

ON THE REDUCTION OF THE CARTE DU CIEL CATALOGUES

Jürgen Stock and Johnny Cova S.

Centro de Investigación de Astronomía, Mérida, Venezuela

Received 1981 December 23

RESUMEN

Con miras a recuperar de la Carte du Ciel (CdC) posiciones útiles para la determinación de movimientos propios utilizando métodos de ajuste de bloques recién desarrollados, un área de la zona de Oxford de la CdC que consiste en 24 placas sobreuestas y con época relativamente homogénea se reanalizó utilizando las medidas originales contenidas en el catálogo. Se obtuvieron posiciones para el equinoccio 1950.0 y época 1901.2 de 2911 estrellas hasta la magnitud límite del catálogo utilizando independientemente como sistema de referencia tanto el AGK3 como el FK4. Nuestros resultados demuestran que se pueden obtener posiciones precisas hasta 0."3 y que el método de ajuste de bloques empleado, es capaz de absorber términos de distorsión que son función lineal de las coordenadas. También se demuestra que no existen otros términos importantes de distorsión en el área escogida.

ABSTRACT

In the hope of retrieving useful positions for proper motion determinations from the Carte du Ciel (CdC) using recently developed block adjustment methods, an area from the Oxford Zone I of the CdC consisting of 24 overlapping plates of relatively homogeneous epoch was reanalyzed using the original measurements contained in the catalogue. Positions for equinox 1950.0 and epoch 1901.1 were obtained for 2911 stars down to the limiting magnitude of the catalogue using independently both the AGK3 and the FK4 catalogues as reference systems. Our results show that positions accurate to 0."3 may be obtained and that the block adjustment method used is capable of absorbing distortion terms which are a linear function of the coordinates. It is also shown that no other important distortion terms are present in the chosen plate material.

Key words: PROPER MOTIONS – STARS-CATALOGS

I. INTRODUCTION

The Carte du Ciel is the oldest practically complete astrophotographic coverage of the sky. The authors were fully aware of the necessity to complete coverage within as short a time span as possible. This, together with atmospheric refraction problems, led to a distribution of the work among a fairly large number of observatories. The consequence of this is a rather inhomogeneous material. Some zones, through subsequent analysis, have become known to be of surprisingly high accuracy, while others may possibly never serve their original purpose.

To make full use of the usable part of the Carte du Ciel two additional sources of data are needed: first, a modern epoch of position observation has to be produced. As has been shown by Della Prugna (1981) and by Cova (1981), not necessarily do the new observations have to be made with the same telescopes. A second and far more serious problem is the production of a reference system for the Carte du Ciel plates, unless one is satisfied with relative proper motions. The latter shall not be pursued any further in this paper.

Furthermore, a detailed analysis of the specific characteristics of the telescopes involved is required. Here we

refer to systematic errors such as field distortion (radial or asymmetric), color and magnitude dependent distortions, etc. For the telescopes responsible for the modern epoch this constitutes no major problem, since comparisons can be made with error-free data (see for instance Stock 1978). Concerning the Carte du Ciel material, use has to be made of the same old epoch plates since it cannot be assumed that the characteristics of the respective telescopes have remained unchanged for almost a century. As will be shown, the generous plate overlap provided by the Carte du Ciel plan permits an *a posteriori* determination of such errors based on the same plate material.

An extensive and detailed description of the status of the Carte du Ciel project is given by Eichhorn (1974). In some cases, for instance the Oxford zones, the original authors already give expressions which permit the conversion of the measured plane coordinates into equatorial coordinates. More recently, Günther and Kox (1972) reanalyzed one of the Oxford zones and give revised plate constants including color and magnitude terms. Also they refer the positions to the now generally accepted reference system defined by the FK4 Catalogue.

We proposed ourselves to elaborate a pilot project of

a reanalysis of a limited section of the Oxford I zone, using the original measurements contained in the catalogue and block adjustment principles. The project shall include an attempt to determine the field distortion of the Oxford astrograph. The AGK3 catalogue will be used as reference system, but it will also be attempted to use the FK4 as the only reference source.

II. THE TEST FIELD

Within a limited portion of the Oxford I catalogue presently available to us we selected as large a block of overlapping plates as possible, imposing the condition of a uniform epoch. The best choice that could be made is a field of 24 plates. Their numbers, epochs, and relative location as shown schematically in Figure 1.

The next step was to identify stars common to two or more plates. For this purpose the plate constants given in the catalogue were used, converting the original X and Y values into equatorial coordinates on a uniform system. These coordinates then were used to establish identities. Figure 2 shows the number of links which exist between the different plates.

III. COORDINATE TRANSFORMATION

Following a procedure proposed by Stock (1981) the measured coordinates X and Y are transformed to cartesian space coordinates u, v, w by

$$\tan r = \frac{(x^2 + y^2)^{1/2}}{F} \quad (1)$$

$$u = x \cos r , \quad (2)$$

$$v = y \cos r , \quad (3)$$

and

$$w = F \cos r . \quad (4)$$

Here it is assumed that tangential projection is applicable to the specific case. It is assumed that the origin of

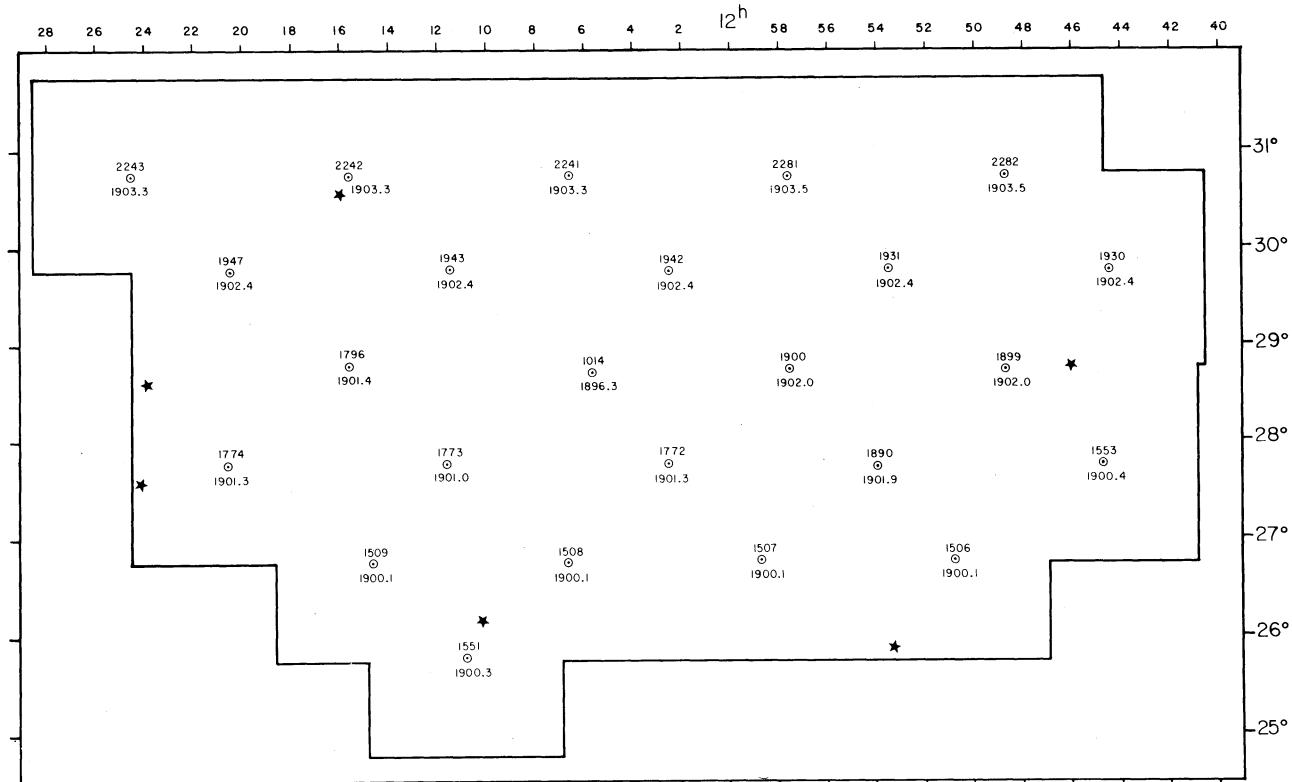


Fig. 1. Relative location, number, and epoch of the Oxford plates used in this paper. Asterisks indicate the location of reference stars contained in the FK4 supplements.

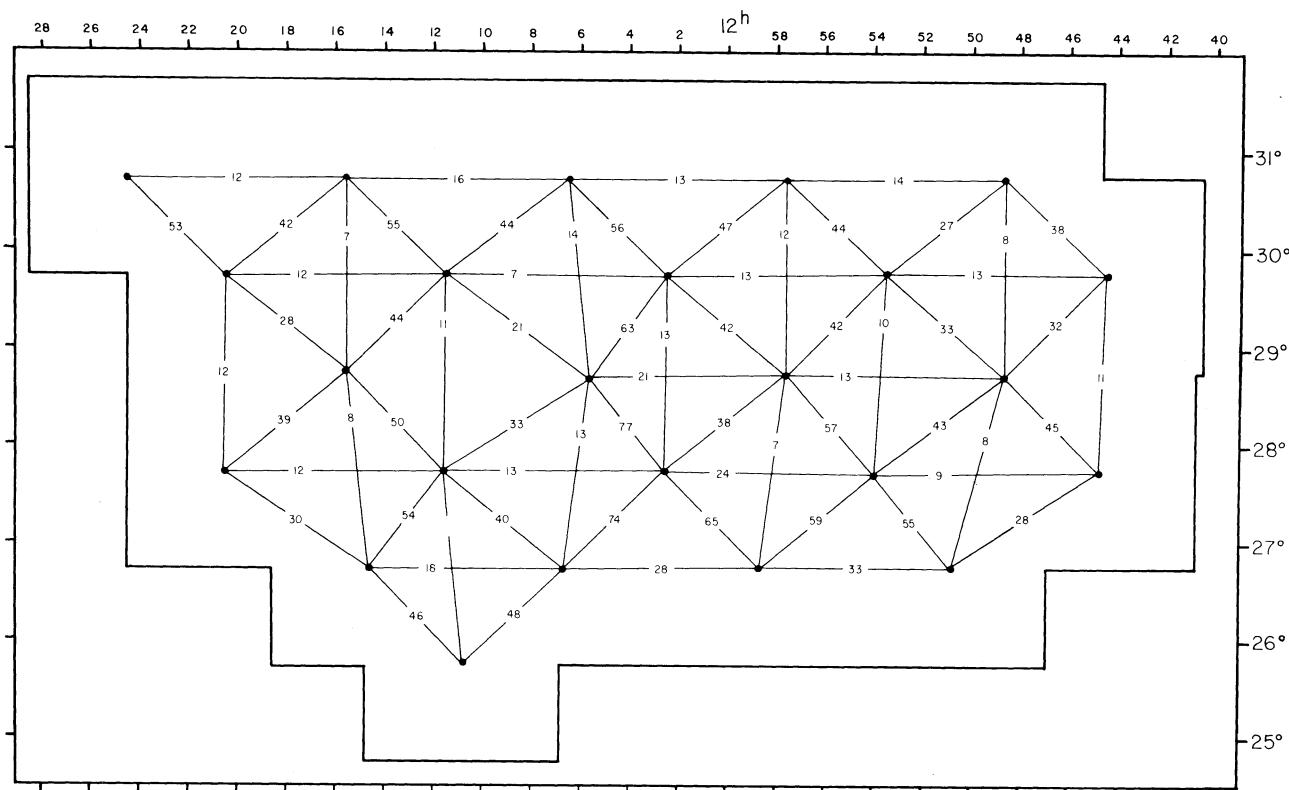


Fig. 2. Schematic representation of stars common to neighboring plates.

the X and Y coordinates coincides with the tangential point. These coordinates are transformed into standard three-dimensional coordinates ξ, η, ζ by

$$\xi = a_{11} u + a_{12} v + a_{13} w , \quad (5)$$

$$\eta = a_{21} u + a_{22} v + a_{23} w , \quad (6)$$

$$\zeta = a_{31} u + a_{32} v + a_{33} w . \quad (7)$$

The latter are related to the equatorial coordinates α and δ by

$$\xi = F \sin \alpha \cos \delta , \quad (8)$$

$$\eta = F \cos \alpha \cos \delta , \quad (9)$$

$$\zeta = F \sin \delta . \quad (10)$$

The matrix a_{ij} in equations (5) to (7) is an orthogonal rotation matrix. The values of the coefficients are determined from stars for which X and Y as well as α and δ are known. If a plate by plate reduction is carried out, a minimum of three reference stars per plate is required. When overlapping plates covering a larger field are available, block adjustment principles may be used. In such a case, a minimum of three reference stars in the entire field is required. Least square methods are applied when the number of equations exceeds the number of unknowns. The equations to be used are

$$a_{m11} u_{mi} + a_{m12} v_{mi} + a_{m13} w_{mi} = \xi_i + \epsilon_{\xi i} , \quad (11)$$

$$a_{m21} u_{mi} + a_{m22} v_{mi} + a_{m23} w_{mi} = \eta_i + \epsilon_{\eta i} , \quad (12)$$

$$a_{m31} u_{mi} + a_{m32} v_{mi} + a_{m33} w_{mi} = \zeta_i + \epsilon_{\zeta i} , \quad (13)$$

in the case of a reference star with the number i measured on the plate with the number m , the values ξ_i, η_i, ζ_i are calculated from equations (8) to (10). The coefficients

a_{mij} are the rotation matrix corresponding to plate m . The errors $\epsilon_{\xi i}$, $\epsilon_{\eta i}$, $\epsilon_{\zeta i}$ are residuals accumulated by errors in the measured coordinates, the coefficients, and the catalogue positions.

For an object i measured on plates m and n the equations

$$\begin{aligned} a_{m11} u_{mi} + a_{m12} v_{mi} + a_{m13} w_{mi} - a_{n11} u_{ni} - a_{n12} v_{ni} \\ - a_{n13} w_{ni} = \epsilon_{\xi i}, \end{aligned} \quad (14)$$

$$\begin{aligned} a_{m21} u_{mi} + a_{m22} v_{mi} + a_{m23} w_{mi} - a_{n21} u_{ni} \\ - a_{n22} v_{ni} - a_{n23} w_{ni} = \epsilon_{\eta i}, \end{aligned} \quad (15)$$

$$\begin{aligned} a_{m31} u_{mi} + a_{m32} v_{mi} + a_{m33} w_{mi} - a_{n31} u_{ni} \\ - a_{n32} v_{ni} - a_{n33} w_{ni} = \epsilon_{\zeta i} \end{aligned} \quad (16)$$

may be used.

Evidently, the distribution of the residuals calculated in the equations (11) to (16) is not necessarily Gaussian, even if the error distribution of the measured data or the catalogue positions are of a Gaussian type. Even so, experience shows that very good approximations for the coefficients a_{mij} can be obtained by imposing

$$\sum \epsilon_{\xi i}^2 = \text{Minimum},$$

$$\sum \epsilon_{\eta i}^2 = \text{Minimum},$$

$$\sum \epsilon_{\zeta i}^2 = \text{Minimum}.$$

In any case the procedure which we have used leads to an algorithm which is very easy to handle.

The sums of the residuals must include all objects and all plates for which either set of the above equations is applicable. For each object weight factors may be applied to either equations (11) to (13) or equations (14) to (16).

IV. FIELD DISTORTION

When the measured plate coordinates X and Y contain distortion components, then equations (1) to (3) cannot be applied directly. The coordinates have to be corrected first to an undistorted system. However, as was mentioned by Stock (1981), if orthogonality is not imposed on the matrices, then the system worked out in Section III is capable of absorbing distortion terms which are linear functions of the coordinates. This means that, excepting large zenith distances, no correction for differential refraction is required. The same is true for other minor effects, such

as for example the aberration of light due to the earth's motion. The principal effect we are concerned with here is due to the optical system. We can distinguish several types of distortions. Some are related to the location of the images, others to their structure. We can also distinguish distortion of radial symmetry which is independent of the position angle on the plate from unsymmetric types which show a position-angle dependence.

Considering the type of optics of the Oxford refractor we may at first instance expect what is usually termed as a "pin cushion" or "barrel" deformation of the field. We shall at this point neglect effects due to either coma or to chromatic aberrations. Thus, the displacement ΔR of an image in the direction of the radius R (distance from tangential point) takes the form

$$\Delta R(R) = \sum_{i=1}^N b_i R^{2i} \quad (17)$$

with

$$R = (X^2 + Y^2)^{1/2}. \quad (18)$$

For reasons of symmetry only even powers of R are used. The extent of the expansion, i.e., the value of N , has to be determined empirically.

Let us consider the case of two partially overlapping plates, with the measured coordinates X_1 , Y_1 and X_2 , Y_2 respectively. If no distortion is present, the three dimensional coordinates ξ_1 , η_1 , ζ_1 , and ξ_2 , η_2 , ζ_2 can be calculated from equations (1) to (4). Between these two sets of coordinates we expect the relation

$$\xi_1 = a_{11} \xi_2 + a_{12} \eta_2 + a_{13} \zeta_2, \quad (19)$$

$$\eta_1 = a_{21} \xi_2 + a_{22} \eta_2 + a_{23} \zeta_2, \quad (20)$$

$$\zeta_1 = a_{31} \xi_2 + a_{32} \eta_2 + a_{33} \zeta_2, \quad (21)$$

Again the matrix a_{ij} is an orthogonal matrix. This time, however, its diagonal elements will be near unity, and the remaining ones near zero.

For the field size under consideration $\xi \sim X$ and $\eta \sim Y$, such that we may use

$$\rho = (\xi^2 + \eta^2)^{1/2} \quad (22)$$

and

$$\Delta \rho(\rho) = \sum_{i=1}^N b_i \rho^{2i} \quad (23)$$

instead of equations (17) and (18).

The components of the distortion in the ξ - and η -direction are

$$\Delta\xi = \frac{\xi}{\rho} \Delta\rho \quad (24)$$

and

$$\Delta\eta = \frac{\eta}{\rho} \Delta\rho \quad (25)$$

These terms have to be introduced into equations (19) and (20). Considering that these correction terms may be expected to be very small, we shall neglect their products with the matrix elements which are small, and find

$$\begin{aligned} \xi_1 \left(1 + \frac{\Delta\rho_1}{\rho_1}\right) &= a_{11} \xi_2 \left(1 + \frac{\Delta\rho_2}{\rho_2}\right) \\ &+ a_{12} \eta_2 + a_{13} \xi_2 , \end{aligned} \quad (26)$$

$$\begin{aligned} \eta_1 \left(1 + \frac{\Delta\rho_1}{\rho_1}\right) &= a_{21} \xi_2 + a_{22} \eta_2 \\ &+ a_{23} \xi_2 . \end{aligned} \quad (27)$$

Each of these two equations contains $3 + N$ unknowns, of which the b_k -terms are common to both. For a least-square determination of the latter from plate pairs with more than $3 + N$ stars in common we can either solve the ξ - and η terms separately and check whether both lead to the same b_k coefficients, or we can combine them into one single set of $6 + N$ equations with an equal number of unknowns, thus imposing equality of the b_k -terms.

For the empirical determination of the b_k -coefficients we selected all plate pairs which had forty or more stars in common, a total of 24 pairs. The effectiveness of the method outlined above was demonstrated accidentally using these plate pairs. Due to an error in the computer program an improper projection geometry was applied to the plates. This error was detected on the basis of the large and consistent coefficients which the test produced, and which corresponded exactly to the difference between the applied and the correct projection. After correcting the error the coefficients became of an erratic nature, amounting to insignificant values if averaged over the 24 plate pairs. The matrix coefficients, on the other hand, deviate significantly and consistently from an orthogonal matrix. This means that the type of field

distortion present in the Oxford Refractor, due to the optics, telescope alignment, atmospheric refraction, screw errors of the measuring machine, etc., are effectively absorbed by the matrix if orthogonality is not imposed.

V. REDUCTION WITH THE AGK3 SYSTEM

A total of 335 stars were found to be in common with the AGK3 catalogue, with an average of 25 stars per plate. For each catalogue star the position was calculated for the epoch of 1901.2, the latter being the average epoch of the 24 Oxford plates. The block reduction was then carried out using unit weight for all links and for all reference objects.

From the position obtained for stars occurring on two or more plates their mean errors can be calculated. The mean rms errors ϵ_α and ϵ_δ for a single image are

$$\epsilon_\alpha = 0^{\circ}031 \quad \text{and} \quad \epsilon_\delta = 0''.22.$$

These correspond to just a little more than half of the last digit of the coordinates in the original Oxford Catalogue. This does not leave much room for color- or magnitude-dependent systematic errors. The latter type of error cannot be absorbed by the matrix elements.

VI. REDUCTION WITH THE FK4 CATALOGUE

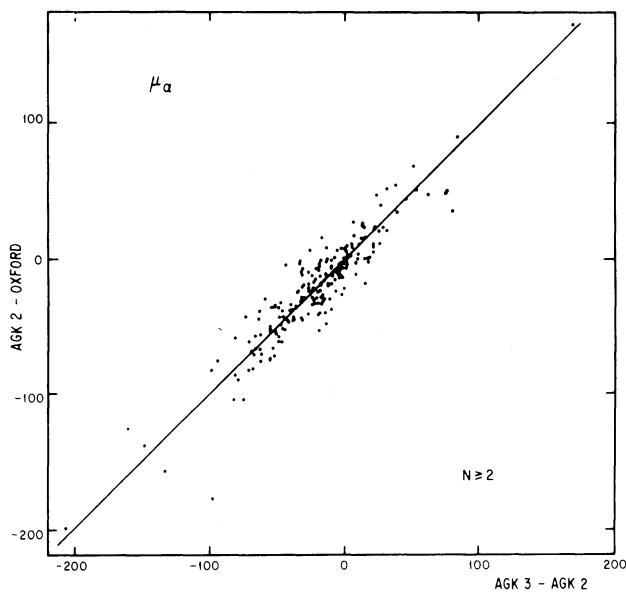
Six stars were found in common with the supplements of the FK4 (1963), none with the main catalogue. As may be appreciated in Figure 2, these stars are not "strategically" located in the field covered by the plates under consideration. Again several solutions were calculated with weights for the reference stars ranging from 1.0 to 100.0. Only minor differences were found between the different solutions. However, they produce rather large systematic differences with the AGK3 in the regions away from the reference stars. These differences amount to several seconds of arc at one edge of the field. Evidently more reference stars, or at least a more favorable distribution is needed. We plan to add plates from neighbouring Carte du Ciel zones in order to increase the number of fundamental reference stars.

VII. THE PROPER MOTIONS

Proper motions were calculated by comparing the positions of the AGK2 catalogue with those obtained from the Oxford data. For the latter, naturally, we used the solution based on the AGK3 as reference source. A mean epoch difference of 28.9 years was adopted. Comparisons of these proper motions, i.e., AGK2-Oxford, with the proper motions AGK3-AGK2 is shown in Figure 3. Only stars appearing on two or more Oxford plates were used for the graphs. In this form practically all stars along the edge of the field were eliminated. The remaining stars were plotted in Figure 4. The notorious increase in the

scatter is attributed to two sources, namely, (1) the Oxford position has less weight, and (2) most of the stars are located outside of the area where the block adjustment is effective. Thus, positions and proper motions, as given in Table 1 and Table 2, are of full weight only when the position is located within the limits.

$$11^{\text{h}} 45^{\text{m}} < \alpha < 12^{\text{h}} 20^{\text{m}}, \quad 26^{\circ} 45' < \delta < 30^{\circ} 45'.$$



VIII. THE POSITION CATALOGUE
The positions given in Table 1 are for a mean epoch of 1901.2, for the equinox 1950.0. The columns contain the following data:

column	1: Running number
columns	2- 4: Right ascension
column	5: Mean error of right ascension

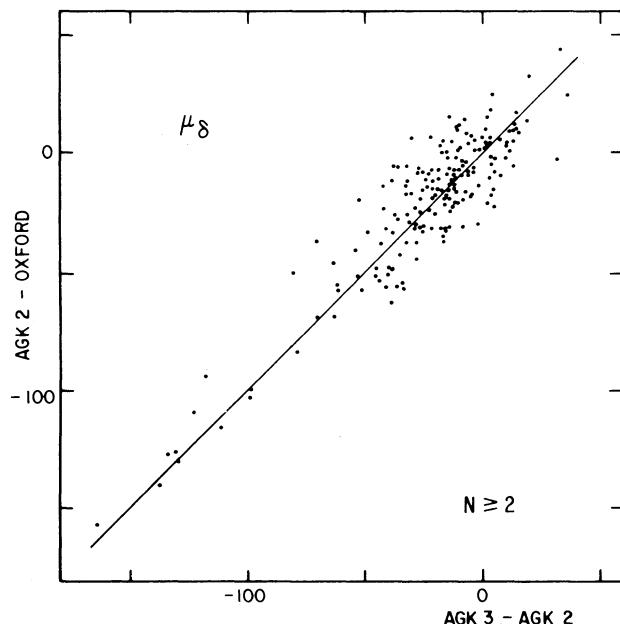


Fig. 3. Comparisons of proper motions AGK3–AGK2 versus AGK2–Oxford for stars which occur on two or more Oxford plates.

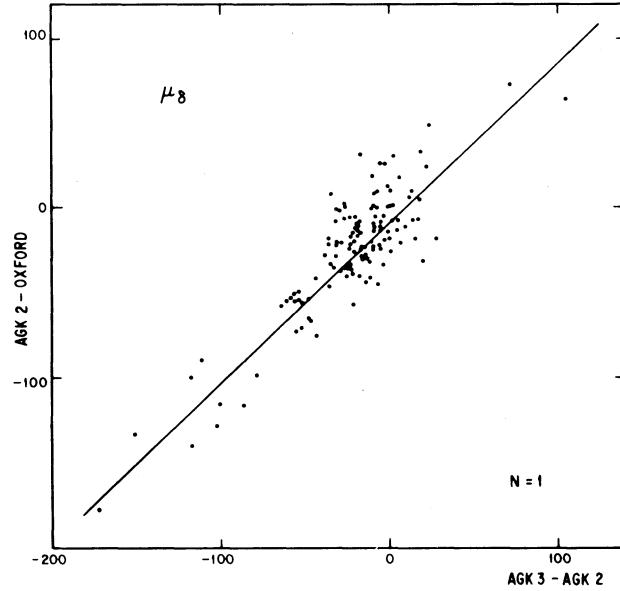
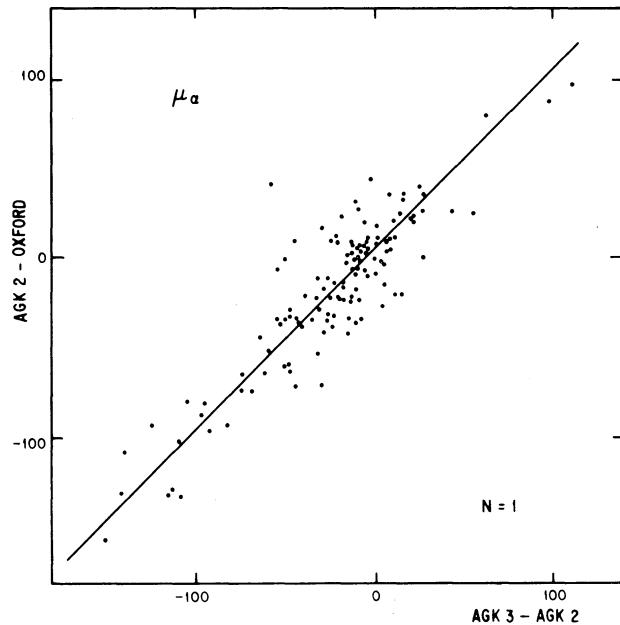


Fig. 4. Comparisons of proper motions AGK3–AGK2 versus AGK2–Oxford for stars which occur on only one Oxford plate.

- columns 6-8: Declination
- column 9: Mean error of declination
- column 10: Magnitude as given in the Oxford Catalogue
- column 11: Number of Oxford plates on which the stars occurs
- column 12: 1 indicates that the star appears in the AGK3; 2 indicates that it appears in the FK4-Supplement.

IX. THE CATALOGUE OF PROPER MOTIONS

The proper motions AGK2–Oxford and AGK3–AGK2 are given in Table 2. The columns contain:

- column 1: Running number of Table 1
- column 2: Right ascension
- column 3: Declination
- column 4: Magnitude as given in the Oxford Catalogue
- column 5: Proper motion in right ascension in $0.^{\circ}001/\text{year}$ from AGK2–Oxford
- column 6: Proper motion in declination in $0.^{\circ}001/\text{year}$ from AGK2–Oxford
- column 7: Proper motion in right ascension in $0.^{\circ}001/\text{year}$ from AGK3–AGK2
- column 8: Proper motion in declination in $0.^{\circ}001/\text{year}$ from AGK3–AGK2.

X. THE CROSS REFERENCE CATALOGUE

For future reference and for other users we give in Table 3 the running number of Table 1 and the corresponding Oxford plate numbers and star numbers. It is important to note that we have used only the last four digits of the star numbers given in the Oxford catalogue.

REFERENCES

- Cova, J. 1981, *Rev. Mexicana Astron. Astrof.*, 6, 123.
- Della Prugna, F. 1981, *Rev. Mexicana Astron. Astrof.*, 6, 119.
- Eichhorn, H. 1974, in *Astronomy of Star Positions*, (New York: Frederick Ungar Publishing Co. Inc.), p. 279.
- Fricke, W. and Kopff, A. 1963, *Veroff. des Astronomisches Rechen-Instituts Heidelberg*, (FK4-Suppl.) No. 11.
- Günther, A. and Kox, H. 1972, *Astr. and Ap. Suppl.*, 6, 201.
- Heckmann, O. and Dieckvoss, W. 1975, *Dritter Katalog der Astronomischen Gesellschaft (AGK3)*, (Hamburg-Bergerdorf).
- Schorr, R. and Kohlschütter, A. 1951, *Zweiter Katalog der Astronomischen Gesellschaft (AGK2)*, (Hamburg-Bergerdorf).
- Stock, J. 1978, in *IAU Coll. No. 48, Modern Astrometry*, eds. F.V. Prochazka and R.H. Tucker, (Vienna: University Observatory), p. 411.
- Stock, J. 1981, *Rev. Mexicana Astron. Astrof.*, 6, 115.
- Turner, H. 1910, *Oxford Astrographic Catalogue*, (Oxford: University Observatory).

REDUCTION OF CDC CATALOGUES

251

2578	21	39.85	30	48	26.9	11.5	1	2716	12	24	3.16	0.02	29	50	30.7	0.3	11.9	1	
2579	12	21	40.04	30	56	1.7	1	2717	12	24	3.62	0.02	31	73	33.4	0.2	11.9	1	
2580	12	21	40.46	0.06	29	45	57.0	0.4	2718	12	24	3.71	0.01	29	50	36.9	0.2	12.4	2
2581	12	21	42.54	28	41	1.9	1	2719	12	24	3.82	0.04	30	54	45.5	0.2	12.4	2	
2582	12	21	42.55	29	41	2.0	1	2720	12	24	5.53	0.2	27	3	4.1	11.7	1	1	
2583	12	21	44.27	27	52	29.7	0.4	2721	12	24	6.28	0.2	31	0	0.4	11.3	1	1	
2584	12	21	45.68	0.01	30	46	43.7	0.4	2722	12	24	6.71	0.2	27	55	3.0	11.4	1	1
2585	12	21	46.23	29	52	14	2.4	2723	12	24	10.48	0.04	30	13	8.9	0.5	12.4	2	
2586	12	21	47.79	31	33	2.4	0.3	2724	12	24	10.57	0.04	25	35	38.7	0.5	11.4	1	
2587	12	21	48.20	0.00	30	23	32.4	0.3	2725	12	24	11.19	0.04	26	45	59.1	0.5	11.4	1
2588	12	21	49.55	28	19	40.0	0.0	2726	12	24	11.94	0.04	31	18	48.1	0.5	11.9	1	
2589	12	21	49.89	28	19	43.3	0.0	2727	12	24	12.86	0.04	29	29	24.3	0.5	12.4	1	
2590	12	21	53.43	26	51	26.2	0.0	2728	12	24	15.63	0.04	31	35	41.7	0.5	12.4	1	
2591	12	21	55.08	27	52	29.7	0.4	2729	12	24	15.74	0.01	30	59	6.0	0.5	12.4	2	
2592	12	21	56.89	24	47	10.5	1	2730	12	24	16.52	0.02	20	32	17.6	0.5	11.7	2	
2593	12	21	57.46	29	23	6.2	1	2731	12	24	17.83	0.04	27	6	9.7	0.5	12.4	2	
2594	12	21	59.39	29	58	17.0	1	2732	12	24	19.58	0.04	29	29	19.3	0.5	12.4	1	
2595	12	22	0.13	29	8	26.7	1	2733	12	24	20.57	0.04	27	31	27.3	0.5	12.4	1	
2596	12	22	1.56	29	8	16.5	0.2	2734	12	24	23.66	0.00	30	45	44.5	0.4	11.4	1	
2597	12	22	1.69	0.03	30	3	21.2	0.5	2735	12	24	23.97	0.00	30	1	6.7	0.4	12.4	2
2598	12	22	1.89	31	33	24.4	1	2736	12	24	25.74	0.00	28	19	41.7	0.4	12.4	2	
2599	12	22	2.70	0.05	30	21	43.6	0.1	2737	12	24	25.27	0.00	28	31	45.1	0.4	12.4	2
2600	12	22	4.61	30	53	24.4	0.1	2738	12	24	27.20	0.00	28	32	50.5	0.4	12.4	2	
2601	12	22	5.99	0.00	30	45	3.9	0.2	2739	12	24	31.87	0.00	27	31	18.7	0.4	12.4	1
2602	12	22	8.82	27	51	58.4	0.2	2740	12	24	29.42	0.00	27	6	9.8	0.4	12.4	1	
2603	12	22	8.96	28	49	45.2	0.2	2741	12	24	30.97	0.00	30	5	44.4	0.4	12.4	1	
2604	12	22	9.86	26	56	24.4	0.2	2742	12	24	31.39	0.00	29	53	14.3	0.4	12.4	1	
2605	12	22	12.42	26	56	36.2	0.2	2743	12	24	32.72	0.00	29	15	43.3	0.4	12.4	1	
2606	12	22	12.72	27	26	11.9	1	2744	12	24	33.38	0.00	28	15	48.9	0.4	12.4	1	
2607	12	22	14.20	0.02	30	17	38.1	0.3	2745	12	24	35.87	0.02	30	44	41.3	0.4	12.4	1
2608	12	22	15.38	28	20	0.9	1	2746	12	24	36.37	0.02	27	31	44.7	0.4	12.4	1	
2609	12	22	15.46	27	31	21.5	0.1	2747	12	24	36.41	0.02	27	37	21.5	0.4	12.4	1	
2610	12	22	16.20	31	35	49.8	0.9	2748	12	24	36.51	0.02	27	55	3.4	1.1	12.4	1	
2611	12	22	16.95	31	39	0.9	1	2749	12	24	36.55	0.02	27	11	50.1	0.4	12.4	1	
2612	12	22	17.31	28	43	1.6	1	2750	12	24	36.56	0.02	28	5	45.3	0.4	12.4	1	
2613	12	22	17.69	27	28	37.7	1	2751	12	24	36.79	0.02	27	22	12.5	0.4	12.4	1	
2614	12	22	18.10	21	22	33.3	1	2752	12	24	37.17	0.02	31	39	5.8	0.4	12.4	1	
2615	12	22	18.16	29	8	6.2	1	2753	12	24	37.17	0.02	30	6	45.8	0.2	12.4	2	
2616	12	22	19.76	29	9	6.2	1	2754	12	24	40.40	0.04	27	37	17.0	0.4	12.4	1	
2617	12	22	20.79	21	12	12.4	1	2755	12	24	41.64	0.04	26	51	45.8	0.4	12.4	1	
2618	12	22	20.32	28	1	45.4	1	2756	12	24	42.31	0.04	26	44	0.0	12.4	1	1	
2619	12	22	21.31	27	41	13.8	1	2757	12	24	42.76	0.03	30	70	12.4	0.0	12.4	1	
2620	12	22	21.79	31	18	54.5	1.1	2758	12	24	43.03	0.00	29	46	57.7	0.1	12.4	1	
2621	12	22	23.84	27	20	49.0	1.1	2759	12	24	43.18	0.00	27	30	30.1	1.1	12.4	1	
2622	12	22	23.84	31	22	32.9	1	2760	12	24	43.24	0.02	36	22	56.5	0.1	12.4	2	
2623	12	22	28.58	31	36	41.5	1	2761	12	24	44.20	0.02	30	35	29.0	0.1	12.4	2	
2624	12	22	28.79	31	17	34.1	1	2762	12	24	44.96	0.02	29	35	29.5	0.1	12.4	2	
2625	12	22	29.72	26	51	7.6	0.3	2763	12	24	46.05	0.02	31	36	11.0	0.0	12.4	2	
2626	12	22	31.52	30	57	12.4	0.3	2764	12	24	46.67	0.02	31	40	18.8	0.0	12.4	2	
2627	12	22	31.64	0.01	26	50	14.3	1	2765	12	24	46.85	0.02	28	53	19.6	0.0	12.4	2
2628	12	22	31.93	29	44	1.4	0.1	2766	12	24	47.36	0.02	30	34	36.0	0.1	12.4	2	
2629	12	22	32.08	0.01	31	32	1.4	1	2767	12	24	47.53	0.01	27	40	40.8	0.0	12.4	2
2630	12	22	33.56	31	33	3.3	1	2768	12	24	48.46	0.01	29	25	9.7	0.0	12.4	2	
2631	12	22	33.89	27	31	19.1	1	2769	12	24	48.99	0.01	27	18	25.9	0.0	12.4	2	
2632	12	22	35.30	31	28	31.1	1	2770	12	24	49.27	0.01	30	56	56.5	0.0	12.4	2	
2633	12	22	36.39	28	4	24.4	1	2771	12	24	51.02	0.01	27	26	44.9	0.1	12.4	2	
2634	12	22	36.87	27	11	14.9	1	2772	12	24	54.27	0.01	28	45.8	0.7	1.1	12.4	2	
2635	12	22	40.09	27	56	22.9	1	2773	12	24	55.26	0.01	27	12	25.1	0.1	12.4	2	
2636	12	22	43.60	27	55	24.8	1	2774	12	24	55.79	0.01	27	1	31.0	1	11.7	1	

