.16	3.91	3.87					3.96	3.89		
6093	8631	4.82	0.34	0.31	5.01	5.05	4.97	4.80	4.76				4.92	4.72			
6095	8635	3.76	0.27	0.29	3.97	4.00	3.94	3.79	3.83					3.72			
6098		4.91	0.55	0.54				4.93	4.72				4.99	4.93		4.87	
6103	8641	4.85	0.97	0.73	5.01	5.00	5.02	4.72	4.50					4.65		4.57	
6104		4.50	1.03	0.78				4.59	4.57		4.56	4.79		4.60		4.84	D
6112		4.63	0.22	0.36				4.76	4.82					4.60			
6115		4.47	-0.07	0.04				4.71					4.67	4.44		4.75	
6117	8662	4.58	-0.01	0.07	4.76	4.76	4.75	4.53	4.69		4.47	4.47		4.44			
6118		4.43	0.28	0.46				4.85	5.03		5.11	5.11		4.72		4.54	V
6129		4.63	0.16	0.16	2.99	2.98	3.00	4.68	4.60					4.56	2.88	4.89	C
6132	8665	2.74	0.91	0.61				2.89	2.82	2.87				2.98			
6134		0.91	1.84	1.55				1.22	1.06					1.44	1.34	0.92	V
6141		4.79	-0.07	-0.06	4.76	4.76	4.75	4.53	4.64		4.94	4.94		4.75		5.12	
6143		4.23	-0.16	-0.06				4.33	4.33	4.14			4.92	4.30	4.28	4.49	V
6146	8709	5.01	1.52	2.52	5.07	5.18	4.96	5.02	5.08				4.46	4.97			
6147		4.27	0.92	0.65				4.40	4.44					4.41		4.34	V
6148	8713	2.77	0.94	0.64	3.01	3.00	3.02	2.81	2.76					2.86			D
6149	8712	3.83	0.01	-0.01	3.98	3.84	4.13	3.85	3.97		3.79	3.79		3.78		4.59	
6153		4.43	0.11	0.13				4.57	4.66		4.66	4.66		4.37			
6159	8732	4.85	1.49	1.20	4.93	4.99	4.87	4.92	5.00					4.85			
6161	8734	5.01	-0.06	0.05	5.18	5.19	5.17	4.98	5.03	4.95				4.96	5.00		C
6165		2.81	-0.25	-0.12				2.91	2.90		2.91	2.91		2.85	2.78	3.10	
6166	8747	4.16	1.57	1.20	4.46	4.47	4.44	4.25	4.25	4.24			4.08	4.50	4.41	4.28	
6168		4.20	-0.01	0.03				4.25	4.25					4.32	4.19		
6171		5.74	0.81	0.61				5.87	5.84		6.12	5.60		5.92			
6175		2.56	0.02	0.10				2.70	2.84		2.48	2.74		2.64		2.80	

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
6212	8803	2.81	0.65	0.51	3.16	3.17	3.16	3.00	3.09					2.92			D
6220	8817	3.50	0.92	0.67	3.76	3.74	3.77	3.61	3.69					3.57	3.56		
6227	8818	6.47	0.54	0.44	6.76	6.76	6.75	4.88	4.93					4.84			
6241	8845	4.84	0.59	0.55	5.04	5.04	5.04	2.36	2.15	2.53			2.29	4.84	2.42	2.34	
		2.29	1.16	0.86										2.44			
6243		4.66	0.47	0.45				4.75	4.68		4.64	4.77		4.78	4.67	4.82	
6247	3.03	-0.22	-0.12	-0.13				3.09	3.09	2.57			3.26	3.19	3.09	3.34	V
6252	3.57	-0.21	-0.13					3.64	5.00	3.24			3.74	3.71	3.69	3.83	
6254	8870	4.82	0.09	0.10	5.04	5.02	5.07	4.86	5.00					4.83	4.74		
6271	3.59	1.36	1.12					3.75					3.53	3.98	3.86	3.62	
6281	4.38	-0.08	-0.09		4.56	4.50	4.61	4.29	4.41		4.16			4.31			
6292	8910	6.08	0.92	0.70	6.30	6.25	6.34	6.33			6.33						
6299	8926	3.20	1.16	0.84	3.36	3.37	3.34	3.42	3.37					3.48			
6313	8945	4.90	0.48	0.45	4.95	5.03	4.87	4.82	4.68					4.91	4.88		V
6322	8955	4.23	0.90	0.70	4.48	4.48	4.48	4.40	4.47		4.32			4.40			
6324	8956	3.92	-0.01	-0.01	4.16	4.24	4.09	3.92	4.04					3.80	4.87	5.07	
6334	4.87	0.26	0.28		5.12	5.11	5.13	5.10	5.11	4.65			4.98	5.10			
6337	9082	4.98	1.60	1.44	5.02	5.03	5.02	4.91	4.88		4.95			4.91			
6355	9010	4.91	0.12	0.12	5.02	5.03	5.02	2.63	2.62		2.45			2.60			D
6378	2.42	0.05	0.03														
6380	3.34	0.40	0.36		3.45	3.45	3.44	3.44	3.27	3.21			3.37	3.50	3.32	3.55	C
6396	9074	3.17	-0.11	-0.06	3.45	3.45	3.44	4.56	4.72			4.53		3.22	3.20		D
6401	4.32	0.86	0.70					3.48	3.59					4.48	4.64	4.44	D
6406	3.06	1.45	2.10		3.46	3.41	3.49	3.16	3.26		3.14	3.19		3.57	3.18		DV
6410	3.13	0.08	0.05											3.05			
6415	4.72	1.15	0.80		4.82	4.74	4.81	4.82	4.95				5.54	4.77	4.82	4.76	D
6416	5.48	0.80	0.72		5.58	5.34	5.29	5.58	3.36	5.87				3.31	3.40	5.62	
6418	3.16	1.44	0.96		3.32	3.34	3.29	5.89					5.85	5.93	5.94	5.86	V
6426	5.91	1.04	0.94		5.12	5.33	4.90							4.67			
6431	4.78	-0.15	-0.05		4.78	4.74	4.81	4.80	4.94		4.39			4.49			
6436	4.66	0.05	0.09		4.46	4.41	4.41	4.46	4.51					4.34	4.30	4.43	
6445	4.31	0.03	0.06		4.35	4.38		4.35	4.38					4.22			
6446	3.26	-0.23	-0.12		3.37	3.44		3.37	3.44				3.48	3.21			
6453	7.05	0.60	0.55		7.20	7.18	7.22										
6484	9184	4.17	0.00	0.02	4.33	4.34	4.32	4.14	4.14					4.05	4.23	4.36	D
6486	4.16	0.28	0.29		4.28	4.47	4.32	4.28	4.47			4.39		4.10	4.08	4.36	
6492	4.27	0.40	0.33		4.37	4.38		4.37	4.38			4.58	4.31	4.22	4.29	4.43	
6493	4.54	0.41	0.38		4.61	4.62		4.61	4.62		4.60			4.45	4.69	4.67	
6498	9198	4.33	1.50	1.10	4.40	4.36	4.44	4.44	4.42			4.50		4.39			
6508	2.68	-0.23	-0.14		2.80	2.84	2.70	2.80	2.84				2.84	2.72	2.81	2.88	
6510	2.95	-0.17	-0.10		2.97			2.97					2.86	4.97	4.79	3.08	
6519	4.81	0.00	0.07		4.88	4.88		4.89	4.88		4.90			4.50	4.65	4.96	
6526	4.41	1.44	1.04		4.62	4.66	4.57	4.48	4.29				1.79	1.79	1.42	1.93	
6527	1.63	-0.22	-0.17		1.71	1.68	1.64	1.71	1.68					2.95	3.06		
6536	9251	2.78	1.00	0.68	3.01	3.03	2.99	2.99	2.97				4.54	2.95	3.06	4.72	
6537	4.59	-0.02	-0.01		4.63			4.63					4.54	4.46	4.38	4.35	
6546	4.29	1.09	0.75		4.34			4.34		4.31			4.19	4.46	4.38	4.35	
6553	1.87	0.40	0.35		2.04			2.04					1.99	2.08	2.02	2.05	
6554	4.88	0.26	0.24		4.98	5.25	5.10	4.98	4.86		5.03			5.13	4.88		

T A B L E 1 (continued)

BS	ID	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
6555	9274	4.88	0.27	0.24	5.16	5.04	5.28	4.95	4.75			4.99		5.10	4.95		
6556	9275	2.07	0.15	0.14	2.54	2.52	2.57	2.14	2.17		3.70			2.10		3.67	
6561		3.52	0.24	0.20				3.64	3.67				4.85	3.52	4.60	4.82	
6567		4.63	0.11	0.18				4.65	4.73					4.45	4.60	4.82	
6569		4.77	0.40	0.29				4.84						4.45	4.82	4.82	
6580		2.41	-0.21	-0.08				2.51		2.18			2.59	2.60	2.45	2.75	
6581		4.24	0.08	0.08				4.39	4.41					4.32	4.35	4.48	
6588	9334	3.80	-0.18	-0.10	4.03	4.01	4.04	3.79	3.92		6.56			3.85	3.61		
6592	9340	6.36	1.20	0.92	6.52	6.44	6.59	6.46				4.88		6.36	4.84	4.96	
6595		4.87	0.47	0.41				4.89	4.98					4.78	4.84		
6596	9345	4.80	0.43	0.41	5.05	5.01	5.09	4.87	4.86	4.84				4.88	4.90		C
6603	9354	2.77	1.17	0.82	3.06	3.04	3.07	2.94	2.90					2.99			
6623	9394	3.42	0.75	0.53	3.62	3.65	3.59	3.48	3.49			3.67		3.47			
6629	9399	3.75	0.04	0.04	4.10	4.19	4.00	3.74	3.82					3.74	4.99		C
6636	9406	4.58	0.43	0.38	4.93	4.82	5.04	4.90	4.84	4.93				4.83	4.99		
6685	9492	5.45	0.34	0.32	5.72	5.73	5.71	5.48	5.63					5.33			
6688	9495	3.75	1.18	0.83	3.95	3.96	3.94	3.90	3.93					3.88			
6695	9507	3.87	1.35	0.90	3.95	3.97	3.92	3.50	3.46		3.63			3.98	3.46		
6698		3.34	0.99	0.71				3.50	3.46			4.93		3.40	4.80		
6700		4.75	-0.05	0.05				4.76	4.60					4.71			
6703	9523	3.70	0.94	0.69	3.88	3.90	3.87	3.82	3.91					3.74			
6705	9528	2.22	1.52	1.14	2.47	2.55	2.40	2.42	2.35					2.48			
6707	9534	4.41	0.39	0.40	4.72	4.74	4.69	4.48	4.63					4.33		4.76	
6710		4.62	0.39	0.33				4.60	4.46			4.77		4.58			
6712	9543	4.60	-0.02	0.13	4.94	4.87	5.01	4.81	4.83					4.82			
6713	9548	4.68	1.27	0.87	4.72	4.70	4.75	4.71	4.53			4.84		4.76			
6714	9550	3.97	0.02	0.10	4.18	4.09	4.27	3.92	4.00			4.52		3.90			
6723	9564	4.42	0.04	0.07	4.54	4.52	4.56	4.44	4.42			6.16		4.39		6.17	
6736		5.97	0.00	0.25				5.86	5.66				3.02	5.77	3.15	3.12	
6746		2.99	1.01	0.73				3.07	3.05	3.07				3.02			
6752	9606	4.03	0.86	0.65	4.12	4.06	4.17	4.07	4.11			4.02		4.06	4.10	4.75	D
6766		4.35	0.95	0.66				4.56	4.69			4.46		4.88	4.73		
6770	9638	4.63	0.97	0.69	4.81	4.81	4.81	4.73	4.82			4.72		4.63			
6771	9639	3.73	0.12	0.14	4.00	4.06	3.94	3.73	3.85			3.65		3.70			
6779	9655	3.83	-0.02	0.03	4.06	4.09	4.04	3.83	3.99					3.67			
6783		4.53	1.01	0.70				4.60	4.48			4.54		4.16	4.66		
6787	9665	4.35	-0.15	-0.06	4.60	4.71	4.49	4.32	4.48					4.16			
6789	9667	4.36	0.02	0.05	4.68	4.68	4.68	4.44	4.34	4.45				4.33			
6806	9691	6.40	0.87	0.77	6.56	6.61	6.51	6.40				4.06		6.40	4.06		V
6812		3.85	0.22	0.27				4.01	4.08					3.90			
6832		3.11	1.56	1.21				3.16	2.97	3.17			2.96	3.38	3.12		
6842		4.63	1.66	1.21				4.69	4.71			4.61		4.74	3.58	3.12	
6859		2.70	1.38	1.00				2.84	2.83			2.87	2.69	2.98	2.84		
6866	9799	4.84	0.91	0.69	4.82	4.86	4.77	4.92	4.97			4.93		4.96	4.82		
6868	9802	4.96	1.58	1.34	5.03	5.08	4.98	4.98	4.81			5.05		5.07			
6869		3.25	0.94	0.70				3.42	3.35			3.43		3.48	3.26		
6872	9803	4.34	1.17	0.86	4.51	4.52	4.50	4.34	4.37					4.30	1.90	2.04	
6879		1.85	-0.03	0.00				1.95	2.12	1.90			1.93	1.81	1.90	2.04	
6884		4.68	0.94	0.72	4.06	4.14	3.99	4.83	4.83	4.79				4.74	4.89		
6895	9841	3.84	1.18	0.85	4.06	4.14	3.99	3.92	3.92					3.91			

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
6896		4.81	1.30	1.10				4.96	4.87		5.00			5.01		4.73	R
6897		3.51	-0.17	-0.13				3.76						3.93	3.60	3.80	D
6913		2.81	1.04	0.75				2.94	3.06		2.86		3.69	2.90			
6917	9869	5.83	0.07	0.08	5.86	5.82	5.91	5.71	5.83		5.66			5.63			VD
6918	9868	5.21	0.50	0.49	5.30	5.08	5.53	5.33	5.21		5.63			5.14			
6920	9870	4.22	-0.10	-0.04	4.54	4.50	4.59	4.24	4.21	4.19				4.26	4.28		D
6923	9874	4.59	0.08	0.05	5.26	5.25	5.26	4.85	4.83					4.95	4.78		D
6927	9881	3.58	0.49	0.44	3.75	3.81	3.69	3.69	3.63	3.63				3.67	3.74		C
6930		4.71	0.07	0.08	4.73	4.71	4.71	4.71	4.71		4.63			4.85	5.00		C
6945	9901	4.82	1.19	0.86	5.00	4.89	5.10	4.99	4.98	4.98				4.99			
6951		4.64	1.02	0.69				4.69				4.10	4.41	4.84	4.80	4.70	
6973		3.83	1.34	0.97				4.06	4.01					4.07			
6978	9958	4.80	0.61	0.53	5.04	5.00	5.07	4.83	4.83				5.07			5.81	
6993		5.74	0.06	0.07	0.38	0.38	0.38	5.80	5.78				5.81				
7001	10002	0.03	0.00	-0.04				0.14	0.19				0.10				
7020		4.72	0.35	0.30				4.74	4.75	4.54	4.69		4.91	4.72	4.60	4.96	V
7029		4.87	-0.18	-0.14				4.82						4.86	4.75	5.05	
7039		3.16	-0.11	-0.01				3.50	3.33			3.41		3.16		5.53	
7056	10103	4.36	0.19	0.15	4.73	4.82	4.64	4.29	4.34				4.24	5.64	5.66		
7059		5.64	0.14	0.13				5.68	5.75								
7061	10106	4.19	0.46	0.39	4.44	4.49	4.40	4.26	4.25					4.25			
7063		4.22	1.09	0.79				4.47	4.35		4.52	4.52		4.48		4.47	
7064	10113	4.84	1.20	0.88	5.10	5.09	5.11	4.86	4.86				4.97	4.26			
7069	10118	4.36	0.12	0.09	4.42	4.29	4.54	4.37	4.52				4.20	4.38			
7116		4.83	1.40	1.01				4.96	5.02			5.09		4.86	5.00	4.84	
7120		4.98	1.32	0.94				5.04	5.15			4.99		5.03	5.06	4.97	
7121		2.05	-0.22	-0.11				2.14	2.30			2.10		2.02			
7125	10196	4.87	1.19	0.90	4.78	4.80	4.77	4.78	4.64				4.80	4.89			D
7133	10212	4.60	0.78	0.64	4.71	4.79	4.63	4.56	4.55				4.58				
7137	10217	4.93	0.90	0.68	5.16	5.16	5.16	4.97	4.94				5.00				
7139	10222	4.30	1.67	1.78	4.37	4.52	4.22	4.52	4.53					4.52			D
7141	10226	4.07	0.17	0.17	4.95	5.04	4.86	4.10	4.08		4.27	4.27	3.94	3.94			D
7150		3.51	1.18	0.80				3.61	3.53			3.66		3.65		3.59	
7157		4.00	1.59	2.05	4.32	4.32	4.32	4.32	4.35				4.30				V
7172	10265	5.22	0.53	0.42	5.40	5.39	5.41	5.37	5.20			5.60		5.31			
7176	10273	4.02	1.08	0.76	4.28	4.29	4.27	4.21	4.10		4.34			4.19			
7178	10276	3.24	-0.05	-0.03	3.55	3.57	3.52	3.50	3.31					3.30			
7180	10282	4.82	1.15	0.85	5.05	5.05	5.04	4.91	4.85				4.97	4.92			
7193		4.02	1.09	0.79				4.15	4.02		4.26			4.18			
7194		2.59	0.08	0.05	2.71	2.89		2.71	2.89	2.44			2.69	2.79	2.57	2.86	D
7215	10335	5.02	0.19	0.21	5.32	5.32	5.33	5.06	5.04					5.07			
7217		3.77	1.00	0.72				3.90	3.91			3.74		4.00	3.93		
7224		3.21	1.20	0.87	3.32	3.29	3.34	3.42	3.48			3.46		3.39	3.49	3.27	
7235	10361	2.99	0.01	0.01				3.02	3.10					2.99	2.96		
7236		3.43	-0.09	-0.03				3.55	3.62		3.45			3.51		3.61	
7254		4.11	0.04	0.04				4.12		3.84			4.22	4.06	4.08	4.41	
7259		4.11	1.20	0.82				4.16		3.94			3.99	4.34	4.32	4.19	
7264		2.88	0.34	0.34				3.02	3.11			2.83		3.11			
7282		4.83	0.55	0.43				4.93	5.19			4.69		4.91			D
7298	10504	4.38	-0.14	-0.10	4.68	4.71	4.65	4.46	4.47				4.50	4.50	4.61		

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	K
7306	10526	4.77	-0.04	0.01	4.98	5.07	4.89	4.60	4.67					4.52			
7310	10541	3.32	1.00	0.70	3.32	3.31	3.24	3.21	3.21	3.19				3.31	3.25		C
7312	10546	5.14	0.31	0.31	5.28	5.33	5.23	5.06	4.92					5.08	5.18		
7314	10547	4.37	1.25	0.87	4.52	4.54	4.50	4.46	4.34		6.37			4.58	6.21		
7317	6.06	1.43	1.12					6.28						6.25			
7328	10575	3.76	0.97	0.63	3.95	3.90	4.00	3.98	3.94		4.07			3.97	3.94		
7340	7340	3.93	0.22	0.19	3.93			3.95	3.93					3.97			
7342	10617	4.61	0.10	0.27	4.42	4.40	4.44	4.63	4.67					4.62	4.44		
7352	10630	4.45	1.25	0.90	4.42	4.40	4.44	4.63	4.54	4.64				4.67	4.66		C
7358	10630	5.18	-0.12	-0.04	5.33	5.40	5.26	4.92	5.01					4.83			
7371	10650	4.59	0.02	0.04	4.80	4.76	4.84	4.63	4.55					4.71	4.86		
7372	10653	4.97	-0.09	0.02	5.10	5.11	5.10	4.86	4.93					4.80			
7377	10663	3.36	0.32	0.25	3.74	3.70	3.77	3.44	3.46		3.46			3.39			
7387	10676	4.67	0.60	0.51	4.82	4.82	4.81	4.86	4.80					4.81			
7405	10724	4.45	1.50	1.21	4.43	4.47	4.40	4.63	4.69		4.98			4.57			
7417	10749	3.08	1.13	0.87	3.16	3.18	3.14	3.24	3.13					3.35			
7420	10757	3.79	0.14	0.11	3.97	3.91	4.03	3.94	3.89		3.90			4.02			
7426	10769	4.74	-0.13	0.01	4.88	4.93	4.84	4.85	4.80					4.90			
7429	10789	4.45	1.18	0.91	4.56	4.56	4.57	4.65	4.68		4.71			4.54	4.68		
7437	10804	4.99	-0.07	-0.01	5.20	5.17	5.22	4.88	4.98					4.77			
7440	4.60	-0.06	-0.03					4.66	4.64		4.57	4.42		4.67	4.75	4.94	
7446	4.96	0.00	0.06					5.04	4.93					4.92	5.12	5.21	
7447	4.36	-0.09	0.02					4.28	4.27					4.28			
7451	10833	5.74	0.48	0.46	5.93	5.89	5.97	5.65	5.57					5.73			
7462	10844	4.69	0.80	0.65	4.87	4.86	4.88	4.78	4.74	4.78				4.81	4.81		C
7469	10866	4.47	0.39	0.35	4.60	4.66	4.55	4.64	4.65		4.87	4.70		4.48	4.48		P
7478	10891	4.70	0.95	0.68	4.78	4.78	4.78	4.79	4.89			4.69		4.78	4.48		
7479	10895	4.37	0.77	0.57	4.52	4.54	4.50	4.37	4.27					4.30	4.54		
7488	10908	4.37	1.05	0.71	4.62	4.61	4.62	4.45	4.40		4.51			4.44			
7503	10939	5.95	0.64	0.45	6.32	6.30	6.34	6.26	6.24		6.01			6.67	5.94		
7504	10941	6.20	0.66	0.44	6.31	6.36	6.26	6.37	6.35		6.33			6.78	6.52		
7525	10975	2.72	1.52	1.07	3.08	3.01	3.14	2.80	2.77					2.84			
7528	10977	2.87	-0.02	-0.01	3.18	3.21	3.14	2.97	3.05					2.90	2.95		
7546	11009	5.00	0.10	0.14	5.23	5.28	5.18	4.95	4.95					4.90	4.99		D
7536	10989	3.83	1.41	1.44	3.66	3.73	3.98	3.78	3.72					3.85			
7557	11027	0.76	0.22	0.14	1.12	1.12	1.12	0.89	0.97		0.95			0.74			
7565	11044	4.96	-0.12	-0.02	5.15	5.14	5.12	4.91	5.02					4.85	4.86		DC
7582	11065	3.82	0.89	0.64	3.99	4.04	3.94	3.99	3.93	3.98	3.99			4.03	4.01		
7589	11071	5.62	-0.07	0.10	5.81	5.76	5.86	5.51	5.64					5.33	5.56		
7592	11075	4.58	-0.06	0.03	4.75	4.37	4.29	4.50	4.66					4.34			
7595	11078	4.68	1.05	0.76	4.85	4.85	4.85	4.86	4.92		4.79			4.88	4.79	4.78	P
7597	11080	4.70	0.75	0.59	4.70	4.70	4.70	4.81	4.95		4.75			4.79	4.79		
7602	11089	3.72	0.86	0.66	3.82	3.70	3.93	3.90	3.95					3.84			
7604	11091	4.50	1.46	1.02	4.62	4.62	4.62	4.72	4.72		4.59			4.60	4.56		
7613	11114	4.95	-0.09	0.01	5.15	5.14	5.17	4.87	4.67					5.00	4.95		
7615	11118	3.93	1.03	0.74	4.08	4.14	4.03	4.03	4.04		4.04			4.00			
7618	11123	4.82	0.89	0.65	5.11	5.18	5.04	4.95	5.03		5.05			4.66			
7619	11123	4.92	0.12	0.10	5.11	5.18	5.04	4.80	4.77					4.83			D
7635	11146	3.47	1.57	1.20	3.83	3.78	3.88	3.71	3.65		3.72			3.76			
7650	4.59	1.65	1.65	1.87				4.60	4.69		4.64			4.53			4.52

T A B L E 1 (continued)

BS	ED	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
7653	11187	4.65	0.18	0.16	4.89	4.86	4.93	4.74	4.93					4.66	4.63		
7665		3.56	0.76	0.61				3.64					3.56			3.73	
7678	11255	5.65	0.54	0.52	5.91	5.87	5.94	5.69	5.50		5.77			5.86	5.64		C
7685	11274	4.50	1.31	0.93	4.73	4.66	4.79	4.66	4.58	4.67				5.74	4.86		
7703		5.32	0.87	0.75				5.34		5.17				5.42	5.42	5.31	
7708	11315	4.92	-0.12	0.03	5.23	5.20	5.26	4.82	4.84					4.80	4.97		
7710		3.32	-0.07	-0.07				3.37						3.23	3.35	3.47	
7722		5.73	0.88	0.71	5.12	5.15	5.10	5.69	5.97					5.66	5.76	5.83	
7754	11376	4.33	0.09	0.16	4.94	4.95	4.94	4.96	5.11					4.94	4.94		
7750	11388	4.83	0.09	0.16				4.96						4.97	4.97		
7735	11396	3.80	1.28	0.97	3.94	3.93	3.94	3.95	3.80					4.02	4.02		V
7736	11401	4.99	0.12	0.20	5.22	5.17	5.27	4.98	5.04					5.10	4.81		
7739	11410	4.77	-0.18	-0.08	5.08	5.03	5.13	4.82	4.76					4.83			
7740	11411	4.30	0.11	0.12	4.54	4.51	4.58	4.32	4.41					4.24	4.38		
7741	11413	5.15	1.04	0.74	5.34	5.38	5.38	5.38	5.49		4.23			5.26			
7744	11416	4.52	1.26	0.96	4.68	4.63	4.72	4.73	4.79					4.67			
7746	11420	6.12	1.04	0.77	6.32	6.30	6.34	6.16	6.15					6.16			
7747		4.26	1.08	0.79				4.55	4.53					4.68		4.43	
7750	11429	4.59	-0.05	-0.02	4.63	4.63	4.62	4.40	4.38					4.41			D
7751	11432	3.98	1.52	1.20	4.16	4.13	4.18	4.16	4.07					4.25			V
7754		3.58	0.95	0.69				3.77	3.78					3.80		3.74	
7763	11468	4.82	0.42	0.54	5.04	5.09	5.00	4.88	4.90					4.87			V
7767	11475	5.84	0.10	0.15	6.05	6.05	6.05	5.82	5.82	5.82				5.82			D
7770	11481	5.17	0.65	0.57	5.31	5.29	5.33	5.18	5.20					5.17			
7773		4.76	-0.04	0.01				4.84	4.68					4.66	5.00	5.00	
7754		3.08	0.79	0.55				3.25	3.38					3.16	3.16	3.36	
7781	11497	5.76	0.12	0.33	5.87	5.90	5.83	5.71	5.69					5.80	5.64		
7784	11509	6.23	0.06	0.06	6.56	6.49	6.64	6.07						6.07			
7790		1.94	-0.20	-0.09				2.12					2.05				
7796	11531	2.23	0.67	0.49	2.48	2.47	2.50	2.32	2.31					2.33		2.18	
7806	11550	4.44	1.33	1.01	4.65	4.57	4.73	4.60	4.60					4.67	4.54		
7822		4.91	0.37	0.35				4.96	4.98					4.99	4.99	5.10	D
7834	11616	4.02	0.40	0.36	4.32	4.25	4.39	4.09	4.13	4.06				4.08			
7844	11640	4.95	-0.09	0.03	5.09	5.16	5.01	4.89	4.97					4.88	4.83		
7847	11643	6.18	1.01	0.85	6.38	6.34	6.41	6.30		6.30				4.88			
7850	11664	4.22	0.20	0.17	4.34	4.26	4.41	4.28	4.33					4.24	4.25		C
7852	11668	4.04	-0.12	-0.02	4.39	4.34	4.44	4.38	4.15	4.28				4.02			
7866	11693	4.63	1.61	1.30	4.79	4.77	4.82	4.83	4.77					4.93			
7871	11702	3.69	0.11	0.13	4.74	4.79	4.70	4.59	4.71					4.67			
7882	11727	3.63	0.44	0.40	4.02	3.95	4.09	3.72	3.65					3.73			D
7884		4.33	0.96	0.67				4.51	4.44					4.51	4.57	4.52	
7891	11745	4.82	-0.02	0.03	5.04	4.99	5.09	4.78	4.82					4.71	4.82		
7906	11758	3.77	-0.06	0.00	4.14	4.11	4.17	3.86	3.96					3.77			
7924	11806	1.25	0.09	0.11	1.59	1.59	1.59	1.33	1.47	1.27				1.25			
7928	11814	4.44	0.32	0.26	4.54	4.60	4.47	4.53	4.57	4.47				4.56			
7936		4.13	0.43	0.36				4.26	4.33					4.29		4.28	
7939	11833	4.91	1.19	0.85	5.10	5.06	5.14	4.73	5.13	4.12				4.29			
7942	11840	4.23	1.06	0.77	4.46	4.43	4.50	4.34	4.29					5.13			
7947	11847	3.91	0.83	0.68	4.19	4.17	4.21	4.12	4.16					4.40			
7949	11848	2.46	1.03	0.73	2.72	2.77	2.68	2.64	2.69					4.07			D

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
7950		3.77	0.00	0.07				3.83	3.81		3.98			3.84	3.63	3.90	
7951		4.44	1.57	1.47				4.60	4.62		4.67			4.78	4.54	4.41	
7955	11856	4.54	0.54	0.47		4.67	4.67	4.63	4.63					4.60	4.74		F
7957	11862	3.43	0.82	0.67		3.64	3.66	3.59	3.59					3.60	3.57		C
7963	11869	4.54	-0.11	-0.04		4.86	4.89	4.47	4.57					4.37			D
7977	11899	4.86	0.43	0.45		4.95	4.86	4.89	5.00			4.23		4.77	4.90		
7980		4.12	1.63	1.25				4.24	4.43		5.09			4.21	4.07		
7990		4.73	0.32	0.28				4.80	4.77					4.59	4.72		
7995	11924	4.61	0.82	0.68		4.80	4.80	4.78	4.73					4.67	4.88		
8001	11943	4.77	-0.14	-0.07		4.97	4.93	4.68	4.59					4.80	4.65		
8020	11996	5.67	0.47	0.48		5.84	5.88	5.76	5.84					5.68			
8028	12011	3.64	0.02	0.05		4.10	4.10	4.04	4.09					3.99			
8034	12025	5.23	0.32	0.32		5.25	5.25	5.29	5.37		5.20			5.31	5.13		
8047	12055	4.75	-0.41	0.13		4.95	4.79	4.86	4.57		4.87			5.01	4.99		
8060		4.84	0.18	0.16				4.93	5.17					4.95	4.78	4.89	
8075		4.07	-0.01	0.01				4.19	4.29					4.05	4.11	4.26	
8079	12117	3.70	1.65	1.28		3.80	3.81	3.82	3.73					3.85	4.05		
8080		4.49	1.60	1.28				4.60	4.63					4.80	4.61	4.62	
8085	12126	5.22	1.17	1.03		5.44	5.47	5.28	5.56					5.51	5.73		
8086	12127	6.03	1.37	1.17		6.09	6.14	6.04	6.27			4.62		6.22	6.44		
8089	12136	4.56	1.56	1.17		4.60	4.72	4.47	4.88					4.80	4.78	4.76	
8093		4.52	0.94	0.69				4.52	4.63					4.42			
8097	12162	4.68	0.26	0.25		4.66	4.74	4.57	4.79					4.72			
8115	12206	3.20	0.99	0.70		3.45	3.51	3.48	3.48					3.45	3.27		D
8123	12221	4.49	0.50	0.43		4.68	4.68	4.61	4.60					4.60	4.62		
8130	12238	3.73	0.40	0.35		3.90	3.91	3.88	3.94					3.83	3.68		D
8131	12239	3.90	0.52	0.44		4.08	4.08	4.14	4.11			4.17		4.06	4.23		
8143	12274	4.23	0.13	0.15		4.50	4.49	4.28	4.52					4.24			
8146	12281	4.42	-0.10	0.05		4.59	4.61	4.42	4.44				5.01	4.40	4.80	5.14	
8151		4.82	0.02	0.09				4.92						4.71			
8162	12316	2.45	0.22	0.21		2.78	2.73	2.60	2.58		2.55			2.63	2.63		
8167		4.27	0.91	0.82				4.30	4.35			6.37		4.26	6.56		
8170	12333	6.40	0.53	0.47		6.73	6.74	6.46	4.28					4.20	4.25	4.44	
8173	12338	4.09	1.11	0.79		4.24	4.28	4.20	4.30				4.27				
8181		4.22	0.48	0.47				4.30									
8204		3.74	1.00	0.64				3.86	3.79					3.94	4.07	3.76	
8207		3.78	1.44	1.05				6.03	6.03			3.72		6.05	6.03	5.77	
8213		4.51	0.91	0.88				4.59	4.46			6.02		4.80	4.61	4.61	
8225	12447	4.57	1.62	1.25		4.62	4.73	4.50	4.76			4.51		4.70	4.81	4.81	
8232		2.87	0.84	0.61				3.07	3.14			3.31		3.02	2.99	2.88	
8238	12476	3.23	-0.22	-0.10		3.40	3.51	3.46	3.39		3.26			3.30	3.35		GDV
8252	12514	4.02	0.89	0.71		4.24	4.25	4.26	4.17		4.37			4.15	4.21		
8255	12518	4.91	1.08	0.82		4.98	4.99	4.97	5.00					4.97	4.97	4.94	
8260		4.72	-0.16	-0.04				4.72	4.53		4.81			4.62	4.72	4.94	
8263		6.25	0.06	0.08				6.27	6.18					6.20	6.42	6.42	
8264		4.69	0.19	0.17				4.78	4.77			4.75		4.76	4.76	4.84	
8278		3.57	0.32	0.23				3.80	3.78					3.72	3.90	3.90	
8279	12372	4.73	0.30	0.31		5.06	5.13	4.99	4.79			4.93		4.84	4.82	4.89	
8283		4.73	0.88	0.67				4.82	4.72		5.02			4.64			
8291	12606	6.11	0.07	0.11		6.31	6.27	6.35	6.05		6.10		6.27	5.77			

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
8297	12611	6.05	2.52	1.83	6.13	6.13	6.13	6.38	4.47		6.32	6.44		6.37	4.78	m46	V
8301	12618	4.67	-0.12	-0.02	4.94	4.96	4.93	4.78	4.87				4.41	4.70	4.35		
8305	12628	4.34	-0.05	-0.01	2.76	2.64	2.87	4.35	4.23	4.22				4.34	4.35	4.53	D
8309	12635	4.51	0.49	0.38	4.72	4.73	4.72	4.45	4.37					2.67	4.50		
8313	12638	4.31	1.18	0.60	4.40	4.36	4.45	4.52	4.44		4.31	4.77		4.34	4.31		
8315	12642	4.02	0.44	0.37	4.24	4.19	4.27	4.21	4.21					4.24	5.00		V
8317	12644	4.57	1.10	0.84	4.68	4.68	4.69	4.85	4.79					4.77	4.31		
8322	12650	2.85	0.29	0.24	6.09	6.09	6.09	2.96	3.01					2.95	5.90		
8327	12660	5.94	0.31	0.28	6.09	6.09	6.09	5.97	6.05					5.92	5.90		
8334	12667	4.29	0.52	0.50	4.48	4.54	4.43	4.46	4.50	4.46				4.40	4.47		
8335	12670	4.24	-0.12	-0.05	4.44	4.40	4.49	4.26	4.44					4.10	4.23		
8353	12768	3.01	-0.12	-0.05	5.94	5.90	5.97	3.16	3.16	3.14	5.86		3.20	3.07	3.14	3.26	
8371	12768	5.80	0.72	0.68	5.06	5.02	5.09	6.01	6.06					6.10	5.41		V
8383	12800	4.90	1.75	1.71	5.06	5.02	5.09	5.35	5.17					5.46	5.41		
8387	12800	4.69	1.06	0.88	4.74	4.74	4.74	4.74	4.74				4.79	4.62	4.69		
8402	12802	4.69	-0.05	-0.01	5.76	5.69	5.82	5.66	5.70					5.33	5.59		
8407	12859	5.60	-0.02	0.03	5.76	5.69	5.82	5.54	5.54					5.22	4.61	4.59	
8410	12860	5.51	0.23	0.18	5.76	5.69	5.82	5.23	5.24	4.64				4.76	4.61	4.59	
8411	12860	4.46	1.57	1.00	5.76	5.69	5.82	4.60	4.60					4.76	4.61	4.59	
8413	12875	4.84	1.44	1.07	5.07	5.19	4.95	4.90	4.80					5.00	4.38		D
8414	12875	2.93	0.97	0.66	4.42	4.38	4.45	3.16	3.16	3.28				3.12	4.38		
8417	12879	4.29	0.34	0.32	4.42	4.38	4.45	4.40	4.45	4.38				4.38	4.38		
8418	12879	4.25	-0.07	-0.05	6.35	6.34	6.36	4.35	4.34					4.36	6.29		
8421	12887	6.12	1.60	1.66	6.35	6.34	6.36	6.29	6.29					4.36	6.29		
8425	12901	1.74	-0.13	-0.08	5.38	5.45	5.31	2.16	2.16				1.92	2.10	2.63	1.97	
8428	12901	5.11	0.08	0.15	4.00	4.03	3.97	3.99	3.99					5.18	4.05		
8430	12908	3.76	0.44	0.40	4.00	4.03	3.97	3.96	3.96					3.83	4.05	4.69	
8431	12940	4.50	0.65	0.07	4.08	4.07	4.08	4.62	4.52	4.69				4.65	4.53	4.69	
8450	12940	5.55	0.67	0.05	4.08	4.07	4.08	3.70	3.76					3.57	4.53	4.69	
8454	12950	4.29	0.46	0.39	4.46	4.53	4.38	4.38	4.41					4.27	4.48		
8461	12966	5.95	0.95	0.72	6.16	6.13	6.20	6.06	6.06		6.09			5.90	6.18		
8465	12971	3.35	1.55	1.08	3.60	3.63	3.57	3.62	3.54					3.70	4.23		
8468	12977	4.79	0.92	0.69	4.95	5.01	4.89	4.99	4.95					5.10	5.27		
8469	12980	5.05	0.24	0.28	5.34	5.29	5.38	5.19	5.29					5.00	5.27		
8473	12982	6.37	-0.06	0.00	6.62	6.54	6.71	6.36	6.36					4.62	4.32	4.35	
8482	12998	4.49	1.39	1.01	4.55	4.55	4.54	4.64	4.65					4.23	4.23		
8494	13021	4.19	0.28	0.27	4.36	4.38	4.34	4.23	4.24					4.30	4.32		
8498	13023	4.13	1.66	1.00	4.32	4.33	4.31	4.22	4.14					4.31	4.32	4.35	
8499	13023	4.13	1.66	1.00	4.32	4.33	4.31	4.22	4.14					4.31	4.32	4.35	
8499	13023	4.13	1.66	1.00	4.32	4.33	4.31	4.22	4.14					4.31	4.32	4.35	
8502	13076	2.83	1.36	1.05	5.01	5.01	5.01	2.91	2.91				2.90	3.81	2.92		
8518	13073	3.84	-0.06	0.04	5.15	5.15	5.15	3.97	4.07					4.82	4.04		P
8520	13073	4.99	-0.10	-0.07	5.15	5.15	5.15	4.93	5.06					4.82	4.92	6.65	P
8521	13076	6.62	2.01	3.44	5.01	5.01	5.01	6.65	6.65					4.78	4.98		P
8522	13076	4.81	0.00	0.09	5.01	5.01	5.01	4.88	4.89					4.78	4.98		P
8523	13079	4.56	-0.10	-0.02	4.72	4.81	4.62	4.66	4.77					4.54	4.67		
8538	13104	4.44	1.02	0.75	4.59	4.63	4.55	4.58	4.52					4.60	4.62		
8539	13108	4.64	-0.04	0.16	4.60	4.53	4.66	4.64	4.59			4.62		4.51	4.65		
8541	13109	4.58	0.09	0.13	4.74	4.81	4.68	4.64	4.64					4.63	4.65		
8551	13153	4.80	1.06	0.78	4.94	4.94	4.88	4.95	4.97					4.89	4.94		

T A B L E 1 (continued)

BS	ID	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m34	m44	m45	m46	R
8556		3.97	1.03	0.73				4.02					4.07	4.01	3.96	4.04	
8558		3.66	0.38	0.39				3.75	3.81					3.79	3.66		D
8560		4.11	1.57	1.73				4.31	4.57				4.26	4.33	4.34	4.32	D
8572	13166	4.37	1.68	1.39	4.48	4.54	4.41	4.61	4.83					4.65	4.61	5.07	
8573		4.81	-0.08	0.00				4.89						4.77			
8576		4.29	0.01	0.02				4.36	4.26	4.37			4.48	4.32	4.31	4.44	D
8579	13178	4.51	-0.09	-0.01	4.71	4.88	4.75	4.54	4.57					4.47	4.58		
8585	13187	3.77	0.01	0.00	3.94	3.94	3.93	3.85	3.90			4.21		3.80			
8597		4.00	-0.10	-0.06	4.88	4.82	4.95	4.13	4.22					3.97			
8613	13250	4.63	0.24	0.22	5.06	5.15	4.98	4.83	4.80					4.93	4.77		
8622	13270	4.88	-0.20	-0.09	4.58	4.62	4.54	4.91	5.04			4.41		4.20	4.76		
8628		4.16	-0.12	-0.06	3.74	3.80	3.67	4.22	4.06				4.35	4.70	4.34		
8630		4.16	0.21	0.22				4.34						4.70	4.51		
8632	13289	4.46	1.33	0.92	5.02	5.02	5.03	4.64	4.70				2.09	2.54	2.50	2.25	
8634	13294	3.40	-0.09	-0.04	3.22	3.30	3.5	3.61	3.59		3.97	3.55		3.20	3.03		
8636		2.11	1.62	1.91				2.24						4.31	4.13		
8641	13303	4.79	-0.01	0.04	4.39	4.38	4.40	4.31	4.23			4.40		4.12	4.13		
8644		4.85	1.03	0.76	4.19	4.27	4.11	4.14	4.18				3.69	4.83	4.79	3.69	
8649		4.69	1.36	0.97	3.86	3.88	3.83	3.69	3.74					4.35	4.04		
8650	13313	2.95	0.86	0.64	3.68	3.69	3.68	4.21	4.07					4.35	3.68		
8665	13354	4.19	0.50	0.43	3.68	3.69	3.68	3.68	3.62	3.72				3.72	3.68		
8667	13355	3.94	1.08	0.76	4.81	4.87	4.75	4.52	4.29	4.47			4.63	4.51	4.54	4.67	D
8675		3.47	0.08	0.11				3.84	3.80					3.99	3.81	3.76	
8679		3.98	1.59	1.19	5.08	5.01	5.14	4.97	4.82					5.02	6.02		
8684	13388	3.48	0.94	0.68	5.00	5.05	4.96	5.89	5.82					5.84			
8694	13399	3.53	1.05	0.83	5.48	5.44	5.52	5.10	5.17					3.54	3.58		
8695		4.46	-0.04	0.02	5.48	5.44	5.52	4.96	4.96					4.88	4.40	4.38	
8698		3.79	1.65	1.42	6.59	6.65	6.53	6.46	6.43					4.28	6.65	6.26	
8702	13421	4.74	1.26	0.94	4.76	4.87	4.75	5.10	5.17					5.20	4.94		
8704		5.81	-0.08	0.01	5.00	5.05	4.96	4.96	4.96					5.06			
8709		3.28	0.05	0.07	5.48	5.44	5.52	5.10	5.17					3.54	3.58		
8717	13449	4.90	0.00	0.04	5.08	5.01	5.14	4.96	4.96					4.88	4.40	4.38	
8720		4.21	0.97	0.74	5.00	5.05	4.96	5.10	5.17					4.28	6.65	6.26	
8721		6.49	1.10	0.95	5.00	5.05	4.96	5.10	5.17					5.20	4.94		
8726	13463	4.94	1.77	1.35	5.48	5.44	5.52	5.10	5.17					5.06			
8728		1.16	0.09	0.06	5.48	5.44	5.52	5.10	5.17					1.26	1.28	1.42	
8729	13469	5.50	0.67	0.54	5.48	5.44	5.52	5.10	5.17					1.26	1.28	1.42	
8737	13480	6.43	0.64	0.53	4.76	4.87	4.75	4.96	4.96					5.61	6.47	4.22	
8747		4.11	0.95	0.77	4.76	4.87	4.75	4.96	4.96					6.54	6.47		
8748	13495	4.72	1.43	1.09	4.76	4.87	4.75	4.96	4.96					5.06			
8752	13498	5.13	1.55	1.17	5.34	5.31	5.37	5.48	5.63					5.37	5.44		V
8762	13515	3.62	-0.09	0.01	4.00	4.02	3.97	3.63	3.77					3.49			
8773	13541	4.52	-0.12	-0.02	4.66	4.66	4.67	4.58	4.57			4.83		4.34			V
8775		2.42	1.67	1.50	4.80	4.83	4.77	2.61	2.56					3.76	2.52		
8780	13548	4.66	1.06	0.74	4.80	4.83	4.77	4.91	4.87					5.08	4.79		
8781	13550	2.48	-0.04	0.01	3.20	3.19	3.21	2.57	2.61					2.61	4.35	4.42	
8787		4.29	0.43	0.38	4.62	4.62	4.62	4.35	4.35					4.23	4.35	4.42	
8789		4.48	0.90	0.71	4.62	4.62	4.62	4.77	4.82					4.54	4.80		
8795	13571	4.51	1.58	1.26	4.62	4.62	4.62	4.69	4.65					4.73			F
8796	13575	4.77	1.35	0.97	4.95	4.93	4.97	4.98	4.89					5.00	5.06		

T A B L E 1 (continued)

BS	PD	V	B-V	V-R	Gr	Gr1	Gr2	mag	m14	m23	m24,1	m24,4	m24	m44	m45	m46	R
8797	13579	4.86	-0.03	0.10	4.97	4.89	5.05	4.93	4.99					5.00	4.79		
8804	13591	5.33	1.41	1.02	5.33	5.29	5.37	6.19	5.67					5.43	5.59		D
8808	13600	6.25	-0.01	0.05	6.54	6.59	6.48	3.80	3.55		4.03			3.81	6.19		
8812		3.64	1.23	0.84				4.94	4.89		5.12			4.80			
8817		4.68	0.64	0.54													
8819	13614	4.42	0.82	0.65	4.54	4.49	4.59	4.56	4.48	4.55				4.63	4.60	4.06	D
8820		3.90	1.02	0.75				4.10	4.70				4.06	4.07	4.20		
8830	13653	4.53	0.30	0.29	4.66	4.67	4.66	5.65	4.70					4.53	4.62		
8832	13657	5.57	1.00	0.83	5.65	5.66	5.64	5.46	4.24					5.73	5.76		
8834		4.22	1.55	1.28				4.40	4.24					4.56			
8841		4.25	1.11	0.79				4.46	4.48		4.63	4.36		4.54		4.28	
8848		3.98	0.39	0.11				4.10					3.98	3.88	4.21		
8852	13690	3.69	0.91	0.72	4.08	3.99	4.16	3.85	3.82					4.68		4.54	
8858		4.40	-0.14	-0.07				4.56	4.53		4.51	5.10		5.00			
8860	13701	4.86	1.67	1.46	4.96	4.96	4.95	4.99	4.87					5.00			
8863		4.41	1.13	0.84				4.51	4.59	4.50			4.34	4.68	4.53	4.43	D
8872	13714	4.76	0.84	0.65	4.90	4.90	4.90	4.90	4.92					4.89	4.92		
8880	13729	4.60	0.17	0.21	4.65	4.60	4.70	4.65	4.71					4.59		4.06	
8892		3.98	1.10	0.82				4.20	4.12	4.48				4.15			
8905	13775	4.41	0.61	0.54	4.70	4.72	4.69	4.57	4.57					4.57			
8906		4.40	1.47	1.13				4.52	4.36				4.69	4.64		4.41	
8911	13789	4.94	0.04	0.07	5.19	5.16	5.22	4.94	4.87					4.88	4.93		
8916	13799	4.30	1.08	0.80	4.48	4.52	4.44	4.45	4.41					4.49			
8923	13815	4.56	0.94	0.74	4.78	4.79	4.59	4.67	4.65					4.72			
8926	13827	4.94	-0.12	0.01	5.13	5.16	5.10	4.89	4.76					4.97	4.97		V
8937		4.37	-0.09	0.00				4.46		4.40			4.58	4.37	4.35	4.62	
8939		4.72	0.02	0.07				4.76	4.73					4.78	4.82		
8947	13878	5.59	0.10	0.12	5.94	5.90	5.99	5.50	5.54				4.72	5.45	4.66	4.95	
8949		4.71	0.08	0.12				4.80					4.87	4.72	4.96	4.98	
8959		4.74	0.08	0.11				4.86					4.92	4.60	4.96		
8961	13908	3.82	1.02	0.78	3.94	3.98	3.90	4.00	3.95			4.04		4.14	3.89		V
8965	13914	4.29	-0.11	0.00	4.48	4.54	4.41	4.28	4.30					4.23	4.30		
8969	13927	4.13	0.51	0.44	4.28	4.27	4.29	4.28	4.28		4.35	4.28		4.21			
8974	13939	3.21	1.03	0.73	3.43	3.45	3.41	3.42	3.37					3.48			
8976	13942	4.14	-0.08	-0.01	4.44	4.33	4.34	4.33	4.42					4.30	4.26		
8982		4.84	0.81	0.62				4.95	4.78					5.07		4.99	
8984	13955	4.51	0.21	0.18	4.78	4.74	4.82	4.61	4.69			4.76		4.44		4.76	
8988		4.51	-0.04	0.02				4.62	4.68		4.63			4.45	5.06		D
8997	13970	4.93	0.96	0.71	5.07	5.14	5.00	4.98	4.93					4.96			V
9004	13990	5.04	2.61	1.87	5.12	5.05	5.19	5.30	5.15					5.44			
9016		4.57	0.00	0.04				4.64	4.56				4.61	4.68	4.62	4.72	
9030	14037	5.79	1.66	0.26	5.92	6.05	5.80	6.11	6.02				6.19	6.11			V
9045	14076	4.52	1.26	0.96	4.92	4.78	4.85	4.85	4.56					5.04	4.96		
9064	14115	4.66	1.59	1.46	4.80	4.84	4.77	4.75	4.56					4.69			
9071	14123	4.88	-0.06	0.04	5.12	5.11	5.14	4.93	4.96		4.66			5.05	5.04		D
9072	14125	4.01	0.42	0.38	4.23	4.28	4.22	4.22	4.16					4.04			
9076		4.46	-0.09	0.02				4.71					4.64	4.78		4.78	
9084	14159	4.79	1.24	0.98	5.96	5.91	6.00	4.73	5.83			4.67	4.62	5.90	5.82	4.84	
9088		3.75	0.67	0.59				5.85						4.79			
9089		4.41	1.63	1.56				4.99	4.98	5.07				5.00	4.86	5.11	
9091		5.00	-0.16	-0.05				4.99	4.98					5.00	4.86	5.11	
9098		4.56	-0.04	0.03				4.62						4.51		4.79	

IV. Multiple regression analysis

Multiple regression is used in data analysis to obtain the best fit of a set of observations of independent and dependent variables by an equation of the form:

$$y = c + b_1x_1 + b_2x_2 + \dots + b_nx_n \quad (3)$$

where y is the dependent variable; x_1, x_2, \dots, x_n are the independent variables; and c, b_1, b_2, \dots, b_n are the coefficients to be determined.

A multiple regression solution gives the least square "best" fit value of these coefficients for a particular sample of observations. The solution also gives a measure of the reliability of each of the coefficients so that inferences can be made regarding the parameters of the population from which the sample of observations was taken.

Thus, the data given in Table 1 can be studied with the help of multiple regression analysis using the above equations. Since we have two colors (B-V and V-R), we have

$$m - V = c + b_1 (B-V) + b_2 (m - \bar{m}) + b_3 (B-V) (m - \bar{m}) \quad (4)$$

and

$$m - V = c' + b'_1 (V-R) + b'_2 (m - \bar{m}) + b'_3 (V-R) (m - \bar{m}) \quad (5)$$

where

m , is one of the magnitudes listed in Table 1, columns 6-17; $V, (B-V)$, and $(V-R)$ are the magnitude and colors also given in Table 1 columns 3-5; $\bar{m} = \frac{1}{n} \sum m$; and the c 's and b 's are the coefficients to be derived.

The IBM 360/40 computer of the University of Chile has been used to carry out the multiple regression analysis. The program was made with the help of Messrs. Quinteros and Pérez, both from the University of Chile. A copy of this program (in Fortran language) is given in Appendix I. The program was prepared to compute first, equation 4 and next equation 5. Immediately it assumed $b_3 = b'_3 = 0$ and it calculated all, again. Forthwith it assumed $b_2 = b'_2 = b_3 = b'_3 = 0$ and it made again all the computations. Only in a few cases it was assumed $b_2 = b'_2 = 0$ and $b_3 \neq b'_3 \neq 0$. Most of the results of these computations are given in Tables 2-5. Tables 2 and 3 give those obtained with Potsdam photometry. Tables 4 and 5 those obtained with Harvard photometry. Tables 2 and 4 list the results employing equation (4). Tables 3 and 5 list the results employing equation (5). The columns of Tables 2-5 give:

- 1st. Line 1, the Postdam or Harvard magnitude, m (see equations (4) and (5)). Line 2, the arithmetic mean of all the m magnitudes entered in the regression (see above). Line 3, the constant term, c , obtained from the computation.
- 2nd. Lines 1-3 the regression coefficients b_1, b_2 and b_3 or b'_1, b'_2 and b'_3 . When in lines 2 or 3 there appears a 0.000000 number, it means that the regression was made without this coefficient (see above).
- 3rd. Lines 1-3, the standard deviation of the coefficients given in the 2nd column.
- 4th. Lines 1-3, T-values (student's T distribution) of the coefficients given in the 2nd column.
- 5th. Line 1, multiple correlation coefficient, R , of the variables. Line 2, standard error of the estimation, ϵ . Line 3, sum of squares "due to" or "explained by" the regression, SSAR.
- 6th. Line 1, k (3, 2 or 1) degrees of freedom. Line 2, SSAR/ k . Line 3, sum of squares of the deviations, SSDR.
- 7th. Line 1, degrees of freedom of SSDR, $n-k-1$. Line 2, mean square error, SSDR/ $n-k-1$. Line 3, F-value

$$F = \frac{SSAR/k}{SSDR/n-k-1}$$

- 8th. Remarks. *All* means that in the sample were included all stars with a given magnitude from one of the columns 6-17 listed in Table 1; $90^\circ \geq \delta > 60^\circ$ means that in the sample were included only stars with declination between 90 and 60 degrees north; and so on.

TABLE 2
POTSDAM STATISTICAL RESULTS WITH B-V

magnitude \bar{m}	c o e f f i c i e n t s			R	k	n-k-1	Remarks
	constant term	Regression	St.deviation	T-values	ϵ SSAR	SSAR/k SSDR	
Gr 4.9247 0.2532640	-0.0697601 0.0009453 -0.0135424	0.0048069 0.0032447 0.0044810	-14.5125942 0.2913503 - 3.0222044	0.4279503 0.0855865 1.5786428	3 0.5262142 7.0411596	959 0.0073422 71.6699677	All
Gr 4.9247 0.2531043	-0.0682179 -0.0058722 0.0000000	0.0047999 0.0023421	-14.2123232 - 2.5071917	0.4187621 0.0860488 1.5115824	2 0.7557912 7.1082201	960 0.0074044 102.0733185	All
Gr 4.9247 0.2526200	-0.0673351 0.0000000 0.0000000	0.0048001	-14.0277815	0.4122646 0.0862851 1.4650402	1 1.4650402 7.1547623	961 0.0074451 196.7785950	All
Gr 4.6093 0.2265248	-0.0663246 -0.0218914 0.0088467	0.0125490 0.0121424 0.0140557	- 5.2852545 - 1.8028927 0.6294054	0.5181920 0.0680242 0.1392908	3 0.0464303 0.3794389	82 0.0046273 10.0339813	$90^\circ \geq \delta > 60^\circ$
Gr 4.6093 0.2255437	-0.0654675 -0.0163093 0.0000000	0.0124294 0.0082631	- 5.2671385 - 1.9737434	0.5147710 0.0677763 0.1374578	2 0.0687289 0.3812720	83 0.0045936 14.9617538	$90^\circ \geq \delta > 60^\circ$
Gr 4.6093 0.2240732	-0.0631210 0.0000000 0.0000000	0.0125839	- 5.0160227	0.4800949 0.0689346 0.1195626	1 0.1195626 0.3991672	84 0.0047520 25.1605225	$90^\circ \geq \delta > 60^\circ$
Gr 4.7569 0.2319596	-0.0556132 -0.0142485 0.0029720	0.0068892 0.0051948 0.0069427	- 8.0724745 - 2.7428427 0.4280795	0.4350872 0.0745988 0.4483082	3 0.1494361 1.9199219	345 0.0055650 26.8528900	$60^\circ \geq \delta > 30^\circ$
Gr 4.7569 0.2321717	-0.0559077 -0.0126433 0.0000000	0.0068467 0.0035910	- 8.1655807 - 3.5208025	0.4345922 0.0745107 0.4472888	2 0.2236444 1.9209414	346 0.0055519 40.2828369	$60^\circ \geq \delta > 30^\circ$
Gr 4.7569 0.2325069	-0.0565123 0.0000000 0.0000000	0.0069581	- 8.1241589	0.3997629 0.0757244 0.3784678	1 0.3784678 1.9897623	347 0.0057342 66.0020447	$60^\circ \geq \delta > 30^\circ$
Gr 5.0875 0.2700045	-0.0779626 0.0045400 -0.0203787	0.0070755 0.0044200 0.0062221	-11.0187244 1.0271530 - 3.2752047	0.4383830 0.0917110 1.0484972	3 0.349499 4.4073200	524 0.0084109 41.5530243	$30^\circ \geq \delta \geq 0^\circ$
Gr 5.0875 0.2700582	-0.0747324 -0.0053970 0.0000000	0.0070710 0.0032438	-10.5688677 - 1.6637897	0.4190975 0.0925567 0.9582749	2 0.4791374 4.4975414	525 0.0085667 55.9299164	$30^\circ \geq \delta \geq 0^\circ$
Gr 5.0875 0.2693141	-0.0733207 0.0000000 0.0000000	0.0070317	-10.4271832	0.4138796 0.0927121 0.9345613	1 0.9345613 4.5212555	526 0.0085955 108.7262726	$30^\circ \geq \delta \geq 0^\circ$
Gr 5.1510 0.2633793	-0.0708126 0.0106499 -0.0215970	0.0078876 0.0044474 0.0066231	- 8.9776812 2.3946638 - 3.2608595	0.4103688 0.0849270 0.5959195	3 0.1986398 2.9427414	408 0.0072126 27.5406647	$0^h \leq \alpha < 8^h$
Gr 5.1510 0.2617189	-0.0644211 0.0007097 0.0000000	0.0077297 0.0032762	- 8.3342705 0.2166209	0.3830533 0.0859213 0.5192271	2 0.2596135 3.0194330	409 0.0073825 35.1661835	$0^h \leq \alpha < 8^h$
Gr 5.1510 0.2617859	-0.0645646 0.0000000 0.0000000	0.0076923	- 8.3934040	0.3829257 0.0858214 0.5188812	1 0.5188812 3.0197792	410 0.0073653 70.4493103	$0^h \leq \alpha < 8^h$
Gr 4.8700 0.2570043	-0.0766062 -0.0053626 -0.0077849	0.0080541 0.0055133 0.0070131	- 9.5114164 - 0.9726515 - 1.1100492	0.5241631 0.0776361 0.5799684	3 0.1933226 1.5309496	254 0.0060274 32.0742035	$8^h \leq \alpha < 16^h$
Gr 4.8700 0.2571548	-0.0765746 -0.0096167 0.0000000	0.0080577 0.0039654	- 9.5032310 - 2.4251776	0.5207962 0.0776713 0.5725416	2 0.2862708 1.5383759	255 0.0060328 47.4520416	$8^h \leq \alpha < 16^h$
Gr 4.8700 0.2567972	-0.0759925 0.0000000 0.0000000	0.0081306	- 9.3464823	0.5044006 0.0784084 0.5370597	1 0.5370597 1.5738583	256 0.0061479 87.3568420	$8^h \leq \alpha < 16^h$
Gr 4.6556 0.2338565	-0.0586587 -0.0331315 0.0081977	0.0087824 0.0083059 0.0103620	- 6.6790838 - 3.9889145 0.7911311	0.4348033 0.0881652 0.5237049	3 0.1745683 2.2464294	289 0.0077731 22.4579620	$16^h \leq \alpha < 24^h$
Gr 4.6556 0.2335710	-0.0584197 -0.0283729 0.0000000	0.0087716 0.0057242	- 6.6601028 - 4.9566469	0.4327791 0.0881083 0.5188400	2 0.2594200 2.2512541	290 0.0077631 33.4171295	$16^h \leq \alpha < 24^h$

TABLE 2 (continued)

magnitude \bar{m}	c o e f f i c i e n t s			R	k	n-k-1	Remarks
	constant term	Regression	St.deviation	T-values	SSAR	SSAR/k SSDR	
Gr 4.6556 0.2327123	-0.0569954 0.0000000 0.0000000	0.0091150	- 6.2529392	0.3441612 0.0916069 0.3281140	1 0.3281140 2.4420204	291 0.0083918 39.0992584	$16^h \leq \alpha < 24^h$
Gr 1 4.9220 0.2442552	-0.0580839 0.0032694 -0.0135433	0.0056104 0.0037758 0.0051970	-10.3529291 0.8658863 - 2.6060028	0.3209109 0.1001268 1.1037941	3 0.3679314 9.6143398	959 0.0100254 36.6999969	All
Gr 1 4.9220 0.2440991	-0.0566413 -0.0035510 0.0000000	0.0055998 0.0027298	-10.1148338 - 1.3008347	0.3108562 0.1004283 1.0357094	2 0.5178547 9.6824245	960 0.0100859 51.3446198	All
Gr 1 4.9220 0.2438279	-0.0561472 0.0000000 0.0000000	0.0055889	-10.0461340	0.3082845 0.1004645 1.0186443	1 1.0186443 9.6994896	961 0.0100931 100.9246216	All
Gr 1 4.6167 0.2360376	-0.0698527 -0.0205730 0.0059305	0.0150832 0.0146732 0.0171000	- 4.6311455 - 1.4020815 0.3468117	0.4680336 0.0817752 0.1538124	3 0.0512708 0.5483497	82 0.0066872 7.6670160	$90^\circ \geq \delta > 60^\circ$
Gr 1 4.6167 0.2353895	-0.0693055 -0.0168449 0.0000000	0.0149208 0.0099341	- 4.6449003 - 1.6956654	0.4668084 0.0813407 0.1530082	2 0.0765041 0.5491539	83 0.0066163 11.5629492	$90^\circ \geq \delta > 60^\circ$
Gr 1 4.6167 0.2338315	-0.0668196 0.0000000 0.0000000	0.0150134	- 4.4506617	0.4368261 0.0822436 0.1339844	1 0.1339844 0.5681776	84 0.0067640 19.8084106	$90^\circ \geq \delta > 60^\circ$
Gr 1 4.7592 0.2246250	-0.0385003 -0.0201158 0.0108888	0.0081187 0.0061357 0.0081345	- 4.7421503 - 3.2784853 1.3385944	0.3142069 0.0880244 0.2928195	3 0.0976065 2.6731625	345 0.0077483 12.5971556	$60^\circ \geq \delta > 30^\circ$
Gr 1 4.7592 0.2253654	-0.0394052 -0.0141952 0.0000000	0.0080998 0.0042574	- 4.8649654 - 3.3342524	0.3066676 0.0881251 0.2789359	2 0.1394680 2.6870461	346 0.0077660 17.9587250	$60^\circ \geq \delta > 30^\circ$
Gr 1 4.7592 0.2258697	-0.0403140 0.0000000 0.0000000	0.0082124	- 4.9089384	0.2548258 0.0894005 0.1925997	1 0.1925997 2.7733822	347 0.0079925 24.0976868	$60^\circ \geq \delta > 30^\circ$
Gr 1 5.0799 0.2565334	-0.0674283 0.0120136 -0.0241867	0.0083088 0.0051465 0.0072311	- 8.1152439 2.3343277 - 3.3447962	0.3474010 0.1078160 0.8360204	3 0.2786734 6.0911303	524 0.0116243 23.9733582	$30^\circ \geq \delta \geq 0^\circ$
Gr 1 5.0799 0.2565535	-0.0636567 0.0002643 0.0000000	0.0083115 0.0037976	- 7.6589108 0.0695921	0.3192392 0.1088570 0.7059715	2 0.3529857 6.2211790	525 0.0118499 29.7881622	$30^\circ \geq \delta \geq 0^\circ$
Gr 1 5.0799 0.2565886	-0.0637234 0.0000000 0.0000000	0.0082484	- 7.7255688	0.3192265 0.1087540 0.7059153	1 0.7059153 6.2212353	526 0.0118274 59.6845245	$30^\circ \geq \delta \geq 0^\circ$
Gr 2 4.9269 0.2616591	-0.0814924 0.0049730 -0.0149799	0.0061580 0.0041505 0.0057502	-13.2334766 1.1981459 - 2.6051168	0.3941398 0.1096309 2.1198578	3 0.7066193 11.5261707	959 0.0120189 58.7921143	All
Gr 2 4.9269 0.2614765	-0.0796658 -0.0025559 0.0000000	0.0061364 0.0029880	-12.9824734 - 0.8553612	0.3864828 0.1099609 2.0382919	2 1.0191460 11.6077366	960 0.0120914 84.2868958	All
Gr 2 4.9269 0.2612491	-0.0792512 0.0000000 0.0000000	0.0061164	-12.9572115	0.3856432 0.1099455 2.0294466	1 2.0294466 11.6165819	961 0.0120880 167.8891907	All
Gr 2 4.6033 0.2223665	-0.0690045 -0.0156504 0.0104581	0.0164390 0.0157489 0.0181362	- 4.1976061 - 0.9937460 0.5766428	0.4225175 0.0890650 0.1413583	3 0.0471194 0.6504714	82 0.0079326 5.9399881	$90^\circ \geq \delta > 60^\circ$
Gr 2 4.6033 0.2211662	-0.0679469 -0.0090418 0.0000000	0.0162706 0.0107585	- 4.1760654 - 0.8404278	0.4185570 0.0887061 0.1387206	2 0.0693603 0.6531090	83 0.0078688 8.8146191	$90^\circ \geq \delta > 60^\circ$
Gr 2 4.6033 0.2203313	-0.0666144 0.0000000 0.0000000	0.0161648	- 4.1209593	0.4100866 0.0885509 0.1331628	1 0.1331628 0.6586668	84 0.0078413 16.9822845	$90^\circ \geq \delta > 60^\circ$
Gr 2 4.7553 0.2416345	-0.0757409 -0.0053608 -0.0030886	0.0089290 0.0066998 0.0090030	- 8.4826126 - 0.8001464 - 0.3430643	0.4227662 0.0965242 0.6995309	3 0.2331769 3.2143383	345 0.0093169 25.0272522	$60^\circ \geq \delta > 30^\circ$

TABLE 2 (continued)

magnitude \bar{m} constant term	c o e f f i c i e n t s			R	k	n-k-1	Remarks
	Regression	St.deviation	T-values	ϵ SSAR	SSAR/k SSDR	SSDR/n-k-1 F	
Gr 2 4.7553 0.2414051	-0.0753829 -0.0070212 0.0000000	0.0088564 0.0046270	- 8.5116510 - 1.5174246	0.4224349 0.0964010 0.6984349	2 0.3492174 3.2154341	346 0.0092932 37.5778809	60° ≥ δ > 30°
Gr 2 4.7553 0.2415167	-0.0755848 0.0000000 0.0000000	0.0088721	- 8.5194311	0.4159136 0.0965818 0.6770373	1 0.6770373 3.2368317	347 0.0093280 72.5808258	60° ≥ δ > 30°
Gr 2 5.0934 0.2798870	-0.0857328 0.0061017 -0.0209131	0.0090834 0.0056880 0.0080359	- 9.4384003 1.0727415 - 2.6024618	0.3841315 0.1176223 1.2548885	3 0.4182962 7.2495451	524 0.0138350 30.2346039	30° ≥ δ ≥ 0°
Gr 2 5.0934 0.2799613	-0.0823507 -0.0040928 0.0000000	0.0090392 0.0041467	- 9.1103506 - 0.9870130	0.3695120 0.1182672 1.1611872	2 0.5805936 7.3432465	525 0.0139871 41.5091095	30° ≥ δ ≥ 0°
Gr 2 5.0934 0.2793798	-0.0812477 0.0000000 0.0000000	0.0089697	- 9.0580435	0.3673377 0.1182643 1.1475620	1 1.1475620 7.3568716	526 0.0139864 82.0481415	30° ≥ δ ≥ 0°

TABLE 3
POTSDAM STATISTICAL RESULTS WITH V-R

magnitude \bar{m}	c o e f f i c i e n t s			R	k	n-k-1	Remarks
	constant term	Regression	St.deviation	T-values	ϵ SSAR	SSAR/k SSDR	
Gr 4.9247 0.2577164	-0.0907475 0.0001492 -0.0120464	0.0062745 0.0034500 0.0059794	-14.4628773 0.0432494 -2.0146351	0.4255722 0.0857930 1.5611467	3 0.5203822 7.0586557	959 0.0073604 70.6999512	All
Gr 4.9247 0.2575418	-0.0897439 -0.0049743 0.0000000	0.0062647 0.0023351	-14.3254223 -2.1302567	0.4214807 0.0859295 1.5312729	2 0.7656364 7.0885296	960 0.0073839 103.6902161	All
Gr 4.9247 0.2572538	-0.0891279 0.0000000 0.0000000	0.0062695	-14.2161350	0.4168437 0.0860875 1.4977655	1 1.4977655 7.1220369	961 0.0074111 202.0985107	All
Gr 4.6093 0.2287253	-0.0820906 -0.0242656 0.0190468	0.0158944 0.0129930 0.0197973	-5.1647520 -1.8675900 0.9620925	0.5104229 0.0683948 0.1351454	3 0.0450485 0.3835843	82 0.0046779 9.6301575	$90^\circ \geq \delta > 60^\circ$
Gr 4.6093 0.2271621	-0.0800420 -0.0146602 0.0000000	0.0157441 0.0083113	-5.0839491 -1.7638884	0.5021798 0.0683641 0.1308156	2 0.0654078 0.3879141	83 0.0046737 13.9949760	$90^\circ \geq \delta > 60^\circ$
Gr 4.6093 0.2262816	-0.0783899 0.0000000 0.0000000	0.0159125	-4.9263248	0.4734474 0.0692180 0.1162745	1 0.1162745 0.4024552	84 0.0047911 24.2686920	$90^\circ \geq \delta > 60^\circ$
Gr 4.7569 0.2365323	-0.0746103 -0.0157929 0.0105705	0.0087718 0.0054292 0.0087475	-8.5057354 -2.9088678 1.2084103	0.4510726 0.0739442 0.4818557	3 0.1606185 1.8863745	345 0.0054678 29.3756104	$60^\circ \geq \delta > 30^\circ$
Gr 4.7569 0.2370249	-0.0747180 -0.0108551 0.0000000	0.0087771 0.0035773	-8.5127897 -3.0344629	0.4473201 0.0739934 0.4738718	2 0.2369359 1.8943586	346 0.0054750 43.2757874	$60^\circ \geq \delta > 30^\circ$
Gr 4.7569 0.2380863	-0.0769252 0.0000000 0.0000000	0.0088498	-8.6923075	0.4228567 0.0748634 0.4234581	1 0.4234581 1.9447727	347 0.0056045 75.5563660	$60^\circ \geq \delta > 30^\circ$
Gr 5.0875 0.2744159	-0.1017380 0.0042700 -0.0226384	0.0095293 0.0047465 0.0085158	-10.6763926 0.8996150 -2.6584072	0.4246572 0.0923810 0.9838679	3 0.3279560 4.4719486	524 0.0085343 38.4281921	$30^\circ \geq \delta \geq 0^\circ$
Gr 5.0875 0.2740638	-0.0979348 -0.0049666 0.0000000	0.0094755 0.0032524	-10.3355532 -1.5270653	0.4114354 0.0929133 0.9235558	2 0.4617779 4.5322609	525 0.0086329 53.4906158	$30^\circ \geq \delta \geq 0^\circ$
Gr 5.0875 0.2733610	-0.0963492 0.0000000 0.0000000	0.0094304	-10.2168932	0.4069267 0.0930308 0.9034251	1 0.9034251 4.5523920	526 0.0086547 104.3850555	$30^\circ \geq \delta \geq 0^\circ$
Gr 5.0875 0.2698008	-0.0947868 0.0118403 -0.0258563	0.0106762 0.0048835 0.0088401	-8.8782911 2.4245663 -2.9248981	0.4058741 0.0851141 0.5829369	3 0.1943123 2.9557238	408 0.0072444 26.8223267	$0^h \leq \alpha < 8^h$
Gr 5.0875 0.2677265	-0.0874684 0.0011565 0.0000000	0.0104743 0.0032711	-8.3507481 0.3535533	0.3836924 0.0858966 0.5209610	2 0.2604805 3.0176992	409 0.0073782 35.3038940	$0^h \leq \alpha < 8^h$
Gr 5.0875 0.2678323	-0.0877250 0.0000000 0.0000000	0.0104380	-8.4043770	0.3833527 0.0858049 0.5200391	1 0.5200391 3.0186214	410 0.0073625 70.6336060	$0^h \leq \alpha < 8^h$
Gr 4.8700 0.2594977	-0.0947223 -0.0060987 -0.0065643	0.0100477 0.0057020 0.0092716	-9.4272575 -1.0695753 -0.7080068	0.5206419 0.0778327 0.5722023	3 0.1907341 1.5387154	254 0.0060579 31.4850006	$8^h \leq \alpha < 16^h$
Gr 4.8700 0.2596654	-0.0949454 -0.0089950 0.0000000	0.0100329 0.0039683	-9.4633665 -2.2667093	0.5192586 0.0777565 0.5691658	2 0.2845829 1.5417519	255 0.0060461 47.0689697	$8^h \leq \alpha < 16^h$
Gr 4.8700 0.2595066	-0.0946422 0.0000000 0.0000000	0.0101128	-9.3586435	0.5048897 0.0783824 0.5381016	1 0.5381016 1.5728159	256 0.0061438 87.5843201	$8^h \leq \alpha < 16^h$
Gr 4.6556 0.2374913	-0.0798534 -0.0359377 0.0205326	0.0114764 0.0083898 0.0136696	-6.9580669 -4.2835140 1.5020618	0.4464106 0.0876074 0.5520393	3 0.1840131 2.2180948	289 0.0076751 23.9754333	$16^h \leq \alpha < 24^h$
Gr 4.6556 0.2368286	-0.0783065 -0.0266755 0.0000000	0.0114548 0.0057013	-6.8361254 -4.6788321	0.4393533 0.0877970 0.5347229	2 0.2673615 2.2354116	290 0.0077083 34.6847992	$16^h \leq \alpha < 24^h$

TABLE 3 (continued)

magnitude \bar{m} constant term	c o e f f i c i e n t s			R	k	n-k-1	Remarks
	Regression	St.deviation	T-values	e SSAR	SSAR/k SSDR	SSDR/n-k-1 F	
Gr 4.6556 0.2371284	-0.0789235 0.0000000 0.0000000	0.0118581	- 6.6556711	0.3634765 0.0908939 0.3659769	1 0.3659769 2.4041576	291 0.0082617 44.2979736	$16^h \leq \alpha < 24^h$
Gr 1 4.9220 0.2481148	-0.0758128 0.0026033 -0.0127353	0.0073206 0.0040113 0.0069350	-10.3560877 0.6489841 - 1.8363895	0.3192750 0.1001852 1.0925684	3 0.3641894 9.6255655	959 0.0100371 36.2843781	All
Gr 1 4.9220 0.2479447	-0.0748610 -0.0028123 0.0000000	0.0073112 0.0027225	-10.2391596 - 1.0329628	0.3142906 0.1003090 1.0587215	2 0.5293608 9.6594124	960 0.0100619 52.6104889	All
Gr 1 4.9220 0.2478009	-0.0745538 0.0000000 0.0000000	0.0073054	-10.2052326	0.3126931 0.1003124 1.0479870	1 1.0479870 9.6701469	961 0.0100626 104.1468658	All
Gr 1 4.6167 0.2383256	-0.0862661 -0.0230261 0.0157920	0.0190847 0.0157041 0.0240677	- 4.5201635 - 1.4662447 0.6561505	0.4595842 0.0821846 0.1483090	3 0.0494363 0.5538531	82 0.0067543 7.3192320	$90^\circ \geq \delta > 60^\circ$
Gr 1 4.6167 0.2370701	-0.0846733 -0.0150852 0.0000000	0.0188647 0.0099734	- 4.4884653 - 1.5125446	0.4550566 0.0819021 0.1454013	2 0.0727006 0.5567608	83 0.0067080 10.8379641	$90^\circ \geq \delta > 60^\circ$
Gr 1 4.6167 0.2361277	-0.0829052 0.0000000 0.0000000	0.0189722	- 4.3698292	0.4303727 0.0825275 0.1300550	1 0.1300550 0.5721071	84 0.0068108 19.0953979	$90^\circ \geq \delta > 60^\circ$
Gr 1 4.7592 0.2276730	-0.0521142 -0.0215516 0.0183626	0.0104153 0.0064450 0.0103235	- 5.0036087 - 3.3439198 1.7787142	0.3237085 0.0877279 0.3107970	3 0.1035990 2.6551847	345 0.0076962 13.4610853	$60^\circ \geq \delta > 30^\circ$
Gr 1 4.7592 0.2284314	-0.0519266 -0.0129394 0.0000000	0.0104473 0.0042671	- 4.9703350 - 3.0323429	0.3107696 0.0880018 0.2864479	2 0.1432239 2.6795340	346 0.0077443 18.4940643	$60^\circ \geq \delta > 30^\circ$
Gr 1 4.7592 0.2298341	-0.0548433 0.0000000 0.0000000	0.0105251	- 5.2107420	0.2693864 0.0890349 0.2152384	1 0.2152384 2.7507439	347 0.0079272 27.1518250	$60^\circ \geq \delta > 30^\circ$
Gr 1 5.0799 0.2610653	-0.0895429 0.0121030 -0.0283964	0.0111453 0.0055021 0.0098643	- 8.0341539 2.1996984 - 2.8787155	0.3397979 0.1081358 0.7998268	3 0.2666089 6.1273232	524 0.0116934 22.8000183	$30^\circ \geq \delta \geq 0^\circ$
Gr 1 5.0799 0.2605759	-0.0847991 0.0005618 0.0000000	0.0110990 0.0037943	- 7.6402349 0.1480532	0.3185495 0.1088837 0.7029243	2 0.3514621 6.2242260	525 0.0118557 29.6450653	$30^\circ \geq \delta \geq 0^\circ$
Gr 1 5.0799 0.2606525	-0.0849721 0.0000000 0.0000000	0.0110271	- 7.7057543	0.3184907 0.1087824 0.7026650	1 0.7026650 6.2244854	526 0.0118336 59.3787079	$30^\circ \geq \delta \geq 0^\circ$
Gr 2 4.9269 0.2668666	-0.1060036 0.0039368 -0.0128194	0.0080331 0.0044123 0.0076645	-13.1959352 0.8922178 - 1.6725721	0.3922880 0.1097254 2.0999851	3 0.6999950 11.5460434	959 0.0120397 58.1407166	All
Gr 2 4.9269 0.2666651	-0.1048180 -0.0015114 0.0000000	0.0080092 0.0029791	-13.0872002 - 0.5073224	0.3891295 0.1098281 2.0663052	2 1.0331526 11.5797234	960 0.0120622 85.6520081	All
Gr 2 4.9269 0.2665668	-0.1046075 0.0000000 0.0000000	0.0079953	-13.0835476	0.3888373 0.1097856 2.0632038	1 2.0632038 11.5828247	961 0.0120529 171.1792297	All
Gr 2 4.6033 0.2246682	-0.0854833 -0.0179449 0.0210174	0.0207821 0.0168053 0.0254932	- 4.1133060 - 1.0678110 0.8244316	0.4161116 0.0893557 0.1371045	3 0.0457015 0.6547252	82 0.0079845 5.7238092	$90^\circ \geq \delta > 60^\circ$
Gr 2 4.6033 0.2228612	-0.0831022 -0.0073341 0.0000000	0.0205407 0.0107851	- 4.0457296 - 0.6800187	0.4077932 0.0891832 0.1316775	2 0.0658388 0.6601521	83 0.0079536 8.2778139	$90^\circ \geq \delta > 60^\circ$
Gr 2 4.6033 0.2224057	-0.0822475 0.0000000 0.0000000	0.0204365	- 4.0245352	0.4020579 0.0888973 0.1279997	1 0.1279997 0.6638300	84 0.0079027 16.1968689	$90^\circ \geq \delta > 60^\circ$
Gr 2 4.7553 0.2480945	-0.1014931 -0.0073716 0.0058723	0.0113312 0.0069946 0.0113055	- 8.9569225 - 1.0538988 0.5194240	0.4417027 0.0955573 0.7636011	3 0.2545337 3.1502686	345 0.0091312 27.8751221	$60^\circ \geq \delta > 30^\circ$

TABLE 3 (continued)

magnitude \bar{m} constant term	c o e f f i c i e n t s			R e	k	n-k-1	Remarks
	Regression	St.deviation	T-values	SSAR	SSAR/k SSDR	SSDR/n-k-1 F	
Gr 2 4.7553 0.2483979	-0.1016786 -0.0046337 0.0000000	0.0113137 0.0045931	- 8.9872437 - 1.0088387	0.4409899 0.0954564 0.7611384	2 0.3805692 3.1527309	346 0.0091119 41.7659912	60° ≥ δ > 30°
Gr 2 4.7553 0.2487940	-0.1025023 0.0000000 0.0000000	0.0112844	- 9.0835047	0.4382952 0.0954589 0.7518650	1 0.7518650 3.1620045	347 0.0091124 82.5100708	60° ≥ δ > 30°
Gr 2 5.0934 0.2842091	-0.1106308 0.0056593 -0.0225784	0.0122242 0.0061078 0.0109867	- 9.0501575 0.9265751 - 2.0550604	0.3686136 0.1184254 1.1555481	3 0.3851827 7.3488855	524 0.0140246 27.4647980	30° ≥ δ ≥ 0°
Gr 2 5.0934 0.2838825	-0.1068059 -0.0035561 0.0000000	0.0121187 0.0041595	- 8.8133221 - 0.8549375	0.3590425 0.1187884 1.0963192	2 0.5481596 7.4081144	525 0.0141107 38.8471069	30° ≥ δ ≥ 0°
Gr 2 5.0934 0.2833647	-0.1056376 0.0000000 0.0000000	0.0120383	- 8.7751198	0.3573498 0.1187580 1.0860062	1 1.0860062 7.4184275	526 0.0141035 77.0027466	30° ≥ δ ≥ 0°

TABLE 4
HARVARD STATISTICAL RESULTS WITH B-V

magnitude m constant term	c o e f f i c i e n t s			R	k	n-k-1	Remarks
	Regression	St.deviation	T-values	e SSAR	SSAR/k SSDR	SSDR/n-k-1 F	
mag. 4.4738 0.0446407	0.0816938 -0.0355761 0.0250484	0.0044039 0.0032277 0.0040926	18.5504913 -11.0221176 6.1204557	0.4716160 0.1052753 4.9581919	3 1.6527300 17.3336487	1564 0.0110829 149.1243896	All
mag. 4.4738 0.0455641	0.0816497 -0.0237199 0.0000000	0.0044549 0.0026117 0.0000000	18.3282318 -9.0822830 -	0.4514397 0.1064945 4.5430326	2 2.2715158 17.7488098	1565 0.0113411 200.2907562	All
mag. 4.4738 0.0467664	0.0793216 0.0000000 0.0000000	0.0045617	17.3885040	0.4022832 0.1092302 3.6075306	1 3.6075306 18.6843109	1566 0.0119312 302.3601074	All
m14 4.3936 0.0362354	0.0972393 -0.0601788 0.0815993	0.0081447 0.0067049 0.0082163	11.9389124 -8.9753389 9.9313564	0.4015818 0.1686599 6.7275095	3 2.2425032 34.9888153	1230 0.0284462 78.8331604	All
m14 4.3936 0.0403886	0.0925792 -0.0165692 0.0000000	0.0084475 0.0052641 0.0000000	10.9593563 -3.1476164 -	0.3066126 0.1752207 3.9218073	2 1.9609032 37.7945251	1231 0.0307023 63.8682861	All
m14 4.3936 0.0408910	0.0916398 0.0000000 0.0000000	0.0084727	10.8158903	0.2944822 0.1758530 3.6176300	1 3.6176300 38.0987091	1232 0.0309243 116.9834900	All
m23 4.1182 -0.0022339	0.1274304 0.0032835 -0.0052077	0.0181564 0.0156581 0.0187754	7.0184832 0.2096996 -0.2773681	0.5023457 0.1450613 1.0795794	3 0.3598598 3.1985064	152 0.0210428 17.1013184	All
m23 4.1182 -0.0022645	0.1266198 0.0010589 0.0000000	0.0178655 0.0134074 0.0000000	7.0874014 0.0789818 -	0.5019692 0.1446230 1.0779619	2 0.5389810 3.2001238	153 0.0209158 25.7690277	All
m23 4.1182 -0.0023708	0.1268292 0.0000000 0.0000000	0.0176107	7.2018433	0.5019390 0.1441557 1.0778322	1 1.0778322 3.2002535	154 0.0207809 51.8665619	All
m24,1 4.8408 0.0402749	0.1266887 -0.0074713 -0.0143409	0.0171566 0.0113668 0.0151560	7.3842640 -0.6572884 -0.9462206	0.4525401 0.1487510 1.2536497	3 0.4178832 4.8679123	220 0.0221269 18.8857727	All
m24,1 4.8408 0.0398607	0.1265032 -0.0141331 0.0000000	0.0171514 0.0089218 0.0000000	7.3756819 -1.5841017 -	0.4489504 0.1487158 1.2338400	2 0.6169200 4.8877220	221 0.0221164 27.8942413	All
m24,1 4.8408 0.0406621	0.1250008 0.0000000 0.0000000	0.0171833	7.2745657	0.4387374 0.1492205 1.1783419	1 1.1783419 4.9432201	222 0.0222668 52.9193268	All
m24,4 4.4626 0.0698280	0.1163110 -0.0161523 0.0115024	0.0153949 0.0104375 0.0131208	7.5551682 -1.5475149 0.8766491	0.3394598 0.2047812 2.4905386	3 0.8301795 19.1225281	456 0.0419354 19.7966309	All
m24,4 4.4626 0.0699858	0.1171484 -0.0110468 0.0000000	0.0153613 0.0086595 0.0000000	7.6261892 -1.2756834 -	0.3372564 0.2047294 2.4583120	2 1.2291555 19.1547546	457 0.0419141 29.3255615	All
m24,4 4.4626 0.0707636	0.1156684 0.0000000 0.0000000	0.0153279	7.5462437	0.3325447 0.2048695 2.3901024	1 2.3901024 19.2229614	458 0.0419715 56.9457855	All
m34 4.0850 0.1265392	-0.1460626 -0.0175633 0.0568282	0.0170937 0.0130646 0.0171892	-8.5448065 -1.3443432 3.3060398	0.4787036 0.1846071 2.8671541	3 0.9557180 9.6445808	283 0.0340798 28.0435333	All
m34 4.0850 0.1277331	-0.1462487 0.0030669 0.0000000	0.0173899 0.0116769 0.0000000	-8.4099770 0.2626497 -	0.4465267 0.1878067 2.4946661	2 1.2473326 10.0170689	284 0.0352714 35.3638763	All
m34 4.0850 0.1276695	-0.1461012 0.0000000 0.0000000	0.0173524	-8.4196472	0.4463091 0.1874997 2.4922352	1 2.4922352 10.0194998	285 0.0351561 70.8904572	All

TABLE 4 (continued)

magnitude \bar{m} constant term	c o e f f i c i e n t s			R	k	n-k-1	Remarks
	Regression	St.deviation	T-values	SSAR	SSAR/k SSDR	SSDR/n-k-1 F	
m44 4.4233 0.0178766	0.1277478 -0.0387526 0.0605181	0.0093305 0.0074479 0.0091223	13.6914835 - 5.2031384 6.6341181	0.3742881 0.2117326 10.3491678	3 3.4497223 63.5251160	1417 0.0448307 76.9499664	All
m44 4.4233 0.0205491	0.1274801 -0.0080819 0.0000000	0.0094708 0.0059272 0.0000000	13.4603004 - 1.3635225 0.0000000	0.3367242 0.2149198 8.3761063	2 4.1880531 65.4981842	1418 0.0461905 90.6690674	All
m44 4.4233 0.0210381	0.1265532 0.0000000 0.0000000	0.0094493 0.0000000 0.0000000	13.3929319 0.0000000 0.0000000	0.3349937 0.2149848 8.2902346	1 8.2902346 65.5840607	1419 0.0462185 179.3704529	All
m44 4.4198 0.0206101	0.1205688 0.0000000 0.0026340	0.0075158 0.0000000 0.0058575	16.0420380 0.0000000 0.4496894	0.3926830 0.1708631 7.5472631	2 3.7736311 41.3973846	1418 0.0291942 129.2595825	All
m44 4.4061 0.0167984	0.1522386 -0.0312699 0.0125538	0.0243130 0.0220753 0.0246560	6.2616186 - 1.4165087 0.5091582	0.5740144 0.1302533 0.7169989	3 0.2389996 1.4590712	86 0.0169659 14.0870228	90° ≥ δ > 60°
m44 4.4061 0.0163985	0.1544827 -0.0232988 0.0000000	0.0238082 0.0154973 0.0000000	6.4886389 - 1.5034161 0.0000000	0.5722513 0.1296976 0.7126009	2 0.3563005 1.4634686	87 0.0168215 21.1812744	90° ≥ δ > 60°
m44 4.4061 0.0198454	0.1489690 0.0000000 0.0000000	0.0236919 0.0000000 0.0000000	6.2877712 0.0000000 0.0000000	0.5567759 0.1306230 0.6745805	1 0.6745805 1.5014896	88 0.0170624 39.5361176	90° ≥ δ > 60°
m44 4.0790 0.0277839	0.1410763 -0.0291473 0.0060222	0.0177875 0.0166654 0.0202149	7.9311953 - 1.7489700 0.2979083	0.7670661 0.0712443 0.3337635	3 0.1112545 0.2334849	46 0.0050758 21.9187775	Circumpolar
m44 4.0790 0.0278383	0.1415125 -0.0255557 0.0000000	0.0175545 0.0113937 0.0000000	8.0613308 - 2.2429638 0.0000000	0.7665485 0.0705503 0.3333132	2 0.1666566 0.2339352	47 0.0049773 33.4830475	Circumpolar
m44 4.0790 0.0303166	0.1373941 0.0000000 0.0000000	0.0181765 0.0000000 0.0000000	7.5589018 0.0000000 0.0000000	0.7371927 0.0734528 0.3082728	1 0.3082728 0.2589756	48 0.0053953 57.1370392	Circumpolar
m44 4.4740 -0.0006065	0.1337823 -0.0141670 0.0585079	0.0160213 0.0130235 0.0160870	8.3502865 - 1.0878019 3.6369591	0.4767513 0.1666980 2.5420847	3 0.8473616 8.6421480	311 0.0277883 30.4934998	60° ≥ δ > 30°
m44 4.4740 0.0014660	0.1355975 0.0172378 0.0000000	0.0163243 0.0099385 0.0000000	8.3064909 1.7344379 0.0000000	0.4409387 0.1599332 2.1745148	2 1.0872574 9.0097179	312 0.0288773 37.6509247	60° ≥ δ > 30°
m44 4.4740 0.0000281	0.1382075 0.0000000 0.0000000	0.0163068 0.0000000 0.0000000	8.4754267 0.0000000 0.0000000	0.4320415 0.1704774 2.0876474	1 2.0876474 9.0965853	313 0.0290626 71.8328552	60° ≥ δ > 30°
m44 4.5387 -0.0195971	0.1523920 -0.0130146 -0.0046693	0.0100902 0.0080093 0.0093265	15.1029148 - 1.6249475 - 0.5006431	0.5909769 0.1241758 3.6330252	3 1.2110081 6.7692270	439 0.0154197 78.5366669	30° ≥ δ > 0°
m44 4.5387 -0.0197245	0.1525674 -0.0157642 0.0000000	0.0100756 0.0058247 0.0000000	15.1423149 - 2.7064524 0.0000000	0.5906627 0.1240700 3.6291628	2 1.8145809 6.7730894	440 0.0153934 117.8805695	30° ≥ δ > 0°
m44 4.5387 -0.0195630	0.1522744 0.0000000 0.0000000	0.0101470 0.0000000 0.0000000	15.0068779 0.0000000 0.0000000	0.5814147 0.1249566 3.5164080	1 3.5164080 6.8858442	441 0.0156142 225.2064056	30° ≥ δ > 0°
m44 4.3741 0.0311508	0.1331332 -0.0727668 0.0266989	0.0146592 0.0112615 0.0156561	9.0819130 - 6.4615803 1.7053394	0.4877893 0.1770144 3.7764072	3 1.2588024 12.0949564	386 0.0313341 40.1735687	0° ≥ δ > -30°
m44 4.3741 0.0323045	0.1325352 -0.0631118 0.0000000	0.0146910 0.0097588 0.0000000	9.0214977 - 6.4671745 0.0000000	0.4818683 0.1774502 3.6852846	2 1.8426418 12.1860790	387 0.0314886 58.5177765	0° ≥ δ > -30°
m44 4.3741 0.0350358	0.1272068 0.0000000 0.0000000	0.0154203 0.0000000 0.0000000	8.2493114 0.0000000 0.0000000	0.3862878 0.1865522 2.3682966	1 2.3682966 13.5030670	388 0.0348017 68.0511322	0° ≥ δ > -30°
m44 4.1460 0.0927031	0.0242598 -0.0525743 0.0539674	0.0239798 0.0209877 0.0254227	1.0116758 - 2.5050039 2.1228027	0.2118262 0.2092150 0.3660185	3 0.1220061 7.7912264	178 0.0437709 2.7873774	-30° ≥ δ
m44 4.1460 0.0947644	0.0271360 -0.0320897 0.0000000	0.0241748 0.0188194 0.0000000	1.1224909 - 1.7051382 0.0000000	0.1438403 0.2112542 0.1687737	2 0.0843868 7.9884710	179 0.0446283 1.8908796	-30° ≥ δ

TABLE 4 (continued)

magnitude \bar{m} constant term	c o e f f i c i e n t s			R	k	n-k-1	Remarks
	Regression	St.deviation	T-values	ϵ SSAR	SSAR/k SSDR	SSDR/n-k-1 F	
m44 4.1460 0.0968485	0.0224580 0.0000000 0.0000000	0.0241456	0.9301078	0.0691601 0.2123706 0.0390171	1 0.0390171 8.1182280	180 0.0451013 0.8651009	-30° $\geq \delta$
m44 4.4098 -0.0016994	0.1611903 -0.0333705 0.1283482	0.0363238 0.0296673 0.0369268	4.4375896 -1.1248255 3.4757462	0.4790736 0.2128101 1.4839373	3 0.4946457 4.9816980	110 0.0452882 10.9221859	60° $\geq \delta$ and $>30^\circ$ $0^h \leq \alpha < 8^h$
m44 4.4098 0.0047001	0.1472393 0.0417392 0.0000000	0.0378605 0.0213170	3.8889952 1.9580202	0.3806470 0.2231796 0.9368198	2 0.4684099 5.5288153	111 0.0498091 9.4040937	60° $\geq \delta$ and $>30^\circ$ $0^h \leq \alpha < 8^h$
m44 4.4098 0.0050783	0.1465003 0.0000000 0.0000000	0.0383346	3.8216228	0.3396432 0.2259854 0.7458596	1 0.7458596 5.7197752	112 0.0510694 14.6048183	60° $\geq \delta$ and $>30^\circ$ $0^h \leq \alpha < 8^h$
m44 4.4537 -0.0293801	0.1266763 -0.0447870 0.0507984	0.0222886 0.0156678 0.0207677	5.6834459 -2.8585358 2.4460249	0.5891012 0.1116531 0.5234351	3 0.1744784 0.9848486	79 0.0124664 13.9958496	60° $\geq \delta$ and $>30^\circ$ $8^h \leq \alpha < 16^h$
m44 4.4537 0.0260652	0.1326786 -0.0229003 0.0000000	0.0228327 0.0132559	5.8109131 -1.7275524	0.5455167 0.1150780 0.4488478	2 0.2244239 1.0594358	80 0.0132429 16.9466705	60° $\geq \delta$ and $>30^\circ$ $8^h \leq \alpha < 16^h$
m44 4.4537 -0.0206969	0.1232980 0.0000000 0.0000000	0.0224476	5.4927025	0.5209461 0.1164791 0.4093252	1 0.4093252 1.0989580	81 0.0135674 30.1697998	60° $\geq \delta$ and $>30^\circ$ $8^h \leq \alpha < 16^h$
m44 4.5505 0.0110423	0.1384385 0.0161710 0.0101836	0.0199659 0.0177867 0.0212851	6.9337511 0.9091587 0.4784395	0.5671611 0.1363302 1.0047588	3 0.3349196 2.1187973	114 0.0185859 18.0200500	60° $\geq \delta$ and $>30^\circ$ $16^h \leq \alpha < 24^h$
m44 4.5505 0.0110443	0.1392719 0.0217668 0.0000000	0.0198230 0.0133555	7.0257797 1.6298056	0.5659592 0.1358724 1.0005054	2 0.5002527 2.1230507	115 0.0184613 27.0973511	60° $\geq \delta$ and $>30^\circ$ $16^h \leq \alpha < 24^h$
m44 4.5505 0.0095518	0.1418544 0.0000000 0.0000000	0.01999001	7.1283197	0.5519153 0.1368389 0.9514681	1 0.9514681 2.1720877	116 0.0187249 50.8130035	60° $\geq \delta$ and $>30^\circ$ $16^h \leq \alpha < 24^h$
m44 3.8315 0.0517263	0.0942457 -0.0555890 0.0595430	0.0434692 0.0237354 0.0329106	2.1681032 -2.3420258 1.8092299	0.2253903 0.2602366 0.5726737	3 0.1908912 10.7002544	158 0.0677231 2.8187008	Ap.J. 117 313, 1953.
m44 3.8315 0.0626799	0.0784354 -0.0246236 0.0000000	0.0428851 0.0165622	1.8289671 -1.4867344	0.1764541 0.2620904 0.3509946	2 0.1754973 10.9219332	159 0.0686914 2.5548658	Ap.J. 117 313, 1953.
m44 3.8315 0.0654739	0.0727295 0.0000000 0.0000000	0.0428743	1.6963434	0.1329179 0.2630798 0.1991608	1 0.1991608 11.0737667	160 0.0692110 2.8775883	Ap.J. 117 313, 1953.
m45 4.5583 -0.0007195	0.1490987 -0.0370624 0.0505635	0.0114708 0.0088710 0.0113166	12.9981136 -4.1779346 4.4680624	0.4427006 0.1914971 6.9275808	3 2.3091936 28.4201355	775 0.0366711 62.9703217	All
m45 4.5583 0.0012462	0.1485658 -0.0127588 0.0000000	0.0116095 0.0070928	12.7969408 -1.7988510	0.4186561 0.1938227 6.1954975	2 3.0977488 29.1522064	776 0.0375673 82.4586945	All
m45 4.5583 0.0018693	0.1473819 0.0000000 0.0000000	0.0116075	12.6971569	0.4145285 0.1941015 6.0739365	1 6.0739365 29.2737732	777 0.0376754 161.2176514	All
m46 4.2328 0.1907595	-0.1133281 -0.0398831 0.0277343	0.0125216 0.0098137 0.0122424	-9.0506306 -4.0640421 2.2654371	0.3928292 0.1881546 3.6240311	3 1.2080097 19.8606262	561 0.0354022 34.1224518	All
m46 4.2328 0.1917139	-0.1133202 -0.0286130 0.0000000	0.0125675 0.0084903	-9.0169106 -3.3700781	0.3828553 0.1888451 3.4423389	2 1.7211695 20.0423126	562 0.0356625 48.2627563	All
m46 4.2328 0.1929229	-0.1157849 0.0000000 0.0000000	0.0126611	-9.1449280	0.3596271 0.1905742 3.0373096	1 3.0373096 20.4473419	563 0.0363185 83.6297150	All

TABLE 5
HARVARD STATISTICAL RESULTS WITH V-R

magnitude \bar{m} constant term	c o e f f i c i e n t s			R	k	n-k-1	Remarks
	Regression	St.deviation	T-values	ϵ SSAR	SSAR/k SSDR	SSDR/n-k-1 F	
mag. 4.4738 0.0430203	0.0990831 -0.0337070 0.0220896	0.0057467 0.0033781 0.0051564	17.2418365 - 9.9779587 4.2838888	0.4461738 0.1068444 4.4376621	3 1.4792204 17.8541870	1564 0.0114157 129.5774841	All
mag. 4.4738 0.0432750	0.1004046 -0.0245934 0.0000000	0.0057701 0.0026386 ?	17.4008484 - 9.3205462	0.4355147 0.1074350 4.2281656	2 2.1140823 18.0636749	1565 0.0115423 183.1598053	All
mag. 4.4738 0.0451663	0.0961553 0.0000000 0.0000000	0.0059077	16.2763519	0.3803843 0.1103413 3.2254581	1 3.2254581 19.0663910	1566 0.0121752 264.9199219	All
m14 4.3936 0.0341217	0.1169004 -0.0613095 0.0962148	0.0106801 0.0070395 0.0106841	10.9456129 - 8.7093897 9.0053883	0.3778934 0.1705064 5.9572382	3 1.9857454 35.7590942	1230 0.0290724 68.3033752	All
m14 4.3936 0.0375835	0.1148823 -0.0178867 0.0000000	0.0110197 0.0052929	10.4251986 - 3.3793497	0.2937455 0.1759661 3.5995531	2 1.7997761 38.1167755	1231 0.0309641 58.1246490	All
m14 4.3936 0.0386231	0.1126176 0.0000000 0.0000000	0.0110457	10.1956024	0.2789445 0.1767086 3.2459497	1 3.2459497 38.4703827	1232 0.0312260 103.9503632	All
m23 4.1182 -0.0109923	0.1693227 0.0005197 -0.0072380	0.0232387 0.0160034 0.0245401	7.2862463 0.0324762 - 0.2949481	0.5200932 0.1432902 1.1572094	3 0.3857365 3.1208763	152 0.0205321 18.7870026	All
m23 4.1182 -0.0108842	0.1677691 -0.0020872 0.0000000	0.0225661 0.0133014	7.4345675 - 0.1569127	0.5196922 0.1428620 1.1554251	2 0.5777125 3.1226606	153 0.0204095 28.3059998	All
m23 4.1182 -0.0106161	0.1671518 0.0000000 0.0000000	0.0221499	7.5463934	0.5195793 0.1424088 1.1549225	1 1.1549225 3.1231632	154 0.0202803 56.9480438	All
m24,1 4.8408 0.0329626	0.1648638 -0.0088190 -0.0162911	0.0225868 0.0121819 0.0206923	7.2991180 - 0.7239451 - 0.7872994	0.4479323 0.1491386 1.2282505	3 0.4094168 4.8933115	220 0.0222423 18.4071045	All
m24,1 4.8408 0.0324091	0.1647758 -0.0153186 0.0000000	0.0225671 0.0089502	7.3015938 - 1.7115240	0.4454114 0.1490102 1.2144642	2 0.6072321 4.9070978	221 0.0222041 27.3477936	All
m24,1 4.8408 0.0337061	0.1619247 0.0000000 0.0000000	0.0226031	7.1638231	0.4333202 0.1496563 1.1494236	1 1.1494236 4.9721384	222 0.0223970 51.3203735	All
m24,4 4.4626 0.0623574	0.1527244 -0.0204077 0.0218614	0.0205485 0.0110617 0.0178778	7.4323902 - 1.8448906 1.2228251	0.3360683 0.2050462 2.4410210	3 0.8136736 19.1720428	456 0.0420440 19.3529205	All
m24,4 4.4626 0.0629395	0.1537438 -0.0120302 0.0000000	0.0205427 0.0086896	7.4841089 - 1.3844442	0.3317124 0.2051573 2.3781519	2 1.1890755 19.2349091	457 0.0420895 28.2510986	All
m24,4 4.4626 0.0641052	0.1511327 0.0000000 0.0000000	0.0204764	7.3808260	0.3260378 0.2053625 2.2974825	1 2.2974825 19.3155823	458 0.0421738 54.4765778	All
m34 4.0850 0.1298152	-0.1755728 -0.0161492 0.0535922	0.0222443 0.0138291 0.0219309	- 7.8929501 - 1.1677713 2.4436836	0.4434850 0.1884560 2.4607954	3 0.8202651 10.0509396	283 0.0355157 23.0958405	All
m34 4.0850 0.1308556	-0.1769443 0.0018137 0.0000000	0.0224310 0.0118158	- 7.8883867 0.1535000	0.4239438 0.1900983 2.2487125	2 1.1243563 10.2630224	284 0.0361374 31.1133575	All
m34 4.0850 0.1308292	-0.1768734 0.0000000 0.0000000	0.0223878	- 7.9004469	0.4238637 0.1897724 2.2478638	1 2.2478638 10.2638712	285 0.0360136 62.4170990	All

TABLE 5 (continued)

magnitude \bar{m} constant term	c o e f f i c i e n t s			R	k	n-k-1	Remarks
	Regression	St.deviation	T-values	ϵ SSAR	SSAR/k SSDR	SSDR/n-k-1 F	
m44 4.4233 0.0139017	0.1587157 -0.0380160 0.0674292	0.0122650 0.0078408 0.0120177	12.9405537 - 4.8485117 5.6108322	0.3511269 0.2137911 9.1079712	3 3.0359898 64.7663269	1417 0.0457067 66.4233551	All
m44 4.4233 0.0165160	0.1587964 -0.0090651 0.0000000	0.0123961 0.0059668 0.0000000	12.8101950 - 1.5192509 0.0000000	0.3221993 0.2160767 7.6690674	2 3.8345337 66.2052307	1418 0.0466892 82.1289825	All
m44 4.4233 0.0172606	0.1571434 0.0000000 0.0000000	0.0123539 0.0000000 0.0000000	12.7201014 0.0000000 0.0000000	0.3199277 0.2161763 7.5613108	1 7.5613108 66.3129730	1419 0.0467322 161.8009186	All
m44 4.4198 0.0164627	0.1514186 0.0000000 -0.0031665	0.0098452 0.0073660 0.0073660	15.3799362 - 0.4298800 0.0000000	0.3782585 0.1719826 7.0029774	2 3.5014887 41.9416656	1418 0.0295780 118.3813477	All
m44 4.4061 0.0124233	0.1865142 -0.0353776 0.0191109	0.0321089 0.0240626 0.0353637	5.8088007 - 1.4702282 0.5404109	0.5588301 0.1319135 0.6795673	3 0.2265224 1.4965029	86 0.0174012 13.0176325	$90^\circ \geq \delta > 60^\circ$
m44 4.4061 0.0112663	0.1913525 -0.0255865 0.0000000	0.0307098 0.0157706 0.0000000	6.2309999 - 1.6224127 0.0000000	0.5567368 0.1313757 0.6744857	2 0.3372428 1.5015841	87 0.0172596 19.5394440	$90^\circ \geq \delta > 60^\circ$
m44 4.4061 0.0160573	0.1823390 0.0000000 0.0000000	0.0304818 0.0000000 0.0000000	5.9818878 0.0000000 0.0000000	0.5376603 0.1325884 0.6290553	1 0.6290553 1.5470142	88 0.0175797 35.7830353	$90^\circ \geq \delta > 60^\circ$
m44 4.0790 0.0272304	0.1656370 -0.0232328 -0.0140430	0.0244195 0.0190605 0.0291874	6.7829895 - 1.2188988 - 0.4811311	0.7250238 0.0764808 0.2981795	3 0.0993931 0.2690689	46 0.0058493 16.9922485	Circumpolar
m44 4.0790 0.0282641	0.1618346 -0.0301766 0.0000000	0.0229155 0.0123483 0.0000000	7.0622435 - 2.4437733 0.0000000	0.7233762 0.0758529 0.2968258	2 0.1484129 0.2704226	47 0.0057537 25.7944641	Circumpolar
m44 4.0790 0.0330477	0.1526980 0.0000000 0.0000000	0.0237505 0.0000000 0.0000000	6.4292526 0.0000000 0.0000000	0.6802192 0.0796847 0.2624648	1 0.2624648 0.3047836	48 0.0063497 41.3352661	Circumpolar
m44 4.4740 -0.0005556	0.1545003 -0.0131829 0.0655214	0.0211232 0.0136980 0.0217170	7.3142576 - 0.9623964 3.0170593	0.4362562 0.1706395 2.1285772	3 0.7095257 9.0556555	311 0.0291179 24.3673706	$60^\circ \geq \delta > 30^\circ$
m44 4.4740 0.0006561	0.1599341 0.0149908 0.0000000	0.0213178 0.0101509 0.0000000	7.5023775 1.4767904 0.0000000	0.4081923 0.1728411 1.8635273	2 0.9317636 9.3207054	312 0.0298741 31.1897278	$60^\circ \geq \delta > 30^\circ$
m44 4.4740 -0.0012684	0.1640089 0.0000000 0.0000000	0.0211783 0.0000000 0.0000000	7.7441807 0.0000000 0.0000000	0.4009935 0.1731668 1.7983770	1 1.7983770 9.3858557	313 0.0299868 59.9723663	$60^\circ \geq \delta > 30^\circ$
m44 4.5387 -0.0261609	0.1950855 -0.0099201 -0.0127601	0.0131209 0.0082760 0.0118359	14.8682938 - 1.1986685 - 1.0780830	0.5863518 0.1246943 3.5763817	3 1.1921272 6.8258705	439 0.0155487 76.6706238	$30^\circ \geq \delta > 0^\circ$
m44 4.5387 -0.0264847	0.1955749 -0.0162264 0.0000000	0.0131155 0.0058555 0.0000000	14.9117708 - 2.7711439 0.0000000	0.5848686 0.1247173 3.5583115	2 1.7791557 6.8439407	440 0.0155544 114.3827209	$30^\circ \geq \delta > 0^\circ$
m44 4.5387 -0.0262112	0.1949882 0.0000000 0.0000000	0.0132127 0.0000000 0.0000000	14.7576342 0.0000000 0.0000000	0.5749685 0.1256582 3.4388676	1 3.4388676 6.9633846	441 0.0157900 217.7878723	$30^\circ \geq \delta > 0^\circ$
m44 4.3741 0.0232853	0.1726184 -0.0779173 0.0377193	0.0198281 0.0121581 0.0216588	8.7057371 - 6.4086924 1.7415228	0.4770344 0.1782154 3.6117172	3 1.2039051 12.2596464	386 0.0317607 37.9054413	$0^\circ \geq \delta > -30^\circ$
m44 4.3741 0.0248733	0.1720858 -0.0654361 0.0000000	0.0198778 0.0098469 0.0000000	8.6571999 - 6.6453428 0.0000000	0.4706301 0.1786829 3.5153904	2 1.7576952 12.3559732	387 0.0319276 55.0525665	$0^\circ \geq \delta > -30^\circ$
m44 4.3741 0.0298057	0.1608334 0.0000000 0.0000000	0.0208780 0.0000000 0.0000000	7.7034674 0.0000000 0.0000000	0.3642216 0.1883591 2.1054535	1 2.1054535 13.7659101	388 0.0354791 59.3433990	$0^\circ \geq \delta > -30^\circ$
m44 4.1460 0.0909044	0.0351991 -0.0544159 0.0652573	0.0307667 0.0216699 0.0316294	1.1440668 - 2.5111246 2.0631847	0.2072079 0.2094269 0.3502321	3 0.1167440 7.8070135	178 0.0438596 2.6617651	$-30^\circ \geq \delta$
m44 4.1460 0.0942119	0.0331565 -0.0315233 0.0000000	0.0310292 1.0685558 0.0000000	0.0187823 - 1.6783524 0.0000000	0.1415895 0.2113234 0.1635332	2 0.0817665 7.9937124	179 0.0446576 1.8309650	$-30^\circ \geq \delta$

TABLE 5 (continued)

magnitude \bar{m} constant term	c o e f f i c i e n t s			R	k	n-k-1	Remarks
	Regression	St.deviation	T-values	ϵ SSAR	SSAR/k SSDR	SSDR/n-k-1 F	
m44 4.1460 0.0960230	0.0284054 0.0000000 0.0000000	0.0310554	0.9146698	0.0680175 0.2123873 0.0377386	1 0.0377386 8.1195068	180 0.0451084 0.8366213	-30° $\geq \delta$
m44 4.4098 -0.0170431	0.2175205 -0.0516306 0.1916553	0.0496032 0.0318932 0.0514754	4.3852119 - 1.6188593 3.7232380	0.4867541 0.2117832 1.5318995	3 0.5106331 4.9337358	110 0.0448521 11.3848095	60° $\geq \delta > 30^\circ$ and $0^h \leq \alpha < 8^h$
m44 4.4098 -0.0080178	0.1986046 0.0401749 0.0000000	0.0521228 0.0213682	3.8103189 1.8801260	0.3751871 0.2237175 0.9101375	2 0.4550688 5.5554972	111 0.0500495 9.0923700	60° $\geq \delta > 30^\circ$ and $0^h \leq \alpha < 8^h$
m44 4.4098 -0.0084070	0.1994927 0.0000000 0.0000000	0.0527072	3.7849216	0.3367528 0.2262350 0.7332187	1 0.7332187 5.7324162	112 0.0511823 14.3256340	60° $\geq \delta > 30^\circ$ and $0^h \leq \alpha < 8^h$
m44 4.4537 -0.0294420	0.1515093 -0.0409782 0.0441291	0.0295513 0.0163745 0.0265411	5.1269875 - 2.5025654 1.6626673	0.5471142 0.1156600 0.4514804	3 0.1504934 1.0568027	79 0.0133772 11.2499542	60° $\geq \delta > 30^\circ$ and $8^h \leq \alpha < 16^h$
m44 4.4537 -0.0285641	0.1610432 -0.0255184 0.0000000	0.0293077 0.0136262	5.4949179 - 1.8727417	0.5242285 0.1169286 0.4144998	2 0.2072499 1.0937834	80 0.0136723 15.1583853	60° $\geq \delta > 30^\circ$ and $8^h \leq \alpha < 16^h$
m44 4.4537 -0.0210895	0.1456957 0.0000000 0.0000000	0.0285707	5.0994797	0.4929745 0.1187243 0.3665490	1 0.3665490 1.1417341	81 0.0140955 26.0046997	60° $\geq \delta > 30^\circ$ and $8^h \leq \alpha < 16^h$
m44 4.5505 0.0176581	0.1498117 0.0186831 0.0012553	0.0261860 0.0189396 0.0299737	5.7210569 0.9864537 0.0418806	0.4982430 0.1435192 0.7754107	3 0.2584702 2.3481445	114 0.0205978 12.5484657	60° $\geq \delta > 30^\circ$ and $16^h \leq \alpha < 24^h$
m44 4.5505 0.0176646	0.1499491 0.0192094 0.0000000	0.0258673 0.0141079	5.7968559 1.3616066	0.4982316 0.1428949 0.7753753	2 0.3876876 2.3481808	115 0.0204190 18.9866333	60° $\geq \delta > 30^\circ$ and $16^h \leq \alpha < 24^h$
m44 4.5505 0.0155297	0.1542808 0.0000000 0.0000000	0.0257653	5.9879351	0.4859171 0.1434199 0.7375199	1 0.7375199 2.3860359	116 0.0205693 35.8554077	60° $\geq \delta > 30^\circ$ and $16^h \leq \alpha < 24^h$
m44 3.8315 0.0501996	0.1143234 -0.0568402 0.0724885	0.0601714 0.0248197 0.0428494	1.8999624 - 2.2901278 1.6917019	0.2111738 0.2610860 0.5027091	3 0.1675697 10.7702188	158 0.0681659 2.4582624	Ap.J. 117 313, 1953.
m44 3.8315 0.0609974	0.0982581 -0.0256002 0.0000000	0.0597642 0.0166800	1.6440973 - 1.5347872	0.1651940 0.2626102 0.3076276	2 0.1538138 10.9653006	159 0.0689641 2.2303448	Ap.J. 117 313, 1953.
m44 3.8315 0.0660308	0.0859246 0.0000000 0.0000000	0.0594718	1.4447956	0.1134833 0.2637203 0.1451779	1 0.1451779 11.1277494	160 0.0695484 2.0874357	Ap.J. 117 313, 1953.
m45 4.5583 -0.0098989	0.1944848 -0.0386581 0.0582015	0.0149735 0.0092822 0.0145934	12.9885759 - 4.1647787 3.9882145	0.4402672 0.1917528 6.8516331	3 2.2838774 28.4960785	775 0.0367691 62.1139832	All
m45 4.5583 -0.0080720	0.1948001 -0.0144642 0.0000000	0.0151164 0.0070927	12.8866386 - 2.0393190	0.4210580 0.1935856 6.2667904	2 3.1333952 29.0809174	776 0.0374754 83.6120300	All
m45 4.5583 -0.0070334	0.1924896 0.0000000 0.0000000	0.0151045	12.7438307	0.4157894 0.1939787 6.1109447	1 6.1109447 29.2367706	777 0.0376278 162.4052124	All
m46 4.2328 0.1936610	-0.1401108 -0.0424979 0.0392261	0.0161185 0.0100332 0.0139145	- 8.6925707 - 4.2357025 2.8190804	0.3791838 0.1893229 3.3766346	3 1.1255445 20.1080170	561 0.0358432 31.4019165	All
m46 4.2328 0.1929486	-0.1350956 -0.0275712 0.0000000	0.0161187 0.0085749	- 8.3813047 - 3.2153511	0.3628376 0.1904895 3.0917826	2 1.5458908 20.3928680	562 0.0362862 42.6026611	All
m46 4.2328 0.1946171	-0.1390597 0.0000000 0.0000000	0.0162042	- 8.5816927	0.3401136 0.1920628 2.7166424	1 2.7166424 20.7680206	563 0.0368881 73.6454163	All

V. Conclusion

Tables 2–5 indicate that the visual photometries of Potsdam and Harvard can be transformed to the BVR–system satisfactorily. For Potsdam the standard errors, ϵ , are smaller than ± 0.1 , while for Harvard they are between ± 0.1 and ± 0.2 (see column 5 in Tables 2–5). The resulting equations depend strongly on the color of the stars (B–V or V–R). The dependence on Pogson scale deviations and Purkinje effect is not large.

It is well known that Potsdam photometry covers a smaller area of the sky than that of Harvard, and that the latter was made with more observers than the former. The consequence of this is that the results for Potsdam are more uniform than for Harvard. Nevertheless, some Harvard results are very good, per example those for m44 –circumpolar stars.

The regression coefficients which describe the Pogson scale deviations and the Purkinje effect listed in Tables 2–5 (column 2, lines 2 and 3) are present with different stages of significance. For instance, in the Potsdam photometry if the sample contains all stars listed in Table 1, column 6 (magnitude “Gr”), then the Pogson scale deviation coefficient is practically zero, while the Purkinje effect coefficient is not zero. If in the last sample we only include those stars with declination between 30° and 60° , then the Pogson scale deviation coefficient is not zero and the Purkinje effect coefficient is nearly zero. Both coefficients are not zero if the sample contains only stars with right ascension between 16 and 24 hours. In Harvard photometry the same phenomenon is also present. Both coefficients are not zero in the systems “mag”, “m14”, “m44”, and “m46”. Both coefficients are very small in the system “m23”. Only one of them is practically zero in the systems “m34” and “m45”. Individual systems like “m44” when divided in groups also present the above combinations.

Rybka (1960) and Winiarski (1963) in their work on systematic differences in Harvard and Potsdam photometries have constructed diagrams which plot the residuals (observed minus computed values) versus magnitudes and colors. The Burroughs 5500 computer of the University of Mexico has been used to construct similar diagrams. The program was made with the help of Mr. Cruz. A copy of this program (in Algol language) is given in Appendix II. Of the 420 Figures obtained we have selected only 48 for publication. Instructions to read these graphs are given in Appendix III. No deviation from linear dependence on colors may be inferred from the diagrams. However, in those in which the computations were made with the Pogson scale deviation equal to zero and those with also the Purkinje effect coefficient equal to zero show a tendency of more positive residuals for the brightest stars and of more negative residuals for the faintest stars. This effect may be also present in most of the Potsdam magnitude *vs* residuals plots, while it is almost unnoticeable on those with all the regression coefficients different from zero. In this respect Harvard photometry is better than that of Potsdam. Harvard visual photometry has a zero point closer to the BVR system than Potsdam’s, and perhaps the results obtained with B–V are slightly better than those with V–R.

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APPENDIX I

MULTIPLE REGRESSION ANALYSIS PROGRAM

```

DIMENSION RX (100), R (55), AB (10), ANS (10), B (10), IKA (10), ISA (10), ISAVE
I (10), D (10), RY (10), SB (10), STD (10), T (10), XBAR (10), W (10)
INTEGER U
COMMON X (10200)
PRINT 1401
1401 FORMAT ('0 PORCION DE LA MUESTRA ORIGINAL///)
      N = 0
      DO 972 I = 1,1700
      READ 81, X (I), X (I + 1700), X (I + 3400), X (I + 5100)
      IF (I - 50) 1217, 1217, 1218
1217 PRINT 81, X (I), X (I + 1700), X (I + 3400), X (I + 5100)
1218 IF (ABS (X (I) - 99.99) - 0.1) 991, 991, 990
      930 N = N + 1
      972 CONTINUE
      991 WRITE (3,993) N
      993 FORMAT ('NUMERO TOTAL DE TARJETAS LEIDAS, N = I4)
      S = 0.
      DO 973 I = 1, N
      973 S = S + X (I + 5100)
      RK = S/N
      WRITE (3,1901) RK
1901 FORMAT ('T. M. DE LECT. ANTIGUA, =', F10.4)
      DO 802 MS = 1, N
      X (MS) = X (MS + 5100) - X (MS)
      X (MS + 5100) = X (MS + 5100) - RK
      X (MS + 6800) = X (MS + 1700)* X (MS + 5100)
      802 X (MS + 8500) = X (MS + 3400)* X (MS + 5100)
      U = 11
      DO 801 MS = 1,4
      I1 = (MS - 1)* 1700 + 1
      I2 = I1 + N - 1
      REWIND U
      WRITE (U) (X (J), J = I1, I2)
      801 U = U + 1
      16 READ (1, 3) PR, PR1, PR2, NS
      3 FORMAT (3A4, I2)
      WRITE (3, 4) PR, PR1, PR2, NS
      4 FORMAT ('1 REGRESION MULTIPLE', 3A4//6X, 'SELECCION', I2//)
      IF (NS - 99) 17, 99, 17
      17 READ (1, 1) M, NOPC, NLIST, NCOMP, NCAM
      1 FORMAT (I4, 4I2)
      NOPC = NOPC + 1
      READ (1, 5) ISA (I), I = 1, M)
      5 FORMAT (40I2)
      KI = 0
      DO 750 I = 1, M
      MS = ISA (I)
      GO TO (701, 702, 703, 704, 705, 705), MS
      701 U = 11
      GO TO 707
      702 U = 12
      GO TO 707
      703 U = 13
      GO TO 707
      704 U = 14
      707 I1 = KI + 1
      I2 = I1 + N - 1
      REWIND U
      READ (U) (X (MS1), MS1 = I1, I2)
      KI = KI + N
      GO TO 750

```

```

705 I1 = KI + 1
      I2 = I1 + N - 1
      MS3 = 1700 * (MS - 1)
      DO 709 MS1 = I1, I2
      MS3 = MS3 + 1
709 X(MS1) = X(MS3)
      KI + KI + N
750 CONTINUE
28 K = M - 1
      DO 18 J = 1, K
18 ISAVE(J) = J + 1
      ISAVE(M) = 1
      NDEP = 1
C .....
20 CALL CORRI(N, M, X, XBAR, STD, RX, R, D, B, T)
C .....
      CALL PRINT3(XBAR, M, STD, RX, D, R)
C .....
      CALL ORDER(M, R, NDEP, K, ISAVE, RX, RY)
C .....
      CALL MINV(RX, K, DET, B, T)
C .....
      IF (DET) 22, 21, 22
21 WRITE (3, 6)
6 FORMAT ('0 LA MATRIZ ES SINGULAR, ESTA SELECCION SE ABANDONA.--')
      GO TO 16
C .....
22 CALL MULTR(N, K, XBAR, STD, D, RX, RY, ISAVE, B, SB, T, ANS)
C .....
      WRITE (3, 7)
7 FORMAT ('0 NUMERO DE ORDEN DE LAS VARIABLES QUE SE OCUPARON EN ESTA.
      IREGRESION (LA PRIMERA ES LA VARIABLE DEPENDIENTE)'/)
      WRITE (3, 8) (ISA(I), I = 1, M)
8 FORMAT ('O', I615)
      MOPC = NOPC - 1
      WRITE (3, 23) M, MOPC, NLIST, NCOMP, NCAM
23 FORMAT ('///, 'LA SEGUNDA TARJETA DE CONTROL DE LA SELECCION FUE'///
      115, 4I2, '(M, NOPC, NLIST, NCOMP, NCAM)'/)
      CONST = ANS(1)
      IF (NOPC - 1) 24, 26, 24
24 IF (NOPC - 5) 25, 26, 25
25 ANS(1) = EXP(ANS(1))
C .....
26 CALL PRINT4(M, ISAVE, B, K, ANS, SB, T)
C .....
      GO TO 16
75 FORMAT(5F5.3)
76 FORMAT(6F5.3)
77 FORMAT(7F5.3)
78 FORMAT(8F5.3)
80 FORMAT(10F5.3)
81 FORMAT(5X, F5.2, 2F7.2, 36X, F6.2)
99 STOP
      END

```

APPENDIX II

RESIDUALS PLOTTING PROGRAM

```

FILE IN TARJ (1,10);
FILE OUT IMPR 17(2, 17); FILE DISCO DISK SERIAL [2:1000](2, 13, 26);
ARRAY C[1:2], A[1:9], B[1:5];
REAL V;
ALPHA COIN;

```

```

LABEL P3;
INTEGER NAME, NES, I, J, K, NE, NPAG, L, L2;
DEFINE PAG = WRITE (IMPR PAGE) #;
FORMAT FT1 (I4, 3F7.3, 9F6.3);
NES ← 0;
PAG;
P3: READ (TARJ, FT1, NAME, V, C[1], C[2], FOR K ← 1 STEP 1 UNTIL 9 DO A[K]);
NES ← NES + 1; WRITE (DISCO, *, NAME, V, C[1], C[2], FOR K ← 1 STEP 1 UNTIL 9 DO
A[K])
; IF NAME < 9999 THEN GO TO P3;
BEGIN COMMENT SE DEFINEN LAS MATRICES;
ARRAY R, Y, Y2 [1:NES]; INTEGER ARRAY NOMBRE [1:NES];
LABEL P4, P10, P12, P13, P5;
FORMAT FT2 (2I1, 5F10.7);
FORMAT FT5 (X35, "C O E F I C I E N T E S           E M P L E A D O S", ///);
FORMAT FT8 (X3, "I =", I1, X4, "J =", I1, X4, "M (PRO) =", F10.7, X4, "K =", F10.7, X4
,"B1 =", F10.7, X4, "B2 =", F10.7, X4, "B3 =", F10.7);
FORMAT FT25 (///, X25, "FIN"), FT35 (//////////);
P4: REWIND (DISCO);
READ (TARJ, FT2, I, J, FOR K ← 1 STEP 1 UNTIL 5 DO B[K]);
IF I = 0 THEN GO TO P10;
IF I = 1 THEN COIN ← "B - V" ELSE COIN ← "V - R";
WRITE (IMPR, FT35);
WRITE (IMPR, FT5);
WRITE (IMPR, FT8, I, J, FOR K ← 1 STEP 1 UNTIL 5 DO B[K]);
NE ← 0;
P12: READ (DISCO, *, NAME, V, C[1], C[2], FOR K ← 1 STEP 1 UNTIL 9 DO A[K]);
IF A[J] = THEN BEGIN IF NAME < 9999 THEN GO TO P12 ELSE GO TO P5 END;
NE ← NE + 1;
R[NE] ← A[J] - V - B[2] - B[3] × C[I] - B[4] × (A[J] - B[1] - B[5] × (A[J] - B[1]) × C[I];
Y[NE] ← V; Y2[NE] ← C[I]; NOMBRE[NE] ← NAME;
GO TO P12;
P5: BEGIN COMMENT DIBUJA LAS GRAFICAS;
ALPHA ARRAY PLANO [-21:133, -60:60]; LABEL SIGUE, CONT;
FORMAT RENG (X3, 12I1A1);
FORMAT FRTO1 ("LA ESTRELLA", I4, "ESTA FUERA DEL RANGO");
FORMAT FT30 (//////////);
DEFINE AVISA = WRITE (IMPR, FRTO1, NOMBRE [K]) #, COSA = GO TO SIGUE END #,
COSAI = IF PLANO [I, J] ← #, COSA2 = THEN BEGIN PLANO [I, J] ← #, COSA 3 =
GO TO CONT END #;
WRITE (IMPR, FT30);
FOR K ← -60 STEP 1 UNTIL 60 DO
FOR L ← -21 STEP 1 UNTIL 113 DO PLANO [L, K] ← " ";
FOR K ← -60 STEP 1 UNTIL 60 DO PLANO [-21, K] ← PLANO [113, K] ← "+";
FOR L ← -21 STEP 1 UNTIL 113 DO PLANO [L, 60] ← PLANO [L, -60] ← "+";
WRITE (IMPR, FT30);
FOR K ← 1 STEP 1 UNTIL NE DO BEGIN
I ENTIER (Y[K] × 13.333333333 + .5); J ← ENTIER (R[K] × 133.333333333 + .5);
IF ABS (J) > 60 OR I < -21 OR I > 113 THEN BEGIN AVISA; COSA;
COSAI " " OR PLANO [I, J] = "+" COSA2 "***"; COSA;
COSAI "*" COSA2 "#"; COSA;
COSAI "#" COSA2 "<"; COSA;
COSAI "<" COSA2 "X"; COSA;
COSAI "X" COSA2 "."; COSA;
COSAI "." COSA2 "-"; COSA;
SIGUE: END;
WRITE (IMPR, FT30);
FOR K ← -21 STEP 1 UNTIL 113 DO
WRITE (IMPR, RENG, FOR L ← -60 STEP 1 UNTIL 60 DO PLANO [K, L]);
FOR K ← -20 STEP 1 UNTIL 133 DO
FOR L ← -60 STEP 1 UNTIL 60 DO PLANO [K, L] ← " ";
FOR K ← -60 STEP 1 UNTIL 60 DO PLANO [-20, K] ← PLANO [133, K] ← "+";
FOR K ← -20 STEP 1 UNTIL 133 DO PLANO [K, 60] ← PLANO [K, -60] ← "+";
WRITE (IMPR, FT30);

```

```

FOR K ← 1 STEP 1 UNTIL NE DO
BEGIN
I ← ENTIER (Y2[K] × 66.66666666 + .5); J ENTIER (R[K] × 133.33333333 + .5);
IF ABS (J) > 60 OR I = -20 OR I > 133 THEN BEGIN AVISA; COSA3;
COSA1 "" OR PLANO [I, J] = "+" COSA2 "*"; COSA3;
COSA1 "*" COSA2 "#"; COSA3;
COSA1 "#" COSA2 "<"; COSA3;
COSA1 "<" COSA2 "X"; COSA3;
COSA1 "X" COSA2 "."; COSA3;
COSA1 "." COSA2 "-"; COSA3;
CONT: END;
WRITE (IMPR, FT30);
FOR K ← -20 STEP 1 UNTIL 133 DO
WRITE (IMPR, RENG, FOR L ← -60 STEP 1 UNTIL 60 DO PLANO [K, L]);
END TERMINA DE DIBUJAR;
GO TO P4;
P10: WRITE (IMPR, FT35);
WRITE (IMPR, FT25);
END;
END.

```

APPENDIX III

KEY DATA FOR FIGURES 1-48

Ordinates range from -0.45 to $+0.45$ mag. ($^{0.9}/_{121}$ mag/+).

Abscissas (magnitude-diagrams) range from -1.6 to $+8.5$ mag ($^{10.1}/_{13}$ mag/+).

Abscissas (color-diagrams) range from -0.3 to $+2.0$ mag ($^{2.3}/_{154}$ mag/+).

- * denotes one observation.
- # denotes two observations.
- V Denotes three observations.
- X denotes four observations.
- . denotes five observations.
- | denotes more than five observations.

c = constant term

b_i = regression coefficients ($i = 1, 2, 3$).

p = observations with residuals larger than $| 0.45 |$

The straight-line is the locus of residuals equal to zero. Above it positive values. Negative colors and bright magnitudes to the left.































